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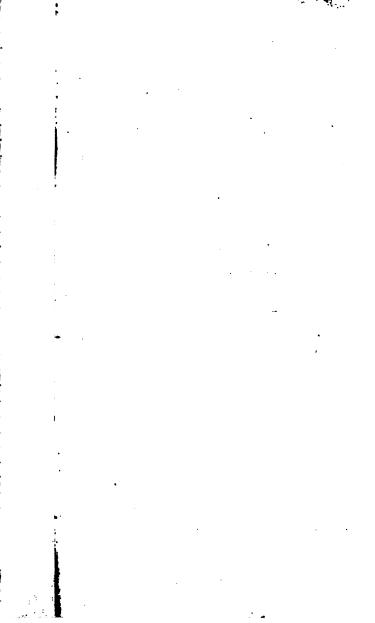
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Gift of Mrs. Emma C. Percy Oakland, calif.

## STANDARD STEEL CONSTRUCTION

A MANUAL FOR

# 

Containing Useful Tables, Formulas and other Information.

Beams, Channels of Structural Shapes,

MADE BY

AMERICAN IRON & STEEL WORKS

Jones & Laughlins, Limited

PITTSBURGH, PA.

CHICAGO, ILL.

REVISED BY D. N. BARKER. PRICE, \$1.00.



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JONES & LAUGHLINS, LIMITED.

ROGERS & SMITH Co., Printers, 148-150 Monroe St., Chicago.

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## PREFACE.

In submitting the following tables of properties of Steel Beams, Channels and other structural material, with tables of strength, etc., we call attention to the fact that they are computed from recent tests and experiments. Although Steel for general construction has been only recently introduced, yet so rapid has been its adoption that all architects and engineers who have kept pace with the time appreciate its advantages and adopt it for all work of any magnitude in preference to wrought and cast iron. The advantages are greater strength and less weight, the material can be made to required specifications and can be inspected at all stages of its manufacture.

We have discontinued making Iron Beams and Channels. We regard our sections of Steel Beams, Channels, Angles, etc., as the most desirable, being the result of our experience. Some of them are lighter sections than made by other mills. We call attention to diagrams showing details.

We are manufacturing Steel Columns of various kinds, notably the "Larimer Column," which is one of the best now on the market. It has proved by tests made and comparison with other Columns to be superior in strength, simplicity in construction, method of connecting, etc.

## Preface to Second Edition.

In this second edition of STANDARD STEEL CON-STRUCTION, we present standard sections of Steel Beams, Channels and Angles, as adopted by the American Association of Steel Manufacturers, January, 1896, and new tables of properties and safe loads; also standard sizes and weights of Larimer Columns, with tables of properties and safe loads.

We also present diagrams of 20 inch Beams, and properties and safe loads of 20 and 24 inch Beams; also diagrams of additional shapes and standard details of roof trusses. We have adopted a different method of numbering our shapes, and call attention to the new system as shown herein. We have added to our steel production an open-hearth basic steel plant of large capacity, and can supply these shapes in Open-Hearth Steel to standard specifications. So satisfactory has been our product of Soft Bessemer and Open-Hearth Steel that we have discontinued the manufacture of our brands of refined iron, and have substituted in all our work our special grades of steel. Our customers, who have used the steel in large quantities, are thoroughly satisfied with the results.

JONES & LAUGHLINS, LIMITED. CHICAGO, July, 1896.



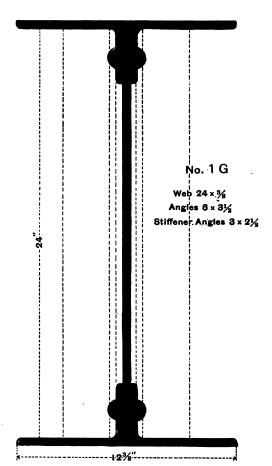
## **DIAGRAMS OF SHAPES**

MANUFACTURED BY

JONES & LAUGHLINS, LIMITED.

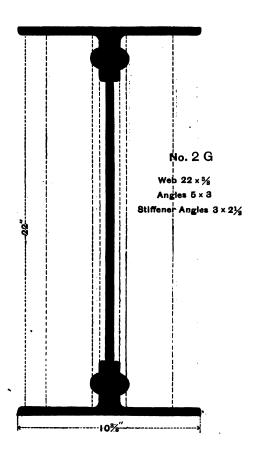


#### PLATE GIRDER. STEEL.



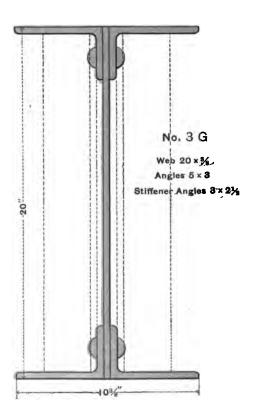
For table giving safe loads see pages 104 and 105.

### PLATE CIRDER. STEEL.



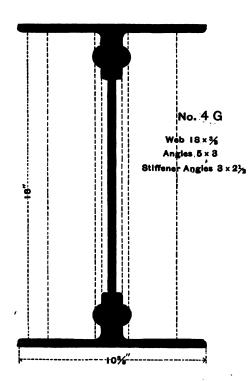
For table giving safe loads see pages 105 and 106.

### PLATE GIRDER, STEEL



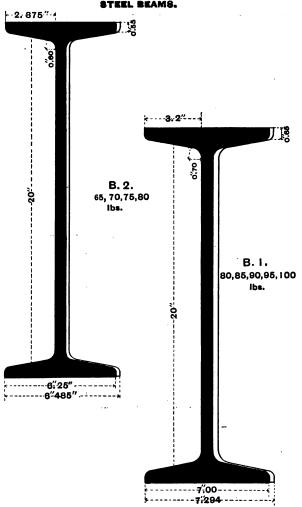
For tables giving safe loads see pages 107 and 108.

### PLATE GIRDERS. STEEL.



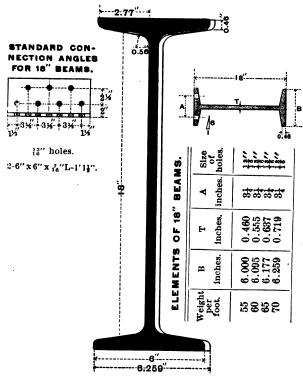
For table giving safe loads see pages 108 and 109.





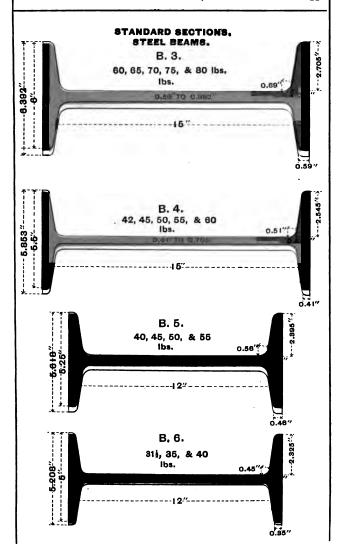
#### STANDARD SECTIONS. STEEL BEAMS.

B. 2 ½ 55, 60, 65 & 70 lbs.

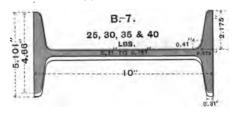


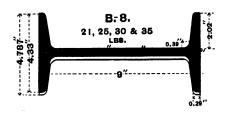
See next page for Properties and Safe Loads.

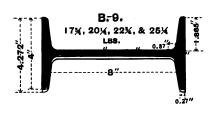
PROPERTIES OF JONES & LAUGHLINS, LIMITED, 18" BEAMS.	13	Radius of Gyration, Meutral Axis as before.	'n	051:1:0 051:1:0 051:1:0 051:1:0	2,000 LBS.	70 Lbs.	22.71	20.97	19.47	18.80	18.17
	12	Moment of In- ertia, Neutral Axia Coinci- dent with Center Line of Web.	ľ	21.19 22.88 23.47 24.68	RJONES & LAUGHLINS, LTD., 18" BEAMS, IN TONS OF	Lbs. 65 Lbs.	.75 21.73 .92 20.86	15 20.	78 18	17 17.	09
	=	Coefficient of Strength of Fiber Strain of 12,500 Lbs. per Sq. In. Used for Bridges.	C,	735,336 778,080 815,000 851,832		55 Lbs. 60	19.61 20	10	81	53	69
	01	Coefficient of Strength for Fiber Strain of 16,000 Lbs. per Sq. In. Used for Buildings.	C.	941,224 995,944 1,048,200 1,090,344		Distance Between Supports In Feet.	07 24 29 25				
	0	Radius of Gyration, Meutral Axis as before.	-	7.06 6.90 6.78 6.68		Lbs. 70 Lbs.	68 32.0 98 30.5	886	32	24	253
	80	Section Factor, Meutral Axis as before.	æ	88.24 93.37 97.80 102.22		Lbs. 65 Ll	29 30. 66 28.	27.	24	23	30
	7	Moment of In- ertia, Neutral Axis perpen- dicular to Web at center.	I	794.15 840.83 880.17 920.02		Lbs. 60	27.63 29. 26.14 27.	2.00	41	88	46
	•	Width of Flange.	Inches.	6.000 6.095 6.177 6.259		Distance Between Supports In Feet,	17				
	10	Thickness of Web.	Inches.	0.460 0.555 0.637 0.719		Lbs. 65 Lbs. 70 Lbs.	54.52				
	4	Area of Section.	Sq. In.	15.93 17.65 19.12 20.59			52.16 47.42 4	19	36	77	9.
	60	Width per Foot.	Lbs.	55 70 70			.80		57	. 30	12
	8	Depth of Beam.	Inches.	18 18 18 18	DB,	55 Lbs. 60	47.06	550	62	38	45
	-	Section.	No.	B 24	SAFE LOA	Distance Between Supports In Feet,	110	53 65	14	15	16

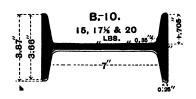


#### STANDARD SECTIONS. STEEL BEAMS.

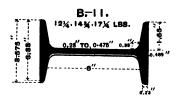


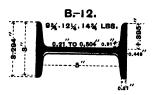


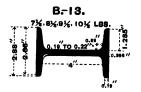




#### STANDARD SECTIONS. STEEL BEAMS.

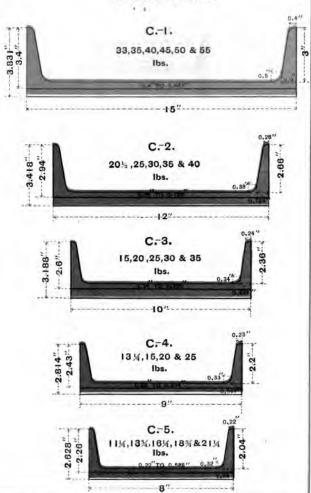




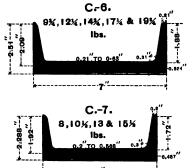


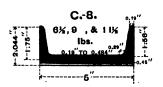
8.14. 5½,6½,7½ LB8. 0.11/"70.0.27 0.886" 0.10"

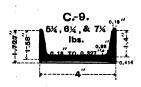
#### STANDARD SECTIONS. STEEL CHANNELS.

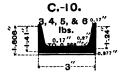


## STANDARD SECTIONS. Steel Channels.



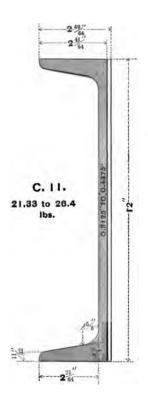






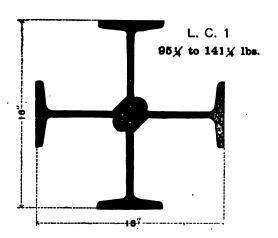
16

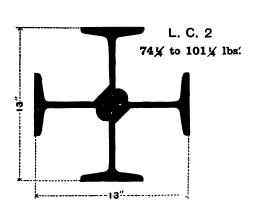
STEEL. CAR TRUCK CHANNEL.



LARIMER COLUMN

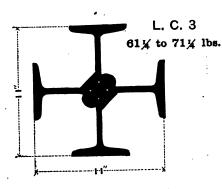


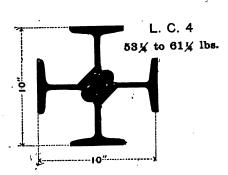




See pages 114 and 115 for safe loads.

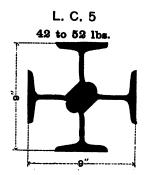
### LARIMER COLUMNS. STEEL.

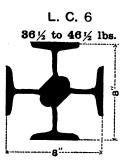


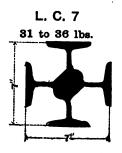


See page 116 for safe loads.

### LARIMER COLUMNS. STEEL,



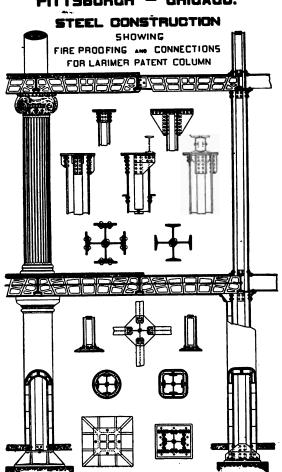


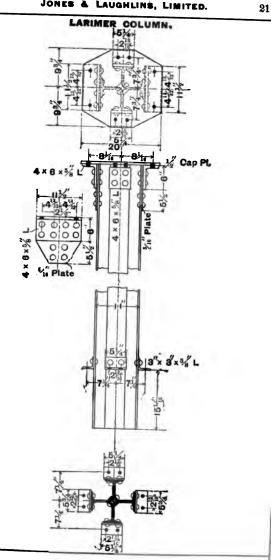




See pages 117 and 118 for safe loads;

## JONES AND LAUCHLINS, LIMITED. PITTSBURGH — CHICAGO.



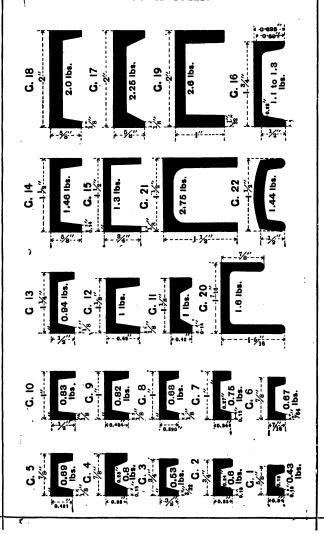


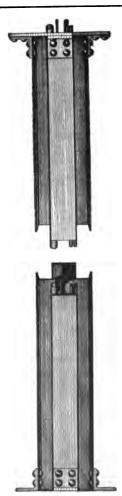


LARINER GREUNIS

MEL BOSCLETS.

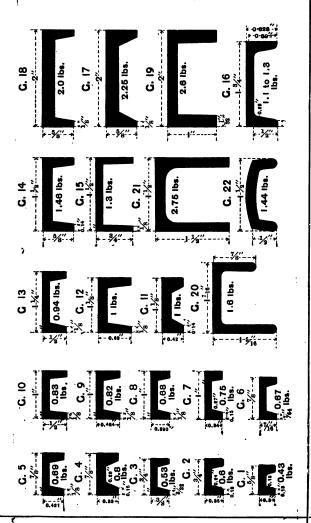
#### GROOVED STEEL.



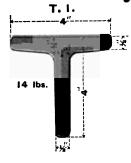


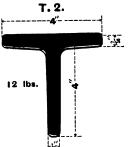
LARIMER COLUMN
SHOWING METURS OF CONCEALING
PIPES, WIRES, ETR.

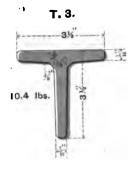
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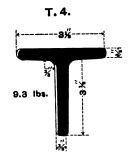


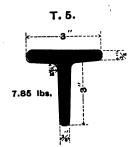
#### EQUAL LEGGED TEES. STEEL.

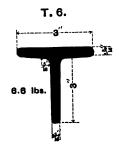


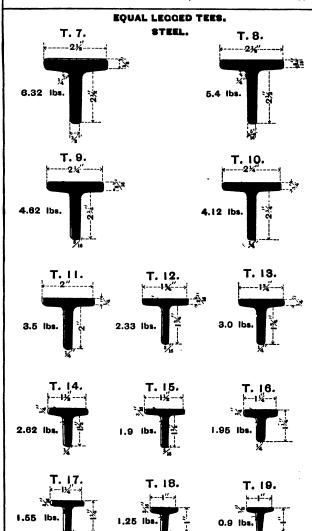




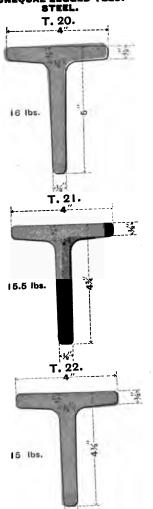






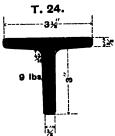


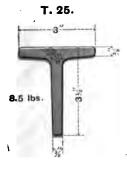
## UNEQUAL LEGGED TEES.

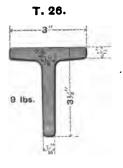


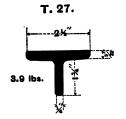
#### UNEQUAL LEGGED TEES. STEEL.

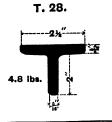
7. 23. 9.8 lbs.



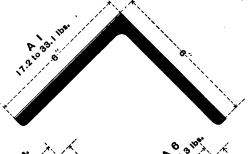


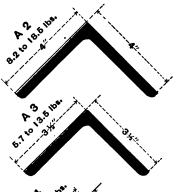


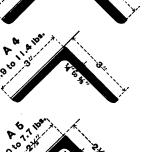




STANDARD SECTIONS STEEL ANGLES WITH EQUAL LEGS.





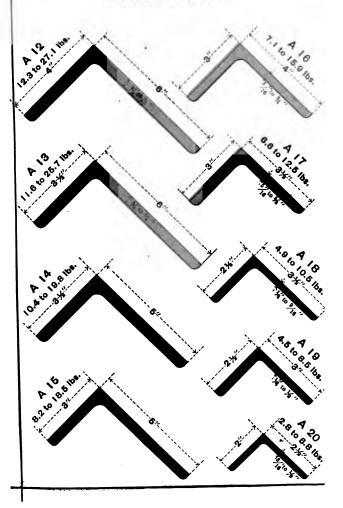








# STANDARD SECTIONS STEEL ANGLES WITH UNEQUAL LEGS

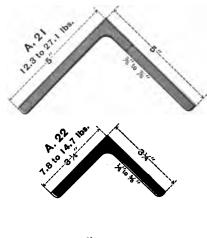


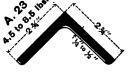
SPECIAL SECTIONS OF ANGLES

MADE TO ORDER

EQUAL LEGS

STEEL.

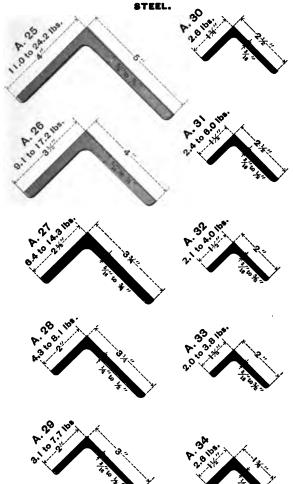






# JONES & LAUGHLINS, LIMITED.

SPECIAL SECTIONS OF AND CALIFORNAL MADE TO ORDER UNEQUAL LEGS



1

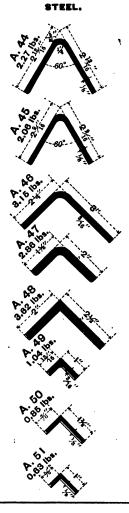
EQUAL LEGGED ANGLES.

Special light sections

STEEL.



SPECIAL SECTIONS OF ANGLES MADE TO ORDER





--24"--M. 6 ---+%"---M. 20 3.5 lbs. 3.50 lbs. M. 7 ---+\*\*\*

M. 14 4.58 lbs. M, 21 3.75 lbs. 3.lbs. ---21/2 --2"--M. 17 ---- 2------+15/6

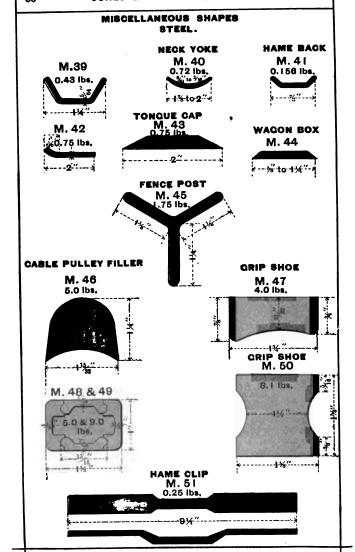
M. 12 5.5 lbs.

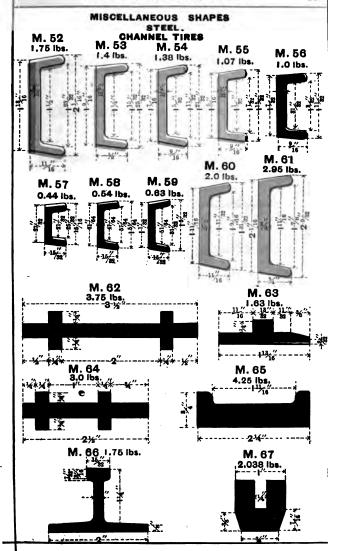
M. 13

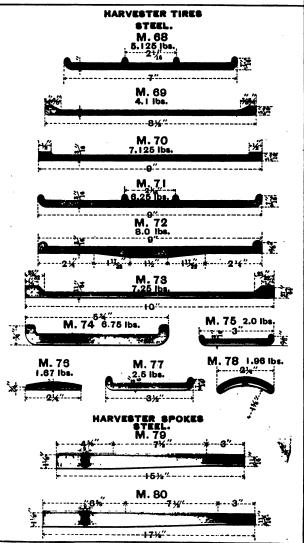
----3---

M. 16 M. 18 6.25 lbs -214" ----1956

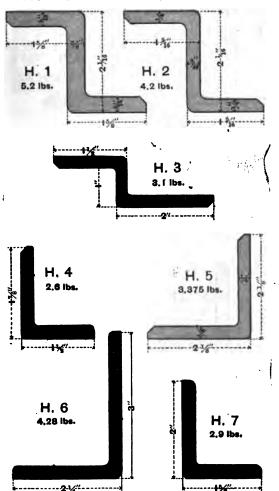
# MISCELLANEOUS SHAPES. STEEL. SCREEN BARS. M. 22 M. 23 M. 24 M. 25 16 -- 46.1 -14" 2.75 lbs. M. 26 M. 28 M. 27 18" ICE SLIDE. M. 29 .75 lbs 1.25 lbs. -1%"-----M. 30 10.625 lbs. M. 31 M. 32 CULTIVATOR BEAM. 9.75 lbs. 12.5 lbs. M. 33 -1 9 16 -1362 PLOW HANDLES. M. 34 2.625 lbs M. 35 --11/4"---M. 38 M. 37 0.75 lbs.



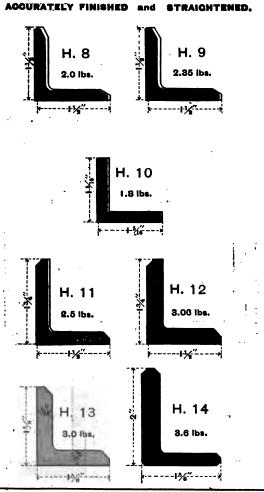




# COLD ROLLED. REAPER and HARVESTER FINGER BARS. ACCURATELY FINISHED and STRAIGHTENED.

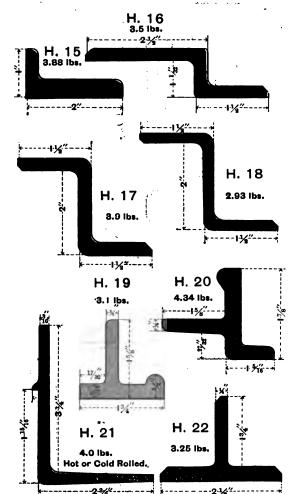


# COLD ROLLED. REAPER and HARVESTER FINGER BARS.

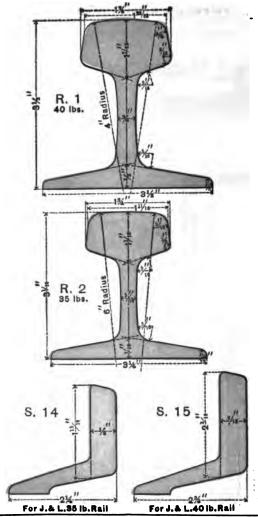


HOT ROLLED.

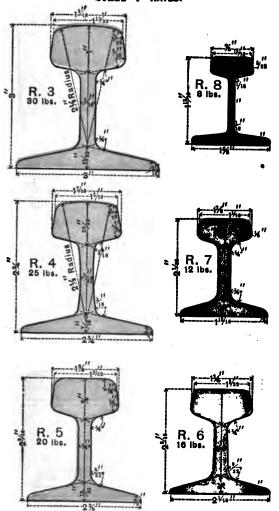
REAPER and HARVESTER FINGER BARS.



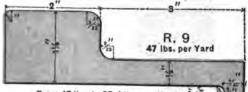




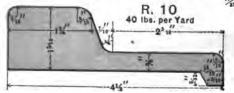
STEEL T RAILS.



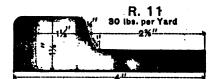
### STEEL STREET RAILS.



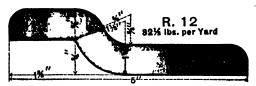
From 47 lbs. to 53.4 lbs. per Yard.



From 87 lbs. to 45% lbs. per Yard.



From 37 lbs. to 85 lbs. per Yard.

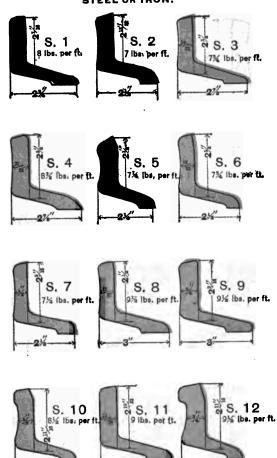


From 25.4 lbs. to 88 lbs. per Yard.

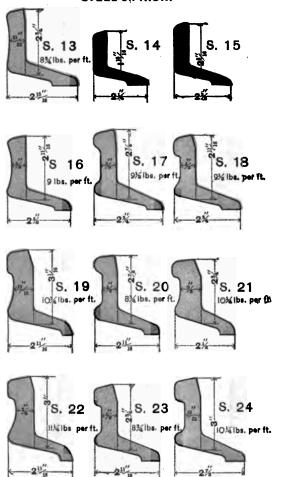


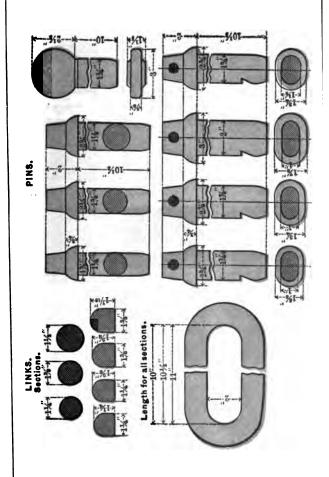
From 24% lbs. to 85 lbs. per Yard.

# ANGLE SPLICES. STEEL OR IRON.

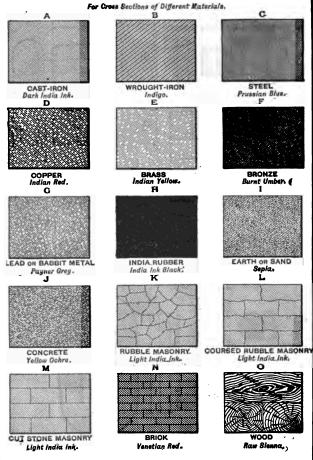


# ANGLE SPLICES. STEEL OR IRON.





# SYMBOLICAL SHADING AND COLORS.



# SIZES WE CAN ROLL.

	ROUNDS.		SQUA	RES.
DIAMETER. INCRES.	DIAMETER. Inches.	DIAMETER. Inches.	SIDE. Inches.	Side.
71	84	1,4	4	1
7 <del>1</del>	84	11	84	15
7	81	116	81	1
6 <del>7</del>	84	1	81	18
64	81	15	8	#
6 <del>§</del>	81	78	24	11
6 <del>1</del>	8	118	24	#
6 <del>8</del>	27	#	21	16
6 <del>1</del>	24	11	28	17
6 <del>1</del>	24	8	21	<b>1</b>
6	21/2	16	21	15
5 <del>7</del>	24	17	2	118
54	21	1 1	115	111
54	21	15	17	8
51	2	78	118	ii.
5 <del>8</del>	111	18	12	10
51	17	8	1111	8 8
5 <del>1</del>	1118	ii	14	ł
5	14	10	1 9	7.
47	111	No. 2	11	18
45	15	39	178	16
45	19	No. 8	18	
41	11	1 1	1 5 1 6	
48	176	No. 4	11	
41	18		13	
41	1.5.	375	118	
4	15	18	178	1
87	12	1	718	}

OVAL.

 $<sup>1\</sup>frac{1}{2}, 1\frac{1}{6}, 1\frac{1}{6}, \frac{1}{6}, \frac{5}{6}, \frac{5}{16}$ .

HALF OVAL.

 $<sup>2\</sup>frac{1}{2}$ , 2,  $1\frac{1}{2}$ ,  $1\frac{1}{2}$ ,  $1\frac{1}{2}$ ,  $1\frac{1}{2}$ ,  $1\frac{1}{2}$ ,  $\frac{1}{2}$ ,

 $<sup>2, 1\</sup>frac{8}{4}, 1\frac{1}{4}, 1\frac{1}{4}, 1\frac{1}{8}, 1, \frac{7}{8}, \frac{8}{4}, \frac{5}{8}, \frac{9}{16}, \frac{1}{2}, \frac{7}{16}, \frac{8}{8}, \frac{5}{16}.$ 

## SIZES WE CAN ROLL.

### FLATS.

22½ × ½ to ½.

14, 12, 10, 9, 8½, 8,

7½, 7½, 7½, 7, 6½, 6½, 6½,

6, 5½, 5½, 5½, 5, 4½, 4½,

4, 8½, 8½, 8½, 8½, 8½, 8½, 8,

2½, 2½, 2, 1½, 1½ and 1½ × ½ to 1½.

1½, 1½, 1½ and 1½ × ½ to 1½.

1½, 1½, 1½ and 1½ × ½ to 1½.

1½, 1½ and 1 × ½ to ½.

½ and ½ × ½ to ½.

¾ and ½ × ½ to ½.

# δ Χ ξ to ξ. ἐ Χ ξ to ξ.

 $221 \times 1$ .

# HOOPS AND SANDS.

× No. 11 to No. 4.

6\(\frac{1}{2}\), 6\(\frac{1}{2}\), 5\(\frac{1}{2}\), 5\(\frac{1}{2}\), 5\(\frac{1}{2}\), 5\(\frac{1}{2}\), 5\(\frac{1}{2}\), 5\(\frac{1}{2}\), 5\(\frac{1}{2}\), 5\(\frac{1}{2}\), 3\(\frac{1}{2}\), 3\(\frac{1}{2}\), 3\(\frac{1}{2}\), 3\(\frac{1}{2}\), 2\(\frac{1}{2}\), 2\(\frac{1}{2}\), 2\(\frac{1}{2}\), 2\(\frac{1}{2}\), 2\(\frac{1}{2}\), 2\(\frac{1}{2}\), 2\(\frac{1}{2}\), 2\(\frac{1}{2}\), 3\(\frac{1}{2}\), 3\(\frac{1}\), 3\(\frac{1}{2}\), 3\(\frac{1}2\), 3\(\frac{1}2\), 3\(\frac{1}2\), 3\(\frac{1}2\), 3\(\frac{1}2\), 3\(\frac{1}2\), 3\(\frac{

10, 9, 81, 8, 72, 71, 7,

18,  $1_{16}^{*}$ ,  $1_{26}^{*}$  and  $1_{16}^{*}$  × No. 18 to  $\frac{1}{2}$ .

18,  $1_{16}^{*}$ ,  $1_{2}^{*}$  and  $1_{16}^{*}$  × No. 20 to  $\frac{1}{2}$ .

18,  $1_{16}^{*}$ ,  $1_{26}^{*}$  and  $\frac{1}{2}^{*}$  × No. 20 to  $\frac{1}{2}$ .  $\frac{1}{6}$  and  $\frac{1}{2}^{*}$  × No. 21 to  $\frac{1}{2}$ .

2,  $\frac{1}{4}$  and  $\frac{1}{8}$  × No. 22 to  $\frac{1}{4}$ .

\$ × No. 17 to 1.

 $\frac{1}{4}$  and  $\frac{1}{4} \times \text{No. 23 to } \frac{1}{4}$ .

# SHEET STEEL.

(Partridge Gauge.)

# MADE ON CHILL ROLLS.

Thickness.	Width.	Maximum Length.
No. 30 29 28	18" to 30" 18" to 30" 18" to 30"	8 "
No. 27 } 26 }	18" to 80"	9 feet.
No. 24}	18" to 30"	10 feet.
No. 22 21 20	18" to 36"	10 feet.
No. 19}	18" to 36"	10 feet.
No. 17	18" to 36"	10 feet.
No. 16}	18" to 42"	10 feet.
No. 14}	18" to 36" 87" to 42"	
No. 12 11 10 9	18" to 36" 37" to 42"	

### PLATE STEEL.

### MADE ON CHILL ROLLS.

Thickness. Inches.	Width. L	exi'm ength Feet.	Thickness. Inches.		axi'm ength Feet.
37 40	(24 to 80	12		24 to 30	28
No. 16	81 to 86	10 8	No. 8	31 to 36 37 to 42	20 16
	24 to 30	14		("" " ==	
No. 14	{ 81 to 86	10		24 to 30	30
	(87 to 42	8	No. 7 or 👫 -	31 to 36	22
NT. 44 8 40	(24 to 30	18	2.00 1 02 16	37 to 42	18
No. 11 & 12	31 to 86	15 12		24 to 30	26
	(37 to 42 (24 to 30	24		81 to 86	20
No. 10	31 to 86	18	7 & 1 ·	37 to 42	<b>16</b>
210. 20	87 to 42	14			
	24 to 80	26	1	20 to 24	25
No. 9	31 to 86	20	<u>.</u>	25 to 30	20
110. 8	37 to 42	18	16 ·	31 to 36	16
	l	ı		( 87 to 42	12

# PLATE STEEL. MADE ON SAND ROLLS.

#### Width. Maxi'm Inches. Length Width. Maxi'm Inches. Length Feet. Thickness. Thickness. Inches. Inches. 31 to 36 44 to 48 18 11 - & ± 37 to 42 49 to 52 9 16 43 to 52 8 44 to 48 16 ₩. 14 18 to 20 16 49 to 52 20 to 24 14 20 to 24 25 20 25 to 30 11 25 to 30 17 31 to 36 9 31 to 36 37 to 42 15 37 to 42 43 to 48 13 43 to 52 7 11 18 to 20 14 49 to 52 20 21 to 24 12 20 to 24 9 25 to 30 16 25 to 30 31 to 36 8 31 to 36 13 37 to 42 12 18 to 20 12 21 to 24 10 43 to 48 10 1 25 to 30 8 49 to 52 9 81 to 86 16 20 to 24 25 to 80 13

# ELEMENTS OF STANDARD STEEL BEAMS.



d Ins	Weight per foot.	b Ins.	t Ins.	8 Ins	a Ins	Size of holes.	d Ins	Weight per foot.	b Ins.	t 'Ins.	s Ins.	a. Ins	Size of holes.
20	100 95 90 85 80	7.220 7.147 7.073	0.894 0.820 0.747 0.678 0.600	0.65	4	13''	10		4.807	0.751 0.604 0.457 0.810	0.31	25	18"
20	80 75 70 64	6.485 6.412	0.785	0.55	31	18"	9	25 21 ——	4.624 4.461 4.880	0.747 0.584 0.421 0.290	0.29	21	18"
15	100 95 90 85	6.694 6.596 6.498	0.898	0.80	32	18"	8	22.75 20.25 17.75	4.181 4.09 4.00	0.542 0.451 0.360 0.270	0.27	21	1 h"
15	80 75 70 65	6.294 6.196 6.008	0.800 0.982 0.884 0.786 0.688 0.590	0.59	32 31 31 31 31 31	18"	7 6	17.5 15 17.25 14.75	3.87 8.765 8.66 	0.250 0.475 0.358	0.25	-	18"
15	60 55 50 45	5.853 5.754 5.656	0.763 0.664 0.566 0.468	0.41	31 3 8 3	18"	5	14.75 12.25 9.75	8.294 3.147 3.000	0.504 0.357 0.210	0.21	12	18"
12	55 50 45	5.618 5.496 5.373	0.410 0.828 0.706 0.583	0.46	3	13"	4	9.5 8.5 7.5	2.806 2.733 2.660	0.190	0.19	11	18"
12	40 40 35 31.5	5.208	0.460 0 558 0.436 0.35		3 21 21	13"	3	6.5	2.526 2.428 2.330	0.268	0.17	176	78"

# ELEMENTS OF STANDARD STEEL CHANNELS.



d Ins	Weight per foot,	b Ins.	t Ins.	8 Ins	a Ins	Size of holes.	d Ins	Weight per foot.	b Ins.	t Ins,	s Ins	a Ins	Size of holes.
15	55 50 45 40 85 33	3.783 3.638 3.538 3.440	0.831 0.733 0.636 0.538 0.440 6.400		21-14-14-14-14-14-14-14-14-14-14-14-14-14	12"	7	17.25 14.75 12.25	2.510 2.405 2.300 2.195 2.000	0.525 $0.420$ $0.315$	-	11 11 11 11 11 11	13"
12	40 35 30 25 20.5	3,290 3,170 3,050	0.758 0.636 0.513 0.390 0.280	0.28	2 2 12 12	13"	6	13.00	2.288 2.166 2.043 1.920	0.446 $0.323$	0.20	13 13 13 14 14	110
10	35 30 25 20 15	3.041 2.894 2.747	0.828 0.681 0.534 0.378 0.240	200	2 2 2 11 11	13"	5	9.00	2.044 1.897 1.750	0.337		11 11 1	20'
9	25 20 15 13 . 25	2.651	0.614 0.451 0.288 0.230	0.25	15 15 15 18 18	12"	4	7 25 6 25 5 25	1.727 1.654 1.580	0.327 0.254 0.180	0.18	1	W.
8	18.75 16.25 13.75	2.586 2.444 2.352	0.588 0.496 0.404 0.312 0.220	0.92	110 101 101 141 141	13"	3	5.00	1.606 1.508 1.410	0.268	0.17	18	ra'

WEIGHTS AND DIMENSIONS OF Jones & Laughlins, Limited, Tees.

TEES.

Section	Size in	Inches.	Thickness	of Metal.	Weight	
Number	Flange	Stem.	Flange.	Stem.	Foot.	
T 20 T 21 T 22 T 1	4 in. 4 " 4 " 4 "	5 in. 42 " 41 " 4	in. to in.	in. to § in.	16.00 15.50 15.00 14.00	
T 2 T 3 T 4 T 23	4 " 8½ " 8½ " 8½ "	4 " 3½ " 3½ " 3 "	7 " " 17 " 16 " 38 " 16 " 3 " " 16 " 7 " " 8 " 16 " 7 " 7 " " 16 " 3 "	7 " " 17 " 16 " 18 " 1 " 1 " 1 " 1 " 1 " 1 " 1 " 1 "	12.00 10.40 9.30 9.80	
T 24 T 26 T 25 T 5	81 " 8 " 8 " 8 "	8 " 81 " 81 " 3 "	8 " " 7 " 7 " " 1 " " 1 " " 1 " 1 " 1 " 1 " 1 " 1	8 " " 7 " 16 " 18 " 18 " 18 " 18 " 18 " 18 " 18	9.00 9.00 8.50 7.85	
T 6 T 7 T 8 T 28	3 " 2½ " 2½ " 2½ "	8 " 21 " 21 " 2 "	5 8 16 7 5 16 16 8 6 8 16 8	5 " " 2 " " 15 " 15 " 15 " 15 " 15 " 15	6.60 6.32 5.40 4.80	
T 9 T 10 T 11 T 27	21 " 21 " 21 " 21 "	21 " 21 " 2 " 1‡ "	E (1 (1 11 (1 12 12 12 12 12 12 12 12 12 12 12 12 12	8 " " 11 " 16 " 88 " 16 " 16 " 88 " " 16 " 16	4.69 4.19 3.50 3.90	
T 18 T 12 T 14 T 15	18 " 18 " 11 " 11 "	18 " 18 " 19 " 11 "	1 44 44 54 44 54 54 54 54 54 54 54 54 54	1	3.00 2.88 2.62 1.90	
T 16 T 17 T 18 T 19	1½ " 1½ " 1 " 1 "	1½ " 1½ " 1 "	1 " " 3 " " 1 " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " " 1 " 1 " " 1 " " 1 " " 1 " 1 " " 1 "	1 " " 9 " " 15 "	1.98 1.58 1.28 0.90	

# JONES & LAUGHLINS, LIMITED, STANDARD ANGLES.

Weights per foot, corresponding to thickness varying by 1 inch.

# EQUAL LEGS.

Size in. Inches.	½6 ————————————————————————————————————	18	14	Ýв	%	18	1/2	18	5∕8	ii	%	13	<b>%</b>
6 x 6						17.2	19.6	21.9	24.2	26.4	28.7	30.9	33.1
4 x 4	<u>, 3</u>	<u>,                                    </u>		8.2	9.7	11.2	12.8	14.2	15.7	17.1	18.5		
3½ x 3⅓	3	7	5.7	7 1	8.5	9.8	11.1	12.3	13.5				
3 x 3	2.6		4.9	6.0	7.2	8.3	9.4	10.4	11.4				
2½ x 2½	2.1		4.0	5.0	5.9	6.8	7.7	<b> </b>			· • · ·		
2 x 2	1.7	2.4	3.2	3.9	4.6	5.3							
1% x 1%	1.4	2.1	2.8	3.4	4.0	4.6							
1½ x 1½	1.2	1.8	2.3	2.9	3.3		• • • •						
1¼ x 1¼	1.0	1.5	1.9							••••	<b> </b> .		•••
1 x 1	0.8	1.2						<b> </b>			···	·	
% x %	0.6	.8											

### UNEQUAL LEGS.

	ize in iches.	3/8	16	34	16	96	176	1/6	16	5/8	11	34	18	%
6	x 4					12.3	14.2	16.2	18.1	19.9	21.8	23.6	25.4	27.1
6	x 3½	7114		****	+++	11.6	13.5	15.3	17.1	18.9	20.6	22.3	24.0	25.7
5	x 314					10.4	12.0	13.6	15.2	16.7	18.3	19.8		
5	x 3	++++	50	* ++	8.2	9.7	11.2	12.8	14.2	15.7	17.1	18.5		
4	ж 3				7.1	8.5	9.8	11.1	12.3	13.5	14.8	15.9		
31/4	х 3				6.6	7.8	9.0	10.2	11.4	12.5				
31/2	x 21/2		1 ex-	4.9	6.0	7.2	8.3	9.4	10.5			.,		
3	x 21/2	ele:	****	4.5	5.5	6.5	7.5	8.5				4441		
214	x 2		2.8	3.6	4.5	5.3	6.0	6.8		1453	222			100

# SPECIAL SECTIONS OF STEEL ANGLES.

Weights per foot, corresponding to thickness varying by 18 inch.

### EQUAL LEGS.

Sizes, Inches.	34	16	34	1.6	96	176	1/2	16	5%	11	*	13	76
5 x 5	3	2			12.3	14.2	16.2	18.1	19.9	21.8	23.6	25.4	27.1
3¼ x 3¼	3	4	1.54.5		7.8	9.0	10.2	11,4	12.5	13.6	14.7		
2% x 2%	2.4		4.5	5.5	6.5	7.5	8.5						
214 x 214			3.6	4.5	5.3	6.0	6.8	.5.5					

### UNEQUAL LEGS.

	Sizes, aches.	1/8	18	*	18	%	178	1/2	18	<del>5</del> ⁄8	11	<b>¾</b>	13	ж
5	<b>x</b> 4	] <u>,</u>	ļ	<b> </b>	ļ	11.0	12.8	14.5	16.1	17.8	19.4	21.0	22.6	24.2
4	x 81/2					9.1	10.5	11.9	13.3	14.6	15.9	17.2		
3¾	<b>x</b> 25/8				6.4	7.7	8.8	10.0	11.1	12.2	13.3	14.3		
3¼	x 2			4.3	5.3	6.2	7.2	8.1						
3	x 2		3.1	4.0	5.0	5.9	6.8	7.7						
2½	x 1%		2.6											
21/2	x 1½		2.4	3.2	3.9	4.6	5.3	6.0						. <b>.</b>
2	x 1½		2.1	2.8	3.4	4.0								ļ
2	x 1%		2.0	2.7	3.3	3.8					•••			
1%	x 1½			2.6										
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# JONES & LAUGHLINS, LIMITED.\_

# CAST SEPARATORS FOR

Separators for 90" beams are made of %" metal.
" 6" to 15" beams are made of %"

" 5" beams and under are made of %" metal.

DESIGNATION OF BEAM.			DISTANCES.		Bolts.			Weights.				
Depth.	No. of Shape.	Weight.	Out to out of flanges of beams.	Center to center of beams.	Size.	Distance, center to center.	Length.	Bolts and nuts.	Increase in weight f separator bolts for I inch additional spread of beams.	Separator.	Increase in weight of separator for 1 inch additional spread of peams.	
in.		lbs.	in.	in.	in.	in.	in.	l bs.	lbs.	lbs.	lbs.	
SEPARATORS WITH TWO BOLTS.												
20 20	B-1 B-2	80 64	143 131	77	7 8 7 8	10 10	91 81	41	0.33 0.33	243 22	315 316	
15 15 15	B-3 B-3 B-4	80 60 42	135 121 111	61 6 6	ajesjesje	7 7 7	9 8 71	3 <u>1</u> 3 <u>1</u> 3	$\begin{array}{c} 0.25 \\ 0.25 \\ 0.25 \end{array}$	18 <u>1</u> 12 <u>1</u> 11 <u>1</u>	12 12 14 14	
12 12	B-5 B-6	40 81‡	11 10 <del>1</del>	5 <del>3</del> 5 <del>3</del>	848	61 61	71 71	8	0.25 0.25	9 <del>1</del> 9 <del>1</del>	17° 11°	
SEPARATORS WITH ONE BOLT.												
12 12	B- 5 B- 6		11 10 <del>3</del>	5 <del>2</del> 5 <del>2</del>	8484	<b> </b> :::	71 78	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.12	9 <u>1</u>	116	
10 10	B- 7 B- 7		11 10‡	6 5½	8 4 3 4		7 <del>1</del> 67	18 18	0.12 0.12	7 71	118	
9	B- 8 B- 8	35 21	10 <u>1</u> 98	5½ 5	8 4 3 4		71 61	1 8 1 8	0.12 0.12	61 6	1 1 8 1 8	
8	B- 9 B- 9		9 <u>1</u> 8‡	5 43	8 4 8 4		6	18 18	0.12 0.12	51 51	15 15	
7 7	B-10 B-10		8 <del>§</del> 81	41/2 5	8484		6 <del>1</del>	1 <del>1</del> 1 <del>1</del>	0.12 0.12	41 41	18 18	
6 6	B-11 B-11	17 <u>1</u> 12 <u>1</u>	71 71 71	4 33	8 4 8 4		5 <del>1</del> 5	1 <del>1</del> 1 <del>1</del>	0.12 0.12	2 <del>1</del> 2 <del>1</del>	1 16	
5 5	B-12 B-12	143 94	7 61	3 <del>3</del> 3 <del>1</del>	848		5 <del>1</del> 4 <del>2</del>	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.12 .0.12	1 <del>3</del> 1 <del>3</del>	178 176	
4	B-18	71	57	31	2	<b></b>	41	11	0.12	11	- <del>3</del>	
8	B-14	51	51	3	1	l	41	1 3	0.12	11	1	

## STANDARD SPACING AND DIMENSIONS OF RIVET AND BOLT HOLES THROUGH FLANGES OF BEAMS AND CHANNELS AND CONNECTION ANGLES.

										<u>1</u> 3			
	STEEL BEAMS.					STEEL CHANNELS.					ANGLES.		
Depth in inches.	Weight per foot. Lbs.	Diameter of Bolt or Rivet. Inches.	Inches.	Inches. W	Depth in inches.	Weight per foot. Lbs.	Diameter of Bolt or Rivet. Inches.	Inches.	Inches. W	Depth of Leg. Inches.	Max. Diam. of Bolt or Rivet. Inches.	Inches.	
20 20 15 15 15 12 12 10 9 8 7 6 5 4	80 64 80 60 42 40 31.5 25 21 17.75 15 12.25 9.75 7.5 5.5	esterate esteratement esterate ester ester ester ester ester ester ester ester ester esterate	4 1 1 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5 5 5 4 5 5 4 5 5 4 5 5 4 5 5 4 5 5 4 5 5 4 5 5 4 5 5 4 5 5 4 5	12 12 10 10 9 9 8 8 7 7 6 6 6 5 5	11.25 17.25 9.75 13 8 11.5 6.5	edesde edesde edesde edesde edesde edesde odoodo -for-fo	21 2 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	45 4 15 4 15 4 1 1 1 1 1 1 1 1 1 1 1 1 1	6 5 4 3\frac{1}{4} 8 2\frac{1}{4} 2 1\frac{1}{4} 2 1\frac{1}{4} 1	1 1 1 1 7 10 7 10 8 14 8 14 8 14 8 10 8 10 10 10 10 10	8 1 2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
• • •	<u>-</u>				3	5.25 4	1 3 3 8	1 15	$\frac{4\frac{8}{16}}{4\frac{8}{16}}$	84		7	

The spaces "B" correspond with spacing given on page 62 for Standard Connection Angles.

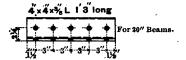
# NOTES ON STANDARD CONNECTION ANGLES FOR JONES & LAUGHLINS, LIMITED, BEAMS.

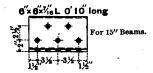
The Standard Connection Angles for Jones & Laughlins, Limited, Steel Beams, illustrated on opposite page, are designed for an allowed shearing strain of 10,000 pounds per square inch, and a bearing strain of 20,000 pounds per square inch on rivets or bolts corresponding with an extreme fibre strain of 16,000 pounds per square inch in the beam. The minimum span length at and above which the standard connections can be used with safety (the beam being loaded with its full capacity) are shown in the tables below. For shorter spans (the beam being loaded with its full capacity) additional strength in the connection should be made.

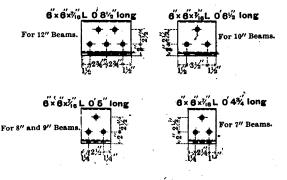
TABLE OF MINIMUM SPANS FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS FOR WHICH STANDARD CONNECTION ANGLES MAY BE SAFELY USED WITH BEAMS LOADED TO THEIR FULL CAPACITY.

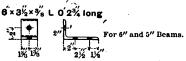
Section No.	Size of Beam.	Weight per foot.	Minimum Safe Span in feet.	Section No.	Size of Beam.	Weight per foot.	Minimum Safe Span in feet.	
B8	15 in.	80	12.6	В 9	8 in.	251	7.6	
B 8	15 "	70	12.0	В 9	8 "	17#	7.0	
B 4	15 "	60	11.6	B 10	7 "	20	6.0	
B 4	15 "	50	11.0	B 10	7 "	15	5.6	
B 4	15 "	42	10.6	B 11	6 · "	171	6.6	
B5	12 "	40	8.6	B 11	6 "	121	6.0	
B6	12 "	311	7.6	B 12	5 "	148	4.0	
B7	10 "	35	10.6	B 12	5 "	9‡	4.0	
B7	10 "	25	9.0	B 13	4 "	101	8.0	
В8	9 "	25	9.6	B 18	4 "	71	8.0	
В8	9"	21	8.6	<b> </b>		•••••		

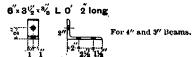
# STANDARD CONNECTION ANGLES FOR STEEL BEAMS.





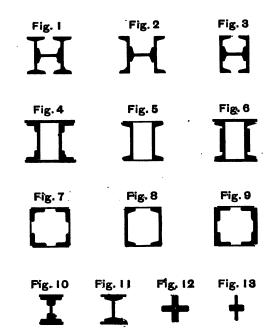




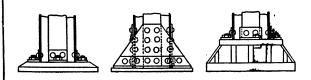


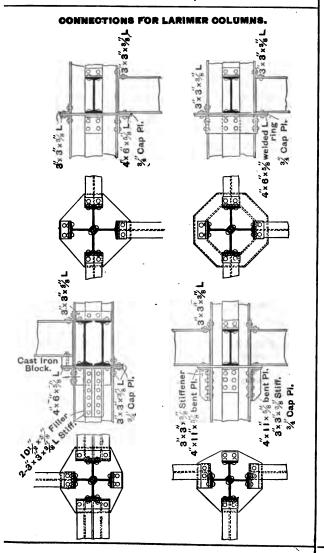
All holes for ¾" bolts or rivets.

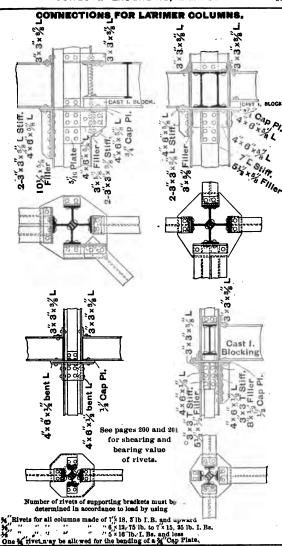
# BUILT COLUMN SECTIONS. Light lines indicate lattice.



# DETAILS OF BASES FOR LARIMER COLUMNS.

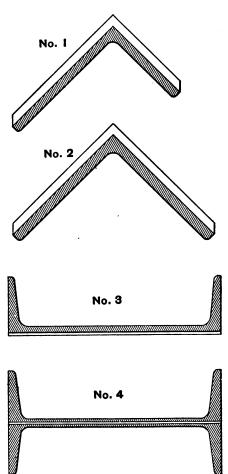




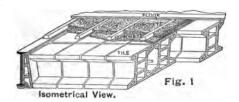


### METHOD OF INCREASING SECTIONAL AREAS.

Dark portions represent the minimum sections, and the blank portions the added areas.



#### FIRE PROOF FLOORS.



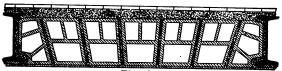
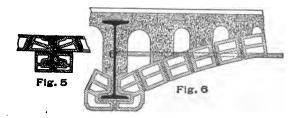
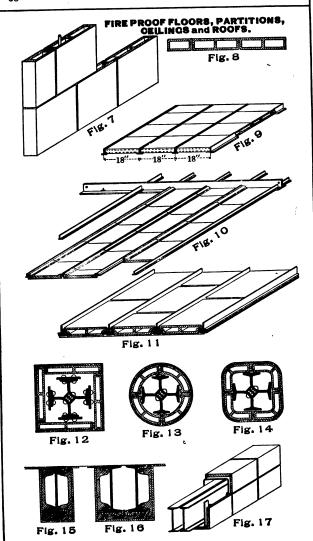


Fig. 2

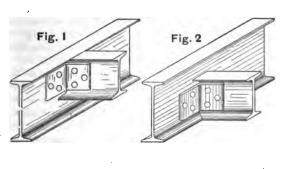


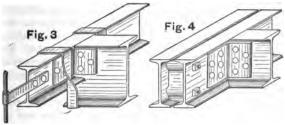






### CENERAL DETAILS OF FLOORS AND CONNECTIONS.









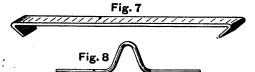


Fig. 9

formed between the flanges, without necessitating the cutting of longitudinal webs, usual in the less modern form of arch shown in Fig. 2. Floor arches are generally designed to fill the space between the beams to within one inch of the top, and are set one inch below the soffits, thus allowing the bottom flange of the beam to be protected from fire by a "beam tile" one inch thick, held securely in place by the V-shaped projection of the "abutment" tile on each side of the beam. The "end section" arch is made for any sized beam up to 15-inch. Should a 20-inch beam be used, the abutment pieces are formed to suit the flange of the beam, and the 6-inch space from the top of the arch to the top of the 20-inch beam is then filled in with a light hollow flat filling tile. It is difficult to determine the most economical depth of beam for floor construction unless all the data of the existing conditions be at hand. With the floor arch filling, however, it is generally accepted that from 9-inch to 15-inch deep beams give the best results. The span of the floor arches necessarily vary according to the framing of the steel work. It is not uncommon in practice where the "end section" arch is used to set the same in place between beams spaced 10' 0" from center to center, though this span should be accepted as the maximum for arches 12 inches in depth or more only.

A great many tests have been made as to strength of hollow tile arches, both by still load and falling of heavy weights, and in every case the "end section" method has demonstrated its greater efficiency over the older systems. The usual manner of setting tile arches is by the use of portable scaffolds formed of 2×10 plank, supported underneath by "center stringers," which in turn are carried by bolts attached to cross pieces resting on the tops of the beams. After the tile arches have been set in cement mortar for thirty-six hours, the center scaffolding is removed and the tops of the arches are then filled in with cement concrete to the required level, 2×4 wooden sleepers being bedded in the concrete to afford nailing surface for the wood flooring; or if marble or mosaic flooring is required, the wood strips are omitted.

Fig. 2 illustrates an average of the old style method of floor arch construction. This system has been extensively used, and with generally satisfactory results. Its application is identical with the description given for Fig. 1, but as the hollows in all the tiles forming the arch run parallel with the beams, not over twenty-five per cent. of the sectional area of each tile is in compression. Hence, to obtain the required strength for the loads imposed, it is necessary to increase the thickness of the web and shell of the tile, thus increasing its weight. A comprehensive example of the relative strength of the "end system," as compared with the older methods, would be clearly illustrated by applying a pressure upon an egg endwise or upon its sides.

Table of weights, etc., for various sizes of Fireproof

Depth of Arch.	Description.	Maximum Safe Span.	Weight per Square Foot.	
7-inch.	Standard.	5′ 0′′	25 pounds.	
8-inch.	"	5' 6"	29 ' ''	
9-inch.	End Section.	7' 0"	25 "	
12-inch.	66 66	10' 0''	35 "	
15-inch.	"	11' 0''	45 "	
5-inch.	Segment.	16' 0"	28 "	
6-inch.		20' 0''	35 "	

The weights given above do not include the concrete filling on top of arches. The safe span given for segment arches contemplates a rise of not less than 1; inch to the foot run. Should a greater rise be permissable the span could be increased proportionately.

Fig. 3 illustrates a hollow tile arch between beams with a segment soffit and flat top. This form of arch has been extensively used in breweries, warehouses, etc., where the necessity for a level ceiling did not exist.

Fig. 4 represents a segment hollow tile arch set in place between beams spaced 18 feet from center to center. The tiles forming this arch are 6"×6" square with outside shell 4-inch thick, and center web 4-inch thick. This form of

arch costs less than the flat systems shown in Figs. 1 and 2, effecting as it does a considerable saving in steel beams. Its use is becoming general for warehouses, malt houses and also office structures, although great care is necessary in the arrangement of steel framing to anticipate the thrust by the proper distribution of tie rods.

Fig. 6 shows in detail the abutment piece completely inclosing the steel beam, also the concrete filling in haunches cored out with metallic cores to lighten the weight of the floor; the wood strips are shown embedded in the concrete, same as described above.

Segment arches the sizes described have been built of 6-inch tile with a span of 18 feet, having 14 inches rise in the center, and tested to carry 300 pounds per foot, with factor of six for safety. Segment arches of 5-inch and 4-inch thick tile are used for smaller spans, and effect considerable saving when a level ceiling is not essential.

Fig. 5 shows method of fire proofing a beam or girder built in a floor that projects below the ceiling line. When desired special formed tile can be made to suit the outline required for ornamental cornices, etc.

On page 68, Figs. 15, 16 and 17 illustrate single and double isolated steel girders inclosed with fire proofing material, and finished out to the plaster line. On same page, Fig. 9 illustrates method of constructing mansard or flat fireproof roofs. For this purpose tees of the required weight are used, spaced 18 inches from center to center. Between the tees hollow tiles 12"×18" are bedded in cement mortar and left ready for the weathering. On steep pitched and mansard roofs the porous tiles are preferable, as the the slates or roofing tiles can be nailed directly to the same. Fig. 10 illustrates a fireproof ceiling constructed by a combination of steel and tile. The main supports are constructed of 8×3 angles spaced six feet from center to center, punched at regular intervals of 12-inch centers, with triangular holes of sufficient size to permit 1"×1" tees passing through the same. 8×3 angles are supported by rods of the required length from the roof rafters at intervals of 8 feet. After the 1"×1" tees are set in place, 1-inch thick flat tiles with grooved edges are set in place between same and the under surface left ready for the receipt of the plaster. This form of fireproof ceiling is sufficiently strong to bear the weight of a man, but should not be used if required to carry anything but its own weight.

Fig. 11 shows tees and tile construction suited for ceilings or attic floors of fireproof buildings. The tees are spaced 16 inches from center to center, 3-inch thick tiles being bedded between same; the soffits of the tees are protected with a slab of tile. A thin coat of cement mortar spread upon the tops of the tile leaves a finished surface suitable for attic floor. Figs. 12, 13 and 14 illustrate three different forms of fireproof covering applied to Larimer's Patent Steel Columns. These tiles are molded to suit any size or form of column, and are secured to each other with steel clamps, and to the column with suitable fastenings. Any form of steel column can be fireproofed in a like manner.

By fireproofing the Larimer column as shown, a channel or duct between the column and tile is formed, thus allowing ample space for all pipes, etc., to be carried up through the building without increasing the exterior dimensions of the column.

Figs. 7 and 8 show an isometrical view and plan of hollow tile partition. These tiles are manufactured from 2 to 6 inches thick, and are 12 inches square. They are laid in place in cement mortar, joints being regularly broken in every course. Steel clamps are used to tie the tiles together whenever the walls are of unusual heights.

### DEFLECTION COEFFICIENTS FOR DIFFERENT SHAPES GIVEN IN 64THS OF AN INCH.

Coeffi	DISTANCE BETWEEN SUPPORTS IN FEET,											
cient Index.	6	8	10	12	14	16	18	20	22			
Ç	<b>38</b> .0 <b>30</b> .0	68.0 58.0	106.0 88.0	152.5 119.0	208.0 102.0	271.0 212.0	843.0 268.0	424.0 831.0	518.0 400.5			
		D	istanci	BETW	BEN SU	PPORTS	IN FE	ET.	<u> </u>			
	24	26	28	30	32	34	36	38	40			
Ç,	610.0 477.0		880.5 642.0	958.0 748.0	1085.0 847.0							

The figures given opposite C and C' are the Deflection Coefficients for steel shapes subject to transverse strain for varying spans, under their maximum uniformly distributed safe loads, derived from a fiber strain of 16,000 and 12,500 respectively, the modulus of elasticity being taken at 29,000,000.

To find the deflection of any symmetrical shape used as a beam, under its corresponding safe load, divide the coefficients given in the above tables by the depth of the beam. This applies to such shapes as beams, channels, etc. For those shapes having unsymmetrical axes, such as tees, angles, etc., divide by twice the greatest distance of the neutral axis from the outside fiber.

Example:—Required the deflection of a 10-inch beam, 25 lbs. per foot, 20-foot span, under its maximum uniformly distributed safe load of 6.51 tons as given on page 84. The above tables give 424.0 as the deflection coefficient; dividing this by 10 gives 42 as the required deflection in 64ths of an inch. For deflections due to different systems of loading, see page 177.

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS. IN TONS OF 2,000 LBS.

in feet supports.		24 Inch Bram, Standard.								
Distance in feet	100	95	90	85	80					
between supports.	lbs.	lbs.	lbs.	1bs.	lbs.					
10	105.82	102.18	99.04	95.90	92.76					
11	95.74	92.89	90.04	87.18	84.33					
12	87.76	85.15	82.53	79.92	77.30					
18	81.01	78.60	76.18	78.77	71.36					
14	75.28	72.99	70.74	68.50	66.26					
15	70.21	68.12	66.03	68.93	61.84					
16	65.82	63.86	61.90	59.90	57.97					
17	61.95	60.10	58.26	56.41	54.57					
18	58.51	56.76	55.02	53.28	51.53					
19	55.42	53.78	52.13	50.47	48.82					
20	52.66	51.09	49.52	47.95	46.38					
21	50.15	48.66	47.16	45.67	44.17					
22	47.87	46.44	45.02	43.59	42.16					
23	45.79	44.43	43.06	41.69	40.33					
24	43.88	42.57	41.27	39.96	38.65					
25	42.13	40.87	39.62	88.36	37.11					
26	40.51	39.30	38.09	36.88	35.68					
27	39.01	37.84	36.68	35.52	34.36					
28	87.61	36.49	35.37	34.25	33.13					
29	86.31	35.28	34.15	33.07	31.99					
30	35.11	34.06	33.01	31.97	30.92					
31	88.97	32.96	31.95	30.94	29.92					
32	82.91	31.93	30.95	29.97	28.98					
83	81.91	30.96	30.01	29.06	28.11					
84	80.98	30.05	29.13	28.20	27.28					
85	80.09	29.19	28.80	27.40	26.50					
86	29.25	28.38	27.51	26.64	25.76					

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS. IN TONS OF 2,000 LBS.

in feet supports.		20 Inch B	BAM, HEAVY	SECTION.	
Distance in feet	100	95	90	85	80
between supports.	lbs.	lbs.	lbs.	lbs.	lbs.
10	88.66	86.05	83.43	80.82	78.21
11	80.59	78.22	75.84	73.47	71.10
12	73.88	71.70	69.53	67.35	65.17
18	68.20	66.19	64.18	62.17	60.16
14	63.33	61.46	59.59	57.78	55.86
15	59.11	57.36	55.62	53.88	52.14
16	55.41	53.78	52.15	50.51	48.88
17	52.15	50.61	49.08	47.54	46.00
18	49.25	47.80	46.35	44.90	43.45
19	46.66	45.29	43.91	42.54	41.16
20	44.33	43.02	41.72	40.41	89.10
21	42.22	40.97	89.70	38.49	87.24
22	40.80	39.11	87.93	36.74	85.55
23	38.55	37.41	36.28	35.14	84.00
24	36.94	35.85	34.76	83.68	82.59
25	35.46	34.42	33.37	32.33	81.28
26	34.10	33.09	32.09	31.08	30.08
27	32.83	31.87	30.90	29.93	28.97
28	81.66	30.78	29.80	28.87	27.98
29	30.57	29.67	28.77	27.87	26.97
80	29.55	28.68	27.81	26.94	26.07
31	28.60	27.76	26.91	26.07	25.23
82	27.70	26.89	26.07	25.25	24.44
33	26.86	26.07	25.31	24.49	23.70
34	26.07	25.31	24.52	23.77	23.00
35	25.83	24.58	23.84	23.09	22.88
36	24.68	23.90	23.18	22.45	21.72

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS.

IN TONS OF 2,000 LBS.

in feet supports.		20 Inch Bram, Standard.									
Distance in feet between supports.	80 lbs.	75 lbs.	70 1bs.	65 lbs.	64 1bs.						
10 11	70.74 64.31	68.13 61.93	65.51 59.56	62.90 57.18	62.37 56.70						
12	58.95	56.82	54.59	52.41	51.98						
18	54.42	52.40	50.39	48.38	47.98						
14	50.53	48.66	46.79	44.93	44.55						
15	47.16	45.42	43.67	41.93	41.58						
16	44.21	42.58	40.94	39.31	38.98						
17	41.61	40.07	38.54	37.00	36.69						
18	39.30	37.85	36.40	34.94	34.65						
19	37.23	35.86	34.48	33.10	32.83						
20	35.37	34.06	32.76	31.45	31.19						
21	33.68	32.44	31.20	29.95	29.70						
22	32.15	80.97	29.78	28.59	28.35						
23	30.75	29.62	28.48	27.35	27.12						
24	29.47	28.41	27.29	26.21	25.99						
25	28.29	27.25	26.20	25.16	24.95						
26	27.21	26.20	25.19	24.19	23.99						
27	26.20	25.23	24.26	23.29	23.10						
28	25.26	24.83	23.45	22.46	22.28						
29	24.38	23.49	22.59	21.69	21.51						
30	23.58	22.71	21.83	20.97	20.79						
81	22.82	21.98	21.13	20.29	20.12						
82	22.11	21.29	20.47	19.66	19.49						
83	21.44	20.64	19.85	19.06	18.90						
84	20.81	20.04	19.27	18.50	18.35						
85	20.21	19.46	18.72	17.97	17.82						
<b>36</b>	19.65	18.94	18.20	17.47	17.88						

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS. IN TONS OF 2,000 LBS.

Distance in feet between supports.		15 INCH BEAM, HEAVY SECTION.									
Distance	100	95	90	85	80						
between	lbs.	1bs.	lbs.	lbs.	1bs.						
10	63.96	62.00	60.04	58.08	56.11						
11	58.14	56.86	54.58	52.80	51.01						
12	53.30	51.66	50.03	48.40	46.76						
13	49.20	47.69	46.18	44.67	43.17						
14	45.68	44.28	42.88	41.48	40.08						
15	42.64	41.33	40.02	38.72	87.41						
16	39.97	38.75	37.52	36.30	35.07						
17	87.62	36.47	35.32	84.16	33.01						
18	85.53	34.44	33.35	82.26	31.17						
19	33.66	32.63	31.60	30.57	29.52						
20	31.98	31.00	30.02	29.04	28.06						
21	80.45	29.52	28.59	27.66	26.78						
22	29.07	28.18	27.29	26.40	25.51						
23	27.81	26.96	26.10	25.25	24.40						
24	26.65	25.83	25.01	24.20	23.38						
25	25.58	24.80	24.01	28.28	22.45						
26	24.60	23.84	23.09	22.34	21.58						
27	23.69	22.96	22.24	21.51	20.78						
28	22.84	22.14	21.44	20.74	20.04						
29	22.05	21.38	20.70	20.03	19.85						
30	21.32	20.67	20.01	19.36	18.70						
31	20.63	20.00	19.37	18.73	18.10						
32	19.99	19.87	18.76	18.15	17.54						
33	19.38	18.79	18.19	17.60	17.00						
34	18.81	18.23	17.66	17.08	16.50						
35	18.27	17.71	17.15	16.59	16.08						
36	17.76	17.22	16.68	16.13	15.59						

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS.

IN TONS OF 2,000 LBS.

Distance in feet between supports.		15 Inch l	Bram, Light	r Section.	
Distance	90	75	70	65	60
between	lbs.	lbs.	lbs.	lbs.	lbs.
10	51.15	49.19	47.28	45.27	43.31
11	46.50	44.72	42.93	41.15	39.37
12	42.62	40.99	39.36	37.72	36.09
13	39.35	87.84	36.33	34.82	83.81
14	36.54	85.13	33.73	32.33	80.93
15	34.10	82.79	31.49	30.18	28.87
16	31.97	80.74	29.52	28.29	27.07
17	30.09	28.93	27.78	26.63	25.47
18	28.42	27.33	26.24	25.15	24.06
19	26.92	25.89	24.86	23.82	22.79
20	25.57	24.59	28.61	22.63	21.65
21	24.36	23.42	22.49	21.56	20.62
22	23.25	22.36	21.47	20.58	19.69
23	23.24	21.39	20.53	19.68	18.83
24	21.31	20.50	19.68	18.86	18.04
25 26	20.46	19.68	18.89	18.11	17.82 16.66
27 28	18.95 18.27	18.22 17.57 16.96	17.49 16.87	16.77 16.17 15.61	16.04 15.47
29 30 31 32	17.64 17.05 16.50 15.98	16.40 15.87 15.37	16.29 15.74 15.23 14.76	15.09 14.60 14.14	14.93 14.44 13.97 13.53
33	15.50	14.91	14.31	18.72	13.12
34	15.04	14.47	13.89	13.81	12.74
35	14.61	14.05	13.49	12.98	12.36
<b>8</b> 6	14.21	13.66	13.12	12.57	12.03

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS. IN TONB OF 2,000 LBS.

s in feet supports.	15 Inch Bran, Standard.								
Distance in feet	60	55	50	45	42				
between supports.	lbs.	1bs.	1bs.	lbs.	lbs.				
10	38.47	36.52	84.55	32.59	31.41				
11	34.97	33.19	31.41	29.63	28.56				
12	32.06	30.42	28.79	27.16	26.18				
13	29.59	28.08	26.58	25.07	24.16				
14	27.48	26.08	24.68	23.28	22.44				
15	25.65	24.34	23.03	21.73	20.94				
16	24.04	22.82	21.59	20.37	19.63				
17	22.63	21.49	20.32	19.17	18.48				
18	21.37	20.28	19.19	18.10	17.45				
19	20.25	19.21	18.18	17.15	16.53				
20	19.28	18.26	17.26	16.29	15.71				
21	18.32	17.38	16.45	15.52	14.96				
22	17.49	16.59	15.70	14.81	14.28				
23	16.73	15.87	15.02	14.17	13.66				
24	16.03	15.21	14.40	13.58	13.09				
25	15.39	14.60	13.82	13.04	12.56				
2 <b>6</b>	14.80	14.04	13.29	12.53	12.08				
27	14.24	13.52	12.80	12.07	11.63				
28	13.74	13.04	12.34	11.64	11.22				
29	13.26	12.59	11.91	11.24	10.83				
30	12.82	12.17	11.52	10.86	10.47				
31	12.41	11.78	11.14	10.51	10.18				
32	12.02	11.41	10.80	10.18	9.82				
33	11.66	11.06	10.47	9.88	9.52				
34	11.31	10.74	10.16	9.58	9.24				
35	10.99	10.43	9.87	9.31	8.97				
36	10.69	10.14	9.60	9.05	8.73				

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR .JONES & LAUGHLINS, LIMITED, STEEL BEAMS. IN TONS OF 2,000 LBS.

in feet upports.	1	12 Ince	BEAM, SECTION	i.	12 Inch Beam, Standard.			
Distance in feet between supports.	55 1bs.	50 lbs.	45 1bs,	40 lbs.	40 lbs.	35 lbs.	81½ lbs.	
10	28.61	27.04	25.48	28.91	21.85	20.28	19.18	
11	26.01	24.58	23.16	21.73	19.86	18.44	17.44	
12	23.84	22.54	21.23	19.92	18.21	16.90	15.99	
18	22.01	20.80	19.60	18.39	16.81	15.60	14.70	
14	20.44	19.32	18.20	17.08	15.62	14.49	18.70	
15	19.08	18.03	16.98	15.94	14.56	18.52	12.79	
16	17.88	16.90	15.92	14.94	13.66	12.68	11.99	
17	16.88	15.91	14.99	14.06	12.85	11.98	11.2	
<b>18</b>	15.90	15.02	14.15	13.28	12.14	11.27	10.6	
19	15.06	14.23	18.41	12.58	11.50	10.62	10.10	
20	14.81	18.52	12.74	11.95	10.93	10.14	9.5	
21	13.68	12.88	12.13	11.38	10.41	9.66	9.14	
22	13.01	12.29	11.58	10.87	9.93	9.22	8.7	
28	12.44	11.76	11.08	10.39	9.50	8.82	8.8	
24	11.92	11.27	10.61	9.96	9.10	8.45	7.9	
25	11.45	10.82	10.19	9.56	8.75	8.11	7.6	
26	11.01	10.40	9.80	9.19	8.40	7.80	7.8	
27	10.60	10.02	9.43	8.85	8.09	7.51	7.10	
<b>28</b>	10.22	9.66	9.10	8.54	7.81	7.24	6.8	
29	9.87	9.33	8.78	8.24	7.53	6.99	6.6	
30	9.54	9.01	8.48	7.97	7.28	6.76	6.39	
81	9.28	8.72	8.21	7.71	7.05	6.54	6.19	
82	8.94	8.45	7.96	7.47	6.83	6.34	5.99	
<b>3</b> 8	8.67	8.19	7.72	7.24	6.62	6.15	5.81	
84	8.42	7.95	7.49	7.03	6.43	5.97	5.64	
85	8.17	7.72	7.28	6.88	6.24	5.79	5.48	
86	7.95	7.51	7.08	6.64	6.07	5.63	5.8	

# SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS. IN TONS OF 2,000 LBS.

in feet supports.		10 Inch Stani			9 Inch Beam, Standard.				
Distance in feet between supports.	40	35	30	25	35	30	25	21	
	lbs.	lbs.							
10	16.94	15.64	14.83	13.02	18.35	12.18	11.00	10.06	
11	15.40	14.22	18.03	11.85	12.14	11.07	10.00	9.15	
12	14.12	13.08	11.94	10.85	11.12	10.15	9.17	8.89	
13	13.03	12.03	11.02	10.02	10.27	9.36	8.46	7.74	
14	12.10	11.17	10.24	9.30	9.58	8.70	7.86	7.19	
15	11.30	10.42	9.55	8.68	8.90	8.12	7.34	6.71	
16	10.59	9.77	8.96	8.14	8.34	7.61	6.88	6.29	
17 18 19 20	9.97 9.41 8.92 8.47	9.20 8.69 8.23 7.82	8.43 7.96 7.54 7.16	7.66 7.24 6.85 6.51	7.85 7.42 7.08 6.67	7.16 6.76 6.41 6.09	6.47 6.11 5.79 5.50	5.92 5.60	
21	8.07	7.45	6.82	6.20	6.36	5.80	5.24		
22	7.71	7.11	6.51	5.92	6.07	5.53	5.00		
23	7.37	6.80	6.23	5.66	5.80	5.29	4.78		
24	7.06	6.52	5.97	5.43	5.56	5.07	4.58		
25	6.78	6.25	5.73	5.21	5.34	4.87	4.40	4.02	
26	6.52	6.01	5.51	5.01	5.13	4.68	4.23	3.87	
27	6.27	5.79	5.31	4.82	4.94	4.51	4.07	3.78	
28	6.05	5.58	5.12	4.65	4.77	4.35	8.93	3.59	
29 80 31 82	5.88 5.65 5.46 5.29	5.21 5.04	4.94 4.77 4.62 4.48	4.49 4.34 4.20 4.07	4.60 4.45	4.20 4.06	3.79 3.67	3.47 3.35	
33 34 35 36	5.18 4.98 4.84 4.71	4.60	4.34 4.21 4.09 8.98	3.95 3.83 8.72 3.62					

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS.
IN TONS OF 2,000 LBS.

in feet supports.			Bean,		7 Inch Bram, Standard.		
Distance in feet	25½	221 <u>4</u>	20½	17%	20	171/4	15
between supports.	lbs.	1bs.	lbs.	lbs.	lbs.	lbs.	1bs.
5 6 7 8	18.31 15.26 13.08 11.44	17.26 14.38 12.33 10.79	16.21 13.51 11.58 10.13	15.17 12.64 10.83 9.48	12.87 10.73 9.19 8.04	11.95 9.96 8.53 7.47	11.04 9.20 7.89 6.90
9	10.17	9.59	9.01	8.43	7.15	6.64	6.13
10	9.15	8.63	8.11	7.58	6.44	5.98	5.52
11	8.32	7.85	7.37	6.89	5.85	5.43	5.02
12	7.63	7.19	6.76	6.32	5.36	4.98	4.60
13 14 15 16	7.04 6.54 6.10 5.72	6.64 6.16 5.75 5.39	5.79 5.40 5.07	5.83 5.42 5.06 4.74	4.95 4.60 4.29 4.02	4.60 4.26 8.99 8.74	4.25 3.94 3.68 3.45
17	5.38	5.08	4.76	4.46	3.79	8.52	8.25
18	5.08	4.79	4.50	4.21	3.57	3.32	8.07
19	4.82	4.54	4.27	3.99	3.37	8.15	2.91
20	4.58	4.32	4.05	3.79	3.22	2.99	2.76
21	4.36	4.11	3.86	8.61	3.06	2.84	2.63
22	4.16	3.92	3.68	3.45	2.93	2.71	2.51
23	3.98	3.75	3.52	3.30	2.80	2.60	2.40
24	8.81	3.60	3.38	8.16	2.68	2.49	2.30
25	3.66	8.45	3.24	8.03	2.57	2.39	2.21

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS.

IN TONS OF 2,000 LBS.

e in feet supports.		Inch Bead Standard.	τ,	5 Inch Bram, Standard.			
Distance in feet	17¼	14%	12¼	14%	123 <u>4</u>	9%	
between supports	lbs.	lbs.	lbs.	lbs.	1bs.	1bs.	
5	9.31	8.58	7.74	6.47	5.81	5.16	
6	7.76	7.11	6.45	5.39	4.84	4.80	
7	6.65	6.09	5.58	4.62	4.15	8.68	
8	5.82	5.88	4.84	4.04	8.63	8.22	
9	5.17	4.74	4.30	8.59	3.28	2.87	
10	4.66	4.26	8.87	3.23	2.91	2.58	
11	4.23	3.88	3.52	2.94	2.64	2.84	
12	3.88	8.55	8.23	2.69	2.42	2.15	
13	3.58	8.28	2.98	2.49	2.24	1.98	
14	3.33	8.05	2.77	2.31	2.08	1.84	
15	3.10	2.84	2.58	2.16	1.94	1.72	
16	2.91	2.66	2.42	2.02	1.82	1.61	
17	2.74	2.51	2.28	1.90	1.71	1.52	
18	2.59	2.37	2.15	1.80	1.61	1.48	
19	2.45	2.24	2.04	1.70	1.58	1.36	
20	2.33	2.13	1.93	1.62	1.45	1.29	
21	2.22	2.08	1.84	1.54	1.88	1.28	
22	2.12	1.94	1.76	1.47	1.82	1.17	

# SAFE LOADS UNIFORMLY DISTRIBUTED FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS. IN TONS OF 2,000 LBS.

in feet apports.			BEAM,		8 Inch Beam, Standard.						
Distance in feet	10½	9½	8½	71/4	7½	61/2	5½				
between supports.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.				
5	3.81	3.60	3.89	8.18	2.08	1.92	1.76				
6	3.17	3.00	2.82	2.65	1.78	1.60	1.47				
7	2.72	2.57	2.42	2.27	1.49	1.89	1.26				
8	2.38	2.25	2.12	1.99	1.30	1.20	1.10				
9	2.12	2.00	1.88	1.77	1.16	1.07	.98				
10	1.90	1.80	1.70	1.59	1.04	.96	.88				
11	1.78	1.64	1.54	1.45	.95	.87	.80				
12	1.59	1.50	1.41	1.33	.87	.80	.73				
13	1.46	1.39	1.30	1.22	.80	.74	.68				
14	1.86	1.29	1.21	1.14	.74	.69	.63				
15	1.27	1.20	1.13	1.06	.69	.64	.59				
16	1.19	1.12	1.06	.99	.65	.60	.55				
17	1.12	1.06	1.00	.94	.61	.56	.52				
18	1.06	1.00	.94	.88	.58	.53	.49				
19	1.00	.95	.89	.82	.55	.50	.46				
20	.95	.90	.85	.79	.52	.48	.44				
21	.91	.86	.81	.75	.50	.46	.42				
22	.88	.82	.77	.72	.48	.44	.40				

Safe load includes weight of Beam. Maximum fiber strain of  $16,000 \, \mathrm{lbs.} \ \mathrm{per} \ \mathrm{square} \ \mathrm{inch.}$ 

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL CHANNELS.
IN TONS OF 2,000 LBS.

Distance in feet between supports.	15 Inch Channel, Standard.												
	55 lbs.	50 lbs.	45 lbs.	40 lbs.	35 lbs.	33 lbs.							
10	30.85	28.80	26.93	24.97	23.01	22.22							
11	28.05	26.27	24.48	22.70	20.92	20.20							
12	25.71	24.08	22.44	20.81	19.17	18.52							
18	23.73	22.22	20.72	19.21	17.70	17.10							
14	22.04	20.64	19.24	17.84	16.44	15.87							
15	20.57	19.26	17.96	16.65	15.34	14.82							
16	19.28	18.06	16.83	15.61	14.38	13.89							
17	18.15	16.99	15.84	14.69	13.53	13.07							
18	17.14	16.05	14.96	13.87	12.78	12.35							
19	16.24	15.21	14.17	13.14	12.11	11.69							
20	15.43	14.45	13.47	12.48	11.50	11.11							
21	14.69	13.76	12.82	11.89	10.96	10.58							
22	14.02	13.13	12.24	11.35	10.46	10.10							
28	18.41	12.56	11.71	10.86	10.00	9.66							
24	12.86	12.04	11.22	10.40	9.59	9.26							
25	12.34	11.56	10.77	9.99	9.20	8.89							
26	11.87	11.11	10.36	9.60	8.85	8.55							
27	11.43	10.70	9.97	9.25	8.52	8.29							
28	11.02	10.82	9.62	8.92	8.22	7.94							
29	10.64	9.96	9.29	8.61	7.98	7.66							
30	10.28	9.63	8.98	8.32	7.67	7.41							

### SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL CHANNELS.

IN TONS OF 2,000 LBS.

in feet supports.	12 Inch Channels, Standard.											
Distance in feet between supports.	40 1bs.	35 lbs.	80 lbs.	25 lbs.	2014 1bs.							
10.	17.50	15.93	14.36	12.80	11.38							
11	15.91	14.49	13.06	11.64	10.35							
12	14.59	13.28	11.97	10.67	9.48							
13	13.46	12.25	11.05	9.85	8.76							
14	12.50	11.38	10.26	9.14	8.18							
15	11.67	10.62	9.58	8.53	7.59							
16	10.94	9.96	8.98	8.00	7.12							
17	10.30	9.37	8.45	7.53	6.69							
18	9.72	8.85	7.98	7.11	6.88							
19	9.21	8.89	7.56	6.74	5.99							
20	8.75	7.97	7.18	6.40	5.69							
21	8.34	7.59	6.84	6.09	5.42							
22	7.96	7.24	6.53	5.82	5.18							
23	7.61	6.93	6.25	5.56	4.98							
24	7.29	6.64	5.99	5.33	4.74							
25	7.00	6.37	5.75	5.12	4.55							
26	6.73	6.13	5.53	4.92	4.38							
27	6.48	5.90	5.82	4.74	4.22							
28	6.25	5.69	5.13	4.57	4.07							
29	6.04	5.49	4.95	4.41	3.92							
80	5.83	5.31	4.79	4.27	8.79							

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS. IN TONS OF 2,000 LBS.

Distance in feet between supports.	15 Inch Beam, Heavy Section.											
Distance	100	95	90	85	80							
between	lbs.	lbs.	1bs.	1bs.	1bs.							
10	63.96	62.00	60.04	58.08	56.11							
11	58.14	56.36	54.58	52.80	51.01							
12	53.30	51.66	50.03	48.40	46.76							
18	49.20	47.69	46.18	44.67	43.17							
14	45.68	44.28	42.88	41.48	40.08							
15	42.64	41.33	40.02	38.72	87.41							
16	89.97	38.75	37.52	36.30	35.07							
17	87.62	36.47	35.32	34.16	33.01							
18	85.53	34.44	33.35	32.26	31.17							
19	83.66	32.63	31.60	30.57	29.52							
20	81.98	31.00	30.02	29.04	28.06							
21	80.45	29.52	28.59	27.66	26.73							
22	29.07	28.18	27.29	26.40	25.51							
23	27.81	26.96	26.10	25.25	24.40							
24	26.65	25.83	25.01	24.20	23.38							
25	25.58	24.80	24.01	23.23	22.45							
26	24.60	23.84	23.09	22.34	21.58							
27	23.69	22.96	22.24	21.51	20.78							
28	22.84	22.14	21.44	20.74	20.04							
29	22.05	21.38	20.70	20.03	19.85							
30	21.32	20.67	20.01	19.36	18.70							
81	20.63	20.00	19.37	18.73	18.10							
82	19.99	19.87	18.76	18.15	17.54							
83	19.38	18.79	18.19	17.60	17.00							
84	18.81	18.23	17.66	17.08	16.50							
85	18.27	17.71	17.15	16.59	16.03							
86	17.76	17.22	16.68	16.13	15.59							

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS.
IN TONS OF 2,000 LSS.

Distance in feet between supports.	15 Inch Bram, Light Section.											
Distance	80	75	70	65	60							
between	lbs.	lbs.	lbs.	lbs.	lbs.							
10	51.15	49.19	47.23	45.27	43.31							
11	46.50	44.72	42.93	41.15	39.37							
12	42.62	40.99	39.36	87.72	36.09							
18 14 15	89.35 36.54 34.10 31.97	87.84 85.18 82.79 80.74	86.33 33.73 31.49 29.52	34.82 32.33 30.18 28.29	33.81 30.93 28.87 27.07							
17	30.09	28.93	27.78	26.63	25.47							
18	28.42	27.38	26.24	25.15	24.06							
19	26.92	25.89	24.86	23.82	22.79							
20	25.57	24.59	23.61	22.63	21.65							
21	24.36	23.42	22.49	21.56	20.62							
22	23.25	22.36	21.47	20.58	19.69							
23	22.24	21.39	20.53	19.68	18.83							
24	21.31	20.50	19.68	18.86	18.04							
25	20.46	19.68	18.89	18.11	17.32							
26	19.67	18.92	18.16	17.41	16.66							
27	18.95	18.22	17.49	16.77	16.04							
28	18.27	17.57	16.87	16.17	15.47							
29	17.64	16.96	16.29	15.61	14.93							
30	17.05	16.40	15.74	15.09	14.44							
31	16.50	15.87	15.23	14.60	13.97							
32	15.98	15.37	14.76	14.14	18.53							
83	15.50	14.91	14.31	13.72	13.12							
84	15.04	14.47	13.89	13.31	12.74							
85	14.61	14.05	13.49	12.93	12.36							
<b>8</b> 6	14.21	13.66	18.12	12.57	12.08							

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL BEAMS. IN TONS OF 2,000 LBS.

Distance in feet between supports.	15 Inch Bram, Standard.											
Distanc	60	55	50	45	42							
between	lbs.	lbs.	lbs.	lbs.	lbs.							
10	38.47	36.52	84.55	32.59	31.41							
11	34.97	33.19	31.41	29.63	28.56							
12	32.06	30.42	28.79	27.16	26.18							
13	29.59	28.08	26.58	25.07	24.16							
14	27.48	26.08	24.68	23.28	22.44							
15	25.65	24.34	23.03	21.73	20.94							
16	24.04	22.82	21.59	20.37	19.63							
17	22.68	21.49	20.32	19.17	18.48							
18	21.37	20.28	19.19	18.10	17.45							
19	20.25	19.21	18.18	17.15	16.53							
20	19.28	18.26	17.26	16.29	15.71							
21	18.32	17.38	16.45	15.52	14.96							
22	17.49	16.59	15.70	14.81	14.28							
23	16.73	15.87	15.02	14.17	13.66							
24	16.03	15.21	14.40	13.58	13.09							
25	15.39	14.60	13.82	13.04	12.56							
26	14.80	14.04	13.29	12.58	12.08							
27	14.24	13.52	12.80	12.07	11.63							
28	13.74	13.04	12.34	11.64	11.22							
29	13.26	12.59	11.91	11.24	10.83							
30	12.82	12.17	11.52	10.86	10.47							
31	12.41	11.78	11.14	10.51	10.18							
32	12.02	11.41	10.80	10.18	9.82							
33	11.66	11.06	10.47	9.88	9.52							
34	11.31	10.74	10.16	9.58	9.24							
35	10.99	10.43	9.87	9.31	8.97							
36	10.69	10.14	9.60	9.05	8.73							

# SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR .JONES & LAUGHLINS, LIMITED, STEEL BEAMS. IN TONS OF 2,000 LBS.

in feet supports.	1	12 Ince	BEAM, SECTION	i <b>.</b>	12 Inch Beam, Standard.						
Distance in feet	55	50	45	40	40	35	81½				
between supports.	1bs.	lbs.	lbs.	1bs.	lbs.	lbs.	lbs.				
10	28.61	27.04	25.48	23.91	21.85	20.28	19.18				
11	26.01	24.58	23.16	21.73	19.86	18.44	17.4				
12	23.84	22.54	21.28	19.92	• 18.21	16.90	15.9				
18	22.01	20.80	19.60	18.39	16.81	15.60	14.70				
14	20.44	19.82	18.20	17.08	15.62	14.49	18.70				
15	19.08	18.08	16.98	15.94	14.56	13.52	12.70				
16	17.88	16.90	15.92	14.94	13.66	12.68	11.90				
17	16.88	15.91	14.99	14.06	12.85	11.98	11.2				
18	15.90	15.02	14.15	18.28	12.14	11.27	10.6				
19	15.06	14.28	18.41	12.58	11.50	10.62	10.1				
20	14.81	18.52	12.74	11.95	10.93	10.14	9.5				
21	18.68	12.88	12.13	11.38	10.41	9.66	9.1-				
22	13.01	12.29	11.58	10.87	9.93	9.22	8.7:				
23	12.44	11.76	11.08	10.39	9.50	8.82	8.8-				
24	11.92	11.27	10.61	9.96	9.10	8.45	7.9:				
25 26 27 28	11.45 11.01 10.60 10.22	10.82 10.40 10.02 9.66	10.19 9.80 9.43 9.10	9.56 9.19 8.85 8.54	8.75 8.40 8.09 7.81	8.11 7.80 7.51 7.24	7.6' 7.3' 7.10				
29 30 31 82	9.87 9.54 9.23 8.94	9.33 9.01 8.72 8.45	8.78 8.48 8.21 7.96	8.24 7.97 7.71 7.47	7.53 7.28 7.05 6.83	6.99 6.76 6.54 6.84	6.69 6.39 6.19				
33	8.67	8.19	7.72	7.24	6.62	6.15	5.8				
34	8.42	7.95	7.49	7.03	6.48	5.97	5.6				
35	8.17	7.72	7.28	6.83	6.24	5.79	5.4				
36	7.95	7.51	7.08	6.64	6.07	5.63	5.8				

# SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL CHANNELS. IN TONS OF 2,000 LSS.

e in feet supports.		6 Inch (	Channei dard.	4,	5 Inch Channel, Standard.					
Distance in feet	15½	13	101/4	8	111/4	9	6½			
between support	1bs.	1bs.	lbs.	lbs.	lbs.	lbs.	lbs.			
5	6.97	6.19	5.41	4.62	4.47	3.82	3.16			
6	5.81	5.16	4.50	3.85	3.78	3.18	2.64			
7	4.98	4.42	3.86	3.30	3.19	2.73	2.26			
8	4.36	8.87	3.38	2.89	2.79	2.39	1.98			
9	3.87	3.44	3.00	2.57	2.48	2.12	1.76			
10	3.49	3.09	2.73	2.31	2.23	1.92	1.58			
11	3.17	2.81	2.45	2.10	2.03	1.75	1.44			
12	2.91	2.58	2.25	1.93	1.86	1.59	1.32			
18	2.68	2.38	2.08	1.78	1.72	1.48	1.22			
14	2.49	2.21	1.93	1.65	1.59	1.36	1.13			
15	2.32	2.06	1.80	1.54	1.49	1.27	1.05			
16	2.18	1.98	1.69	1.44	1.39	1.19	.99			
17	2.05	1.82	1.59	1.36	1.31	1.18	.93			
18	1.93	1.72	1.50	1.28	1.24	1.06	.88			
19	1.84	1.62	1.42	1.22	1.17	1.01	.83			
20	1.74	1.55	1.35	1.15	1.11	.96	.79			
21	1.66	1.47	1.29	1.10	1.06	.91	.75			
22	1.58	1.40	1.22	1.05	1.01	.87	.72			
23	1.52	1.35	1.17	1.00	.97	.83	.69			
24	1.45	1.29	1.12	.96	.93	.79	.66			
25	1.39	1.24	1.08	.92	.89	.76	.63			

Safe load includes weight of Channel. Maximum fiber strain of 16,000 lbs. per square inch.

SAFE LOADS, UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, STEEL CHANNELS.

IN TONS OF 2,000 LBS.

in feet upports.		CH CHANI	, ,	8 Inch Channel, Standard.						
Distance in feet	7½	6¼	5½	6	5	4				
between supports	1bs.	lbs.	lbs.	lbs.	1bs.	lbs.				
5	2.44	2.23	2.02	1.48	1.82	1.16				
6	2.04	1.86	1.69	1.23	1.10	.97				
7	1.74	1.59	1.44	1.06	.94	.83				
8	1.53	1.39	1.26	.92	.82	.73				
9	1.36	1.24	1.12	.82	.78	.65				
10	1.22	1.12	1.01	.74	.66	.58				
11	1.11	1.01	.92	.67	.60	.53				
12	1.02	.93	.84	.62	.55	.48				
13	.94	.86	.78	.57	.51	.45				
14	.87	.79	.76	.53	.47	.41				
15	.81	.74	.67	.49	.44	.39				
16	.76	.69	.63	.46	.41	.36				
17	.72	.66	.60	.43	.39	.34				
18	.68	.62	.56	.41	.36	.32				
19	.64	.59	.53	.39	.35	.31				
20	.62	.56	.51	.37	.33	.29				
21	.58	.53	.49	.35	.81	.28				
22	.55	.50	.46	.33	.30	.26				
23	.53	.48	.44	.32	.29	.25				
24	.51	.46	.42	.31	.27	.24				
25	.49	.45	.40	.29	.26	.23				

TEES. SAFE LOADS, IN TONS OF 2,000 LBS., UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, TEES.

Section No.	Size flange		Dis	TANCI	BET	WEEK	SUPE	ORTS	m F	BET.	
Sec	by stem.	1	2	8	4	5	6	7	8	9	10
T 20 T 21 T 22 T 1	4 ×5 4 ×4¾ 4 ×4¼ 4 ×4	18.40 12.22 11.08 8.75	6.70 6.11 5.51 4.87	4.47 4.07 8.67 2.92	3.85 3.06 2.76 2.19	2.68 2.44 2.20 1.75	2.04	1.91 1.75 1.57 1.25	1.68 1.58 1.88 1.09	1.86 1.22	1.84 1.22 1.10 0.88
T 2 T 8 T 4 T 23	4 ×4 8½×8½ 8½×8½ 8½×3	7.71 5.53 4.79 4.09	8.86 2.77 2.89 2.04	2.57 1.84 1.60 1.86	1.93 1.88 1.20 1.02	1.11 0.96	1.29 0.92 0.80 0.68	1.10 0.79 0.69 0.58	0.96 0.69 0.60 0.51	0.61 0.53	0.55
T 24 T 26 T 25 T 5	8½×8 8 ×8½ 3 ×8½ 3 ×3	8.54 5.89 4.67 8.58	1.77 2.69 2.88 1.79	1.18 1.80 1.56 1.19		0.71 1.08 0.93 0.72	0.59 0.90 0.78 0.60	0.51 0.77 0.67 0.51	0.44 0.67 0.58 0.45	0.60 0.52	
T6 T7 T8 T28	8 ×8 2¼×2¼ 2½×2½ 2½×2	3.08 2.44 2.09 1.27	1.54 1.22 1.04 0.64	1.08 0.81 0.70 0.42	0.77 0.61 0.52 0.82	0.49		0.44 0.85 0.80 0.18	0.88 0.30 0.26 0.16	0.27 0.28	0.24 0.21
T 9 T 10 T 11 T 27	2¼×2¼ 2¼×2¼ 2 ×2 2¼×1¾	1.60 1.81 1.02 0.77	0.80 0.65 0.51 0.89	0.58 0.44 0.84 0.26	0.40 0.38 0.26 0.19		0.27 0.22 0.17 0.18	0.28 0.19 0.15 0.11	0.16 0.18	0.15	0.18 0.10
T 13 T 12 T 14 T 15	1%×1% 1%×1% 1%×1% 1%×1%	0.77 0.51 0.55 0.46	0.38 0.26 0.28 0.23	0.26 0.17 0.18 0.15	0.13	0.15 0.10 0.11 0.09	0.18 0.09 0.09 0.08	0.11 0.07 0.08 0.07			0.05
T 16 T 17 T 18 T 19	11/4×11/4 11/4×11/4 1 ×1 1 ×1	0.89 0.29 0.19 0.14		0.06	0.07	0.06	0.07 0.05 0.08 0.02	0.08	0.05 0.04 0.02 0.02	0.08	0.03

JONES & LAUGHLINS, LIMITED.

UNIVERSITY OF CALIFORNIA

#### ANGLES.

SAFE LOADS, IN TONS OF 2,000 LBS., UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, ANGLES, WITH EQUAL LEGS.

	Size					:	D187	ran	CE	Bl	ITW	E	n S	δŪ	PPO	R1	rs 11	N	FEI	ET.	•		
	Ang	ΙŒ	<b>,</b>		1		2		В		4		5		6		7		8		9	1	10
3	×6 ×6		× X × X			8 15	14 28	5. 10.			07 64				72 09				04 82			1. 8.	
,	×5		×Ħ		.88		44						78									o.	
•	×5		×¾				04						62							2.		1.	
ŀ	X4	į	××	6	.08		04						22									Q.	
Ŀ	×4		× %	11	. 24	١٥	62	3.	75	z.	81	z.	25	1.	.87	ı.	61	1.	41	μ.	25	1.	17
34	4×8	4	× %	4 ا	.60	2	.30	1.	58	1.	15	o.	92	o.	.77	O.	66	o.	58	o.	51	0.	41
	€×8				.12		.06															ŏ.	
	ί×8				.96		98															Õ.	
	×8				.44	2	.72	1.	81	1.	86	1.	09	0.	. 91	0.	78	0.	.68	0.	<b>6</b> 0	0.	5
3	·×8		×¾	2	.82	1	.16	l o	77	o.	58	o.	46	lo.	.89	o.	88	0	29	lo.	26	0.	2
ś	- 28		χŵ		.20		.60															ŏ.	
3	٤×٤				.92		96	Ō.				Ō.	88	0.						0.		Ō.	
33	٤×٤	×	×У	8	.56	1	.78	1.	18	0.	.89	0.	71	0.	.58	0.	51	0.	45	0.	40	0.	8
24	<b>4</b> ×2	46	×¥	1	.60	0	.80	0	53	lo.	40	0.	82	0	.27	0.	.28	o.	20	o.	18	0.	10
εį	₹×2	Ý,	ХÝ	2	.92	1	46	0	97	0.			58		. 49			0.	.87	0.	82	0.	2
	₹×2				.28		.64						26									0.	
33	4×2	×	×Ж	2	.82	1	. 16	0	77	0	58	0.	46	0	. 89	0.	.88	0.	29	0.	.26	0.	2
5	׿		×ч	0	.60	0	.80	0	.20	0	15	o.	12	0	.10							0.	0
5	XS		×		.60		.80															0.	
	٤×1				.44		.22															0.	
13	€×1	×	×	1	.20	0	.60	0	40	0	.80	0.	24	0	.20	0.	. 17	10.	. 15	0.	. 18	0.	Ľ
13	<b>6</b> ×1	14	×ч	lo	. 81	0	. 16	lo	10	0	.08	0.			.05	0.	.04	o.	.04	0.	.08	o.	0
١į	4×1	1/2	××	0	.77		.89															0.	
13	ίX1	×	×Я		.20		.098								.083								
Į	ŽX1	×	×¥	0	. 36	0	. 18	0	. 12	Ю	.09	0.	072	0	.060	0.	.051	0	.045	0	.040	0.	0
ı	<b>X</b> 1		×¾	10	.18	6	.065	0	.048	0	.088	0	026	0	.022	0	.019	o	.016	0	.014	o.	0
i	Χī		×X ×i	il c	.17		.085	0	.057	10	.043	0.	.084	0	.028	0	.024	0	.021	0	.019	0.	0
3	ΚX	×	×Я	0	.07	0	.085	0	.028	10	.018	10.	.014	0	.012	0	.010	0	.009	10	.008	0.	0
3			×i		.095	0	.048	0	.032	10	.024	0	.019	10	.016	0	.014	:0	.012	0	.011	0	.0

Safe Loads include weight of Angle. Maximum fiber strain 12,000 lbs. per square inch. Neutral axis through center of gravity parallel to one leg.

#### ANGLES.

# SAFE LOADS, IN TONS OF 2,000 LBS., UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, ANGLES, WITH UNEQUAL LEGS.

#### LONG LEG VERTICAL.

	Size of			Dist	ANCE	BETV	VEEN	SUPP	ORTS :	n Fi	BT.	
	Angle.		1	2	8	4	5	6	7	8	9	10
6 6 6	X4 X X	% 18 %	13.28 26 60 13.00 24.80	6.50	4.48 8.87 4.88 8.27	8.32 6.65 8.25 6.20	2.66 5.82 2.60 4.96	2.21 4.48 2.17 4.18	1.90 8.80 1.86 8.54	1.66 8.88 1.68 8.10	1.47 2.96 1.44 2.76	1.88 2.66 1.30 2.48
5 5 5 5	X4 X X81/4 X	% % % %	9.40 17.24 9.16 16.88	4.58	3.13 5.75 3.05 5.68	2.85 4.81 2.29 4.22	1.88 8.45 1.83 3.88	1.57 2.87 1.58 2.81	1.84 2.46 1.81 2.41	1.18 2.16 1.15 2.11	1.92 1.02	0.94 1.78 0.92 1.69
5 5 4 4	×8 × ×8½×	% % % %	8.92 16.52 6.00 10.92	8.26 3.00	2.97 5.51 2.00 8.64	2.28 4.18 1.50 2.78	1.78 3.80 1.20 2.18	1.49 2.75 1.00 1.82	1.27 2.36 0.86 1.56	1.12 2.07 0.75 1.87	1.84 0.67	0.89 1.65 0.60 1.09
	×3 × (×25/4×	**************************************	5.72 10.64 5.04 9.16	5.82 2.52	1.91 8.55 1.68 3.05	1.43 2.66 1.26 2.29	2.18	1.77	0.82 1.52 0.72 1.31	0.72 1.33 0.63 1.15	1.18 0.56	
8½ 8½	4×8 × 4×24×	% % % %	4.86 8.12 8.00 5.84	4.06 1.50	1.45 2.71 1.00 1.95	1.09 2.08 0.75 1.46	1.62 0.60	1.85 0.50	0.62 1.16 0.48 0.88	1.02 0.88	0.90	0.81 0.80
	×24 ×	14 14 14 14 14	2.24 4.12 2.04 4.64	2.06 1.02		0.56 1.08 0.51 1.16	0.82 0.41	0.69	0.59	0.28 0.52 0.26 0.58	0.46	0.41
	×2 × ×2 × 4×2 × 4×2 ×	16 16 16 16 18	8.86 4.00 1.16 2.84	2.00 0.58		1.00	0.80	0.67	0.57	0.50	0.44	0.40
	(×1¼×	13 1% 1%	0.84 0.28 0.11	0.12	0.08	0.06	0.05	0.04	0.08	0.08	0.03	0.02

Safe Loads include weight of Angle. Maximum fiber strain of 12,000 lbs. per square inch. Neutral axis through centre of gravity parallel to short leg.

#### ANGLES.

SAFE LOADS, IN TONS OF 2,000 LBS., UNIFORMLY DISTRIBUTED, FOR JONES & LAUGHLINS, LIMITED, ANGLES, WITH UNEQUAL LEGS.

#### SHORT LEG VERTICAL.

Size of	DISTANCE BETWEEN SUPPORTS IN FEE1.									
Angle.	1	2	8	4	5	6	7	8	9	10
6 ×4 ×% 6 ×4 ×18 6 ×8½×% 6 ×8½×18	12.60 4.92	6.80 2.46	1.64		1.28 2.52 0.98 1.93	2.10 0.82	1.80 0.70	1.58 0.62	1.40	0.64 1.26 0.49 0.96
5 ×4 ×% 5 ×4 ×% 5 ×8%×% 5 ×3%×%	11.44	5.72	2.09 3.81 1.60 2.91	1.57 2.86 1.20 2.18		1.91 0.80	1.63 0.69	1.48	1.27	0.68 1.14 0.48 0.87
5 ×3 ×% 5 ×8 ×% 4 ×3½×% 4 ×3½×%	6.44 4.72	3.22 2.36	2.15 1.57	0.89 1.61 1.18 2.18	1.29	1.07 0.79	0.92 0.67	0.81 0.59	0.72 0.52	0.86 0.64 0.47 0.85
4 ×8 ×% 4 ×8 ×% 8 × 2 % × % 8 × 2 % × %	6.24		2.08	0.85 1.56 0.66 1.18		1.04 0.44	0.89 0.88		0.69	0.84 0.62 0.26 0.47
814×8 × 16 814×8 × 16 814×214×14 814×214×14	6.08	3.04	2.03	0.83 1.52 0.41 0.81	1.22		0.87 0.23	0.42 0.76 0.21 0.41	0.68	0.38 0.61 0.16 0.82
8 ×2½×½ 8 ×2½×½ 8½×2 ×½ 8½×2 ×½	2.92		0.58 0.97 0.28 0.64	0.40 0.78 0.21 0.48	0.82 0.58 0.17 0.88	0.24 0.49 0.14 0.82	0.42	0.20 0.37 0.11 0.24	0.18 0.32 0.09 0.21	0.16 0.29 0.08 0.19
8 ×2 ×4 8 ×2 ×½ 2½×2 ×4 2½×2 ×½	1.88		0.27 0.63 0.25 0.62	u.20 0.47 0.19 0.47	0.16 0.38 0.15 0.87	0.18 0.81 0.18 0.31	0.11 0.27 0.11 0.27	0.10 0.24 0.10 0.28	0.09 0.21 0.08 0.21	0.08 0.19 0.08 0.19
1%×1%×5 1%× %×% 1 × %×%	0.10	0.05	0.08		0.02	0.02	0.01	0.05 0.01 0.006	0.01	0.04 0.01 0.005

Safe Loads include weight of Angle. Maximum fiber strain of 12,000 lbs, per square inch. Neutral axis through centre of gravity parallel to long leg.

#### GIRDERS.

SAFE LOAD, IN TONS OF 2,000 LBS.
UNIFORMLY DISTRIBUTED, FOR BOX GIRDERS COMPOSED
OF TWO 10" BEAMS AND TWO 12X\frac{3}{2}" PLATES.

	54"								
to center of the feet.	_	Beams. . per foot.			2-12x½" Steel Plates.				
Distance, center to center of bearings, in feet.	Safe Load in Tons, including weight of Girder.	Weight of Girder in pounds.	Add to Safe Load for 5 pounds in- crease in weight of Beam.	Add to Safe Load for A" increase in thickness of Plates.	Add to weight of Girder for 5 pounds increase in weight of Beam.	Add to weight of Girder for A. increase in thickness of plates.			
12 13 14 15 16 17 18	82.5 30.0 27.9 26.0 24.4 22.9 21.7	1114 1206 1299 1392 1485 1578 1670	1.56 1.44 1.34 1.25 1.17 1.10 1.04	2.35 2.17 2.01 1.88 1.76 1.66 1.57	120 130 140 150 160 170 180	61 66 71 77 82 87 92			
19 20 21 22 23 24 25	20.5 19.5 18.6 17.8 17.0 16.3 15.6	1763 1856 1949 2042 2134 2227 2320	0.98 0.93 0.89 0.85 0.81 0.78 0.75	1.48 1.41 1.34 1.28 1.23 1.17	190 200 210 220 230 240 250	97 102 107 112 117 122 128			
26 27 28 29 80 31 82	15.0 14.4 13.9 13.4 13.0 12.6 12.2	2413 2506 2598 2691 2784 2877 2970	0.72 0.69 0.67 0.64 0.62 0.60 0.58	1.08 1.04 1.01 0.97 0.94 0.91 0.88	260 270 280 290 300 310 320	133 138 143 148 153 158 163			
33 34 35 36 37 38	11.8 11.5 11.1 10.8 10.5 10.3	3062 3155 3248 3341 3434 3526	0.57 0.55 0.53 0.52 0.51 0.49	0.85 0.83 0.81 0.78 0.76 0.74	330 340 350 360 370 380	168 173 179 184 189 194			

Above values are based on maximum fiber strain of 13,000 lbs. per square inch, ‡¾" rivet holes deducted. Weights correspond to lengths, center to center of bearings.

#### GIRDERS.

SAFE LOAD, IN TONS OF 2,000 LBS.
UNIFORMLY DISTRIBUTED, FOR BOX GIRDER COMPOSED
OF TWO 12" STEEL BEAMS AND TWO 14X}" STEEL PLATES.

Distance, center to center of bearings, in feet.	2-12" Beams. 314 lbs. per foot. 2-14x4". Steel Plates.			2-12" Beams. 40 lbs. per foot. 2-14xgi". Steel Plates.					
Distance, cen	Safe Load in Tons, including weight of Girder.	Weight of Girder in pounds.	Add to Safe Load for 1 pound in- crease in weight of Beam.	Safe Load in Tons, including weight of Girder.	Weight of Girder in pounds.	Add to Safe Load for 5 pounds in- crease in weight of Beam.	Add to Safe Load for 14" increase in thickness of Plates.	Add to weight of Girder for 14" in- crease in thickness of flange plates.	
12 13 14 15 16 17 18	47.7 44.0 40.9 88.1 85.7 83.6 81.8	1351 1464 1576 1689 1802 1914 2027	0.395 0.364 0.338 0.816 0.296 0.279 0.263	53.0 48.9 45.4 42.4 39.7 37.4 35.3	1555 1685 1814 1944 2074 2203 2333	1.94 1.79 1.66 1.55 1.45 1.87 1.29	8.36 8.10 2.88 2.69 2.52 2.37 2.24	71 77 83 89 95 101 107	
19 20 21 22 23 24 25	30.1 28.6 27.2 26.0 24.9 23.8 22.9	2139 2252 2365 2477 2590 2702 2815	0.249 0.287 0.225 0.215 0.206 0.197 0.189	83.5 31.8 80.3 28.9 27.6 26.5 25.4	2462 2592 2722 2851 2981 3110 3240	1.22 1.16 1.11 1.06 1.01 0.97 0.93	2.12 2.02 1.92 1.83 1.75 1.68 1.61	118 119 125 181 187 148 149	
26 27 28 29 30 31 32	22.0 21.2 20.4 19.7 19.1 18.4 17.8	2928 3040 3153 3265 3378 8491 8603	0.182 0.175 0.169 0.163 0.158 0.153 0.148	24.4 23.5 22.7 21.9 21.2 20.5 19.9	3370 3499 3629 3758 3888 4018 4147	0.89 0.86 0.83 0.80 0.77 0.75 0.73	1.55 1.49 1.44 1.39 1.34 1.30 1.26	155 161 167 178 179 184 190	
83 84 85 86 87 88	17.3 16.8 16.3 15.9 15.4 15.0	8716 8828 8941 4054 4166 4279	0.143 0.139 0.135 0.131 0.128 0.124	19.3 18.7 18.2 17.7 17.2 16.7	4277 4406 4536 4666 4795 4925	0.70 0.68 0.66 0.65 0.63 0.61	1.22 1.19 1.15 1.12 1.09 1.06	196 202 208 214 220 226 lbs.	

Above values are based on maximum fiber strain of 13,000 lbs. per square inch, 13" rivet holes deducted. Weights correspond to length, center to center of bearings.

### GIRDERS.

SAFE LOAD, IN TONS OF 2,000 LBS., UNIFORMLY DISTRIBUTED, FOR BOX GIRDER COMPOSED OF TWO 18" STEEL BEAMS AND TWO 14X!" STEEL PLATES.

	6"				6"				
er of	Beams. per foot.		2-14xi'' Steel Plates.	Beams. per foet.	4	<del>-</del>	Z-14xi," Steel Plates.	r A" in-	
et.	16. B		2-14xi bei Pia				2-14×1 0 Pin	200	
5 8	2-16" 12 lbs.	1 1	Ster	80-15. 15.		- 1 '	St.	P. C.	
s, fin	-		<b>-</b>		-	<del>-</del>		E SE	
Distance, center to center of bearings, in feet.	Safe Load in Tons, including weight of Girder.	Weight of Girder in pounds.	Add to Safe Load for 1 pound in- crease in weight of Beam.	Safe Load in Tons, including weight of Girder.	Weight of Girder in pounds.	Add to Safe Load for 5 pounds in- crease in weight of Beam.	Add to Safe Load for A" increase in thickness of Plates.	Add to weight of Girder for 14" in- crease in thickness of flange plates	
12	76.6	1746	0.486	90.2	2178	2.47	4.20	72	
18 14	70.7 65.7	1891 2037	0.449 0.417	83.2 77.3	2359 2541	2.28 2.11	3.87 3.60	78 84	
15	61.3	2182	0.389	72.1	2722	1.97	8.86	90	
16	57.5	2328	0.365	67.6	2904	1.85	8.15	96	
17 18	54.1 51.1	2473 2619	0.343 0.324	63.6 60.1	3085 3267	1.74 1.64	2.96 2.80	102 108	
19	48.4	2764	0.307	56.9	3448	1.56	2.65	114	
20 21	46.0 43.8	2910 3055	0.292 0.278	54.1 51.5	3630 3811	1.48 1.41	2.52 2.40	120 126	
22	41.8	3201	0.265	49.2	3993	1.84	2.29	132	
23	40.0	3346	0.253	47.0	4174 4356	1.29	2.19	188	
24 25	38.3 36.8	3492 3637	0.243 0.233	45.1 43.3	4537	1.23 1.18	2.10 2.01	144 150	
26	85.4	3783	0.224	41.6	4719	1.14	1.94	156	
27 28	34.1 32.8	3928 4074	0.216	40.1 38.6	4900 5082	1.10 1.06	1.86 1.80	162 168	
29	81.7	4219	0.200	87.3	5263	1.00	1.74	174	
80	30.7	4365	0.195	36.1	5445	0.99	1.68	180	
81	29.7	4510	0.189	84.9	5626	0.95	1.62	186	
32	28.7	<b>4656</b>	0.182	83.8	5808	0.92	1.57	192	
83	27.9	4801	0.177	82.8	5989	0.90	1.52	198	
34 85	27.0	4947	0.172	31.8	6171	0.87	1.48	204	
36	26.3 25.5	5092 5238	0.167 0.162	36.9 30.0	6352 6534	0.84	1.44 1.40	210 216	
37	24.9	5383	0.158	29.2	6715	0.80	1.36	222	
38	24.2	5529	0.154	28.5	6897	0.78		228	

Above values are based on maximum fiber strain of 13,000 lbs. per square inch, 13" rivet holes deducted. Weights correspond to lengths, center to center of bearings.

### GIRDERS.

SAFE LOAD, IN TONS OF 2,000 LBS., UNIFORMLY DISTRIBUTED, FOR BOX GIRDER COMPOSED OF TWO 20" STEEL BEAMS AND TWO 16X2" STEEL PLATES,

	i 7211 II di 711									
Distance, center to center of bearings, in feet.	2-20" Steel Beams 60 lbs. per feet.	71"	2-16x3" Steel Plates.	2-20" Steel Beams. 64 lbs. per foot.		Steel P	f Girder for 14" in-			
Distance, cen	Safe Load in Tons, including Weight of Girder. Weight of Girder in pounds.	Add to Safe Load for 5 pounds in- crease in weight of Beam.	Add to Safe Load for 14" increase in thickness of Plates.	Safe Load in Tons, including weight of Girder. Weight of Girder in pounds.	Add to Safe Load for 1 pound in- crease in weight of Beam.	Add to Safe Load for A" increase in thickness of Plates.	Add to weight of Girder for 18" crease in thickness of plates			
12 13 14 15 16 17 18	167.5 2923 154.7 8167 143.6 3410 134.0 3654 125.7 3898 118.3 4141 111.7 4885	3.24 2.99 2.78 2.59 2.43 2.28 2.16	6.02 5.56 5.16 4.81 4.51 4.25 4.01	148.7 2539 137.8 2751 127.5 2962 119.0 3174 111.5 3386 105.0 3597 99.1 3809	0.597 0.555 0.518 0.485	6.12 5.65 5.25 4.90 4.59 4.82 4.08	82 88 95 102 109 116 122			
19 20 21 22 23 24 25	105.8 4628 100.5 4872 95.7 5116 91.4 5359 87.4 5603 83.8 5846 80.4 6090	2.05 1.94 1.85 1.77 1.69 1.62 1.55	8.80 8.61 3.44 8.28 3.14 3.01 2.89	93.9 4020 89.2 4232 85.0 4444 81.1 4655 77.6 4867 74.4 5078 71.4 5290	0.409 0.388 0.370 0.353 0.338 0.324 0.811	3.86 3.67 3.50 3.34 3.19 3.06 2.94	129 136 143 150 156 163 170			
26 27 28 29 30 31 32	77.3 6384 74.5 6577 71.8 6821 69.3 7064 67.0 7308 64.8 7552 62.8 7795	1.50 1.44 1.39 1.34 1.30 1.25 1.21	2.78 2.68 2.58 2.49 2.41 2.33 2.26	68.6 5502 66.1 5713 63.7 5925 61.5 6136 59.5 6348 57.6 6560 55.8 6771	0.299 0.288 0.277 0.268 0.259 0.251 0.243		177 184 190 197 204 211 218			
33 34 35 36 37 38	60.9 8089 59.1 8282 57.4 8526 55.8 8770 54.8 9013 52.9 9256	1.18 1.14 1.11 1.08 1.05 1.03	2.19 2.12 2.06 2.01 1.95 1.90	54.1 6983 52.5 7194 51.0 7406 49.6 7618 48.2 7829 47.0 8041	0.235 0.228 0.222 0.216 0.210 0.204	2.16 2.10 2.04 1.98 1.93	224 231 238 245 252 258 1bs.			

Above values are based on maximum fiber strain of 18,000 lbs. per square inch, †?" rivet holes deducted. Weights correspond to lengths, center to center of bearings.

STEEL PLATE GIRDERS.
SAFE LOAD IN POUNDS, UNIFORMLY DISTRIBUTED.

		No. 1	G.			No. 1	G.	
	6 X84	Web Plan  X Flan  X Stiff  Fillers.	ge Ans	gles. ngles.	II &	% Web l %×% Fl %×% St % Filler		ngles. Angles.
Clear Span in feet.	Safe Load, including weight of Girder, for fiber strain of 16,000 lbs. per sq. in.	Safe Load, including weight of Girder, for fiber strain of 18,600 lbe. per sq. in.	Estimated weight of Girder.	Deflection.	Safe Load, including weight of Girder, for Aber strain of 16,000 lbs. per sq. in.	Safe Load, including weight of Girder, for fiber strain of 12,500 lbs. per eq. in.	Estimated weight of Girder.	Deflection.
14 15 16 17 18	148960 134760 126625 119385 112900	112065 104860 98480 94720 87720	1849 1941 2034 2126 2218	••••	115275 115190 114425 107880 102015	95775 94730 88965 83840 79235	1728 1808 1893 1978 2063	
19 20 21 22 28	107005 101715 96880 92470 88415	83085 78925 75130 71660 68475	2355 2447 2540 2632 2724	 .278 .305 .333 .363	96680 91885 87520 83535 79860	75050 71275 67840 64705 61880	2191 2276 2361 2447 2582	.278 .805 .833 .363
24 25 26 27 28	84635 81175 77970 74980 72195	65495 62775 60250 57890 55695	2855 2947 8089 8132 3224	.398 .426 .460 .494 .530	.76445 78810 70415 67710 65185	59125 56660 54875 52250 50265	2653 2739 2824 2909 2994	.894 .426 .459 .494
29 80 81 82 83	69545 67105 64810 62640 60595	53595 51675 49850 48140 46525	3354 3446 3539 3631 3728	.567 .606 .645 .686 .728	62785 60580 58505 56550 54595	48365 46620 44975 48480 41965	8116 8201 8286 8871 8456	.567 .605 .645 .686 .728
84 85 86 87 88	58680 56805 55065 58425 51860	44970 48515 42145 40885 89590	8850 8948 4085 4127 4220	.772 .817 .863 .910 .959	52915 51260 49695 48200 46785	40545 89240 87995 86810 85685	8575 8660 8745 8880 8915	.772 .816 .862 .909

The above values are found on the moments of inertia of the sections with a fiber strain of 16,000 lbs. and 12,500 lbs. respectively for steel; \(\frac{1}{2}\)' rivet holes deducted. Weights of girders include 13 inches of bearing at each end, stiffeners, fillers and rivet heads.

		No. 1	G.		No. 2 G.						
	6 ×314	Web Plan ×% Flan ×% Stiff Fillers,	ge Ans	gles. ngles.	5 V2	% Web I ×½ Fl ½×% St ½ Filler	ango A	ngles. Angles.			
Clear Span in feet.	Safe Load, including weight of Girder, for fiber strain of 16,000 lbs. per sq. in.	Safe Load, including weight of Girder, for fiber strain of 12,500 lbs. per sq. in.	Estimated weight of Girder.	Deflection.	Safe Load, including weight of Girder, for fiber strain of 16,000 lbs. per sq. in.	Safe Load, including weight of Girder, for fiber strain of 12,500 lbs. per sq. in.	Estimated weight of Girder.	Deflection.			
14 15 16 17 18	115400 108015 101495 95670 90460	89810 84015 78905 74340 70250	1598 1676 1753 1831 1909		105630 102400 96200 90685 85725	85120 79620 74760 70435 66545	1618 1698 1778 1857 1937				
19 20 21 22 23	85720 81465 77595 74040 70790	66530 63185 60145 57350 54790	2029 2107 2184 2262 2340	.277 .305 .333 .362	81225 77185 73495 70125 67025	62995 59825 56925 54275 51835	2054 2134 2214 2294 2373				
24 25 26 27 28	67745 64970 62390 59995 57755	52385 50200 48170 46285 44515	2454 2532 2609 2687 2765	.393 .425 .459 .493 .529	64130 61490 59040 56750 54630	49550 47470 45540 43740 42050	2490 2570 2650 2730 2809	.422 .456 .492 .529			
29 30 31 32 33	55620 53655 51805 50070 48430	42820 41275 39805 38430 87130	2878 2956 3034 3112 3190	.566 .605 .644 .685	52595 50725 48965 47305 45735	40445 38965 37575 36255 35015	2924 3004 3084 3164 3243	.607 .648 .691 .734			
34 35 36 37 38	46840 45360 43975 42645 41390	35870 34700 33595 32545 31540	3300 3378 3456 3534 3612	.771 .815 .861 .908 .957	44225 42825 41495 40235 39025	33815 32705 31645 30645 29685	3356 3436 3515 3595 3675	.826 .872 .928 .974 1.026			

The above values are found on the moments of inertia of the sections with a fiber strain of 16,000 lbs. and 12,500 lbs. respectively for steel; \$\frac{1}{2}\text{" rivet holes deducted. Weights of girders include 12 inches of bearing at each end, stiffeners, fillers and rivet heads.

STEEL PLATE GIRDERS.
SAFE LOAD IN POUNDS, UNIFORMLY DISTRIBUTED.

=								
		No. 2	G.			No. 2	G.	
	22 × 3 5 × 3	Web Pla	tes.	. !		% Web I	Plates.	
	5 ×3 8 ×24	X Flan	ge Ang	rles.	5 ×3 8 ×2	X% Fl	ange Ar	igles.
	24.	×4 Flan ×4 Stiff Fillers.	ener A	IIR ICE.	844×	%×% Sti % Filler	шенег д В.	ruRies.
Clear Eron in seet.	Cafer road, including Verson of Cirtler, for filter strain of 13,000 lbs. yer eq. in.	Safe Load, including weight of Girder, for fiber strain of 1,500 lbs. per sq. in.	weight ler.		including Firder, for 1 of 16,000 in.	Safe Load, including weight of Girder, for fiber strain of 13,500 lbs. per sq. in.	Estimated weight of Girder.	l
â	Str.	der			fincludi Girder, in of 16,	der fer	Ð,	1
ū	.45° 25	학을 걸다.		a	1101	<b>경우 교육</b>	žğ.	ا ا
5	Cafe and, Very of Caber fradi	Safe Load, incluweight of Girden fiber strain of 1 lbs. per sq. in.	Estimated of Gir	Deflection.	Safe Load, incl weight of Gird fiber strain of lbs. per eq. in.	or G	<u>\$</u> 5	Deflection.
-	, t 4	r str	o iii	8	Sam F	3## g	ä to	8
9	i son	edg Per ger	'sti	eg	Safe Load weight of fiber strai	Saga S	<u> </u>	뜋
0	GPGE	3 142	<u> </u>	<u> </u>	Ø ≱ ∉ ≅	92 ≥ ± 12	<u> </u>	<u> </u>
14 15	99240	77180	1512		88615	68915	1406	
15	02855	72185	1586		82925	<b>6444</b> 5	1474	
16	87220	67780	1659		77890	60510	1542	
17	82205	63845	1733		78410	56990	1610	
18	77715	60315	1807		69390	53830	1678	
19	73635	57105	1917	ll	65730	50960	1780	
20	69960	54000	1990		62450	48380	1848	.297
21	66615	51595	2064		59465		1916	.326
22 23	<b>6</b> 2560	49180	2138		56715	43875	1983	. 357
23	60750	46970	2212	.388	54210	41900	2051	.388
24	58120	44890	2321	.421	51855	40035	2154	.421
25	<b>5571</b> 5	43005	2895	.456	49710		2221	. 456
26	53490	41250	2469	.492	47720	36780	2289	.491
27	51495	39605	2543	.529	45865	85315	2357	.529
28	49485	38085	2616	.567	44185	33945	2425	.567
29	47635	36615	2724	.607	42475	32635	2525	.607
80	45940	35270	2798		40955	31425	2593	.648
81	44340	84010	2871	.690	39530	80300	2661	.690
82	42835	32815	2945	.734	38180	29230	2729	.734
83	41420	31690	8019	.780	86915	28225	2797	.779
84	40035	30595	8124	.826	85675	27235	2894	.825
35	38760	29580	3198	.874	84540	26340	2962	.873
36	37560	28630	3272	.923	33460		3030	.923
37	36415	27715	3346		32430			.973
38	35320	<b>2684</b> 0	3420	1.025	81455	23875	8166	1.025

The above values are found on the moments of inertia of the sections with a fiber strain of 16,000 lbs. and 12,500 lbs. respectively for steel; 1§" rivet holes deducted. Weights of girders include 12 inches of bearing at each end, stiffeners, fillers and rivet heads.

			No. 8	Gł.			No. 8	G.	
		20 × %	Web Pla	tes.	. 1		% Web_I	Plates.	_
		5 ×8	X% Flan	ge Ang ener Ai	gles.	5 X8	XX FI	ange A	ngles. Angles.
	- 1	21/4× 1/4	×% Stiff Fillers.			2½×	XXX Sti Filler	В.	
	듛	9 1 0 9 1 0	for 500	bt		for 600,	20.00	pt	
	Clear Span in feet.	Safe Load, including weight of Girder, for fiber strain of 16,000 lbs. per aq. in.	검실	Estimated weight of Girder.		Safe Load, including weight of Girder, for fiber strain of 16,000 lbs. per sq. in.	Safe Load, including weight of Girder, for fiber strain of 19,500 lbs. per sq. in.	weight der.	l
	7	d Ford	Safe Load, incl weight of Gird fiber strain of lbs. per sq. in.	ted weig Girder.	ایا	Safe Load, includ weight of Girder, fiber strain of 16, 1bs. per sq. in.	Safe Load, incl weight of Gird fiber strain of lbs. per sq. in.	ted wei Girder.	ی ا
	8	4 2 4 5	40 4 8	36	[ 5]	40 4 8	45 2 3	32	5
	20	of the Period	Part P	o B	ect	33.5	S # E	a to	8
	9	a per se	Safe Load, weight of ( fiber strais lbs. per sq.	138	Deflection.	Safe Load, weight of G fiber strain	Safe Load, weight of ( fiber strain lbs. per sq.	Estimated of Gird	Deflection.
_	_	- FGS	20 F CI CI	<u> </u>		Ø F Q Z	Ø F CI CI	<u> </u>	<u> </u>
	14	96800	75280	1548		87685	68185	1443	
	15	90575	70405	1626		82045	63765	1515	
	16	85085	66095	1703		77055	59835	1586	
_	17 18	80180 75795	62240 58805	1780 1857		72625 68630	56875	1657 1728	
•	- 1						53240		
	19	71795	55655	1967		65020	50390	1881	
	20	68205	52835	2044	.328	01760	47840	1902	.328
	21	<b>6494</b> 0 <b>6194</b> 0	50260 47900	2121 2199	.360 .393	58795 56085	45505 43365	1973	.859
	22 23	59195	45745	2276	.428	53585	41405	2044 2116	.428
	24	56625	48715	2386	.464	51260	39560	2218	.464
	25	54275	41855	2463	.502	49180	87880	2290	.502
	26 27	52100 50065	40140 38535	2540 2617	.542 .583	47160 45820	36320 34870	2861 2482	.540
	28	48175	87085	2694	.625	43595	38505	2508	.625
	- 1								
	29	46365	85605	2804	.669	41955	32205	2606	.668
	30 31	44700 43140	84290 33050	2881 2959	.714 .761	40445 39030	81015 29890	2677 2748	.714
	32	41665	81885	3036	.809	87690	28830	2820	.809
	33	40275	30775	3113	.859	36430	27830	2891	.858
		88920	29700	3220		35200	26850	2990	.909
	84 85	87 <b>6</b> 75	28715	3297	.910 .963	34070	25950	2990 3061	.962
	36	36495	27765		1.017	32995	25085	3133	1.016
	37	85870	26870	8451		31975	24275	8204	1.072
	38	84290	26010		1.180		23505	3275	1.129

The above values are found on the moments of inertia of the sections with a fiber strain of 16,000 lbs. and 12,500 lbs. respectively for steel; ‡8" rivet holes deducted. Weights of girders include 12 inches of bearing at each end, stiffeners, fillers and rivet heads.

		No. 8	Gł.		1	<b>N</b> o. 4	ı G.		
	5 ×8	Web Pla ×% Flan ×% Stiff Fillers.	ge Ang	des. ngles.	5 ×8	% Web Plates. X¼ Flange Angles. ¼X% Stiffener Angles. ¾ Fillers.			
Clear Span in feet.	Safe Load, including weight of Girder, for fiber strain of 16,000 lbs. per sq. in.	Safe Load, including weight of Girder, for fiber strain of 12,500 No. per eq. in.	Estimated weight of Girder.	Deflection.	Safe Load, including weight of Girder, for fiber strain of 16,000 lbs. per eq. in.	Safe Load, including weight of Girder, for fiber strain of 12,500 lbs. per sq. in.	Estimated weight of Girder.	Deflection.	
14 15 16 17 18	78180 78145 68700 64735 61180	60800 56845 58860 50245 47460	1840 1405 1470 1585 1600		76545 71610 67250 63660 59870	59505 55640 52210 49160 46410	1878 1442 1511 1579 1648	•••••	
19 20 21 22 23	57945 55040 52395 49970 47745	44905 42620 40545 88630 86875	1696 1761 1826 1892 1957	.327 .359 .392 .427	56695 53850 51250 48870 46680	43915 41670 89630 87750 86030	1743 1812 1880 1949 2018	.865 .400 .437 .476	
24 25 26 27 28	45655 43760 41995 40350 38815	85225 83730 82385 81030 29825	2053 2118 2183 2248 2313	.464 .502 .541 .582 .624	44635 42765 41035 39420 37910	34415 82935 81565 80290 29100	2115 2184 2253 2821 2890	.517 .559 .603 .648 .695	
29 30 31 32 33	87850 86005 84730 88585 82410	28660 27585 26580 25635 24740	2408 2473 2538 2603 2668	.668 .713 .760 .808 .857	86475 35150 33900 32720 31610	27945 26900 25910 24980 24090	2484 2552 2621 2690 2758	.744 .794 .846 .900 .955	
34 35 36 37 38	81820 80800 29335 28480 27555	23870 23060 22295 21560 20865	2959	.909 .961 1.015 1.071 1.128	80585 29585 28585 27690 26830	20970	2855 2924 2993 3061 3130	1.018 1.071 1.181 1.198 1.257	

The above values are found on the moments of inertia of the sections with a fiber strain of 16,000 lbs. and 12,500 lbs. respectively for steel; 14" rivet holes deducted. Weights of girders include 12 inches of bearing at each end, stiffeners, fillers and rivet heads.

		No. 4	Gł.			No. 4	G.	
	5 ×8 8 ×24	Web Pla ×% Flan ×% Stiff Fillers.	ge Ang	des.	4 ×3	% Web F ×% Fl %×% Sti % Filler	ange Ai	ngles. Angles.
Clear Span in feet.	Safe Load, including weight of Girder, for fiber strain of 16,000 lbs. per sq. in.	Safe Load, including weignt of Girder, for fiber strain of 12,500 lbs. per sq. in.	Estimated weight of Girder.	Deflection.	Safe Load, including weight of Girder, for fiber strain of 16,000 lbs. per sq. in.	Safe Load, including weight of Girder, for fiber strain of 12,500 lbs. per sq. in.	Estimated weight of Girder.	Deflection.
14 15 16 17 18	68170 63765 59875 56410 58300	52980 49525 46475 48750 41810	1271 1883 1896 1459 1521		58900 55095 51725 48720 46020	45760 42775 40125 37770 35650	1179 1287 1294 1352 1409	
19 20 21 22 23	50470 47925 45615 43490 41540	39080 37075 35255 33580 32040	1610 1678 1735 1798 1861	.364 .400 .440 .476	48306 41360 89350 87515 35825	33506 31980 30400 28955 27615	1494 1552 1609 1667 1724	.358 .393 .430 .468
24 25 26 27 28	39710 38045 36505 35060 33710	30600 29285 28065 26920 25860	1951 2014 2076 2139 2202	.516 .558 .602 .648 .694	34240 32795 31455 30200 29080	26360 25215 24155 28170 22240	1809 1866 1924 1981 2089	.508 .550 .593 .637 .684
29 30 31 32 33	32430 81250 30135 29085 28090	24830 23900 23015 22175 21890	2289 2351 2414 2477 2539	.743 .794 .846 .899 .955	27920 26890 25925 25015 24150	21350 20530 19765 19085 18360	2121 2178 2236 2293 2351	.732 .781 .832 .885 .939
34 85 36 37 38	24580	20620 19910 19235 18590 17980	2755 2818	1.011 1.070 1.130 1.192 1.256	23315 22540 21800 21105 20435	15925	2434 2492 2549 2607 2664	.996 1.053 1.112 1.173 1.236

The above values are found on the moments of inertia of the sections with a fiber strain of 16,000 lbs, and 12,500 lbs. respectively for steel; 18" rivet holes deducted. Weights of girders include 12 inches of bearing at each end, stiffeners, fillers and rivet heads.

Distance Center to Center of Bearings, in Feet.			30"×%" Web Plate.	12"×%" Flange Plates. 5"×3½"×½" Angles.			33"X 1/4" Web Plate.	5"×3½"×½" Angles.
Distance Center to Bearings, in	Safe Load, including weight of girder,	Weight of girder, in tons.	Increase in safe load for 15" in- crease in thickness of flange plates.	Increase in weight of girder for 1,8" increase in thickness of flange plates.	Safe Load, including weight of girder.	Weight of girder, in tons.	Increase in safe load for 15" in- crease in thickness of flange plates.	Increase in weight of girder for 15" increase in thickness of flange plates.
20	81.18	1.62	4.00	.05	91.71 87.34	1.70	4.40	.05
21 22 23 24 25 26 27 28 29	77.32 73.80	$\frac{1.69}{1.76}$	3.80	.05 .06	87.34	1.77 1.84	4.20 4.00	.05
00	70.60	1.86	9.47	.06	20.04	1.04	9.00	.00
94	67.66	1.93	9 99	.00	83.37 79.74 76.42 73.36 70.54 67.93 65.50 63.25 61.14 59.16 57.32 55.58	1.95 2.02 2.09 2.17 2.24 2.31 2.42 2.49 2.56	9 87	.06 .06 .07 .07 .07 .07 .08 .08 .08 .08
95	64.95	2.01	2 10	.06 .06 .07 .07	72 26	2 00	9.59	06
26	62.45	9 07	8.07	07	70.54	2 17	3 39	07
27	60.14	2.14 2.21 2.31 2.38	2.96	07	67.93	2.24	3.26	.07
28	57.99	2.21	2.85	.07	65.50	2.31	8.15	.07
29	55.99 54.12	2.31	2.75	.07	63.25	2.42	3.03	.07
30 31	54.12	2.38	2.66	.07 .08 .08 .08 .08 .08	61.14	2.42 2.49 2.56 2.64 2.71	2.94	.08
31	52.38	2.40	2.57	.08	59.16	2.56	2.85	.08
32	50.74	2.52	2.50	.08	57.32	2.64	2.75	.08
32 33 34	49.20	2.59	2.42	.08	55.58	2.71	2.67	.08
34	47.76	2.66	2.34	.09	53.94	2.78	2.59	.09
35	46.39	2.73	2.28	.09	52.40	2.85	2.52	.09
36 37 38	45.10	2.83	3.63 3.47 3.19 3.07 2.96 2.85 2.75 2.50 2.42 2.28 2.22 2.16 2.10 2.05	.09	50.95	2.96	2.45	.09
37	43.88 42.78	2.90	2.16	.09 .10 .10	49.57	3.03	2.38	.09
38	42.78	2.97	2.10	.10	48.27	$\frac{3.11}{3.18}$	2.31	.10
39 40	41.63		2.10 2.05 2.00	.10	53.94 52.40 50.95 49.57 48.27 47.03 45.85	3.18	3.83 3.67 3.52 3.39 3.15 8.03 2.94 2.75 2.67 2.59 2.45 2.38 2.31 2.25 2.25	.09 .10 .10
40	40.59	5,11	2.00	.10	45.85	5.25	2.21	.10

The above values are founded on the moments of inertia of the sections using a maximum fiber strain of 18,000 lbs. per square inch for steel; \(\frac{1}{4}\)'' rivet holes in both flanges deducted. Weights of girders correspond to lengths center to center of bearings and include rivet heads, stiffeners and fillers.

STEEL PLATE GIRDERS.
SAFE LOADS IN TONS, UNIFORMLY DISTRIBUTED.

Distance Center to Center of Bearings, in Feet.			36"×½" Web Plate.	12" ×%" Fininge Finices. 5"×3%"×%" Angles.	42"×%" Web Plate.  14"×%" Flange Plates.  6"×6"×%" Angles.			
Distance Cent Bearings	Safe Load, including weight of girder.	Weight of girder, in tons.	Increase in safe load for 15" increase in thickness of flange plates.	Increase in weight of girder for $\frac{1}{18}$ " increase in thickness of flange plates.	Safe Load, including weight of girder.	Weight of girder, in tons.	Increase in safe load for th' in- crease in thickness of flange plates.	Increase in weight of girder for $\frac{1}{48}$ " increase in thickness of flange plates.
20 21 22 23 24 25 26 27 28 29 30 31 33 34 35 36 37 38 39 40	102.57 97.67 93.28 89.18 85.46 82.04 78.88 75.96 70.73 68.37 66.16 64.10	2.68 2.75		.05 .05 .06 .06 .06 .07 .07 .07 .08 .08 .08 .09 .09 .09	152.54 145.28 138.68 132.65 127.12 122.04 117.34 113.00 108.97 105.20 101.70 98.42 95.34	3.71 3.88 4.00 4.12 4.23	6.71 6.39 6.09 5.88 5.58 5.16 4.97 4.78 4.63 4.48 4.82 4.20	.06 .06 .07 .07 .07 .08 .08 .08 .09 .09 .10 .10 .11 .11 .11
33 34 35 36 37 38 39 40	62.16 60.33 58.60 56.98 55.44 53.98 52.59	2.82 2.89 2.98 3.09 3.16	2.47	.08 .09 .09 .09 .09 .10 .10	92.45 89.74 87.17 84.74 82.46 80.29 78.23 76.27	4.59 4.76 4.87 4.99	3.94 3.83 8.73 3.62 8.58	.10 .10 .10 .11 .11 .11 .12 .12

The above values are founded on the moments of inertia of the sections using a maximum fiber strain of 13,000 lbs. per square inch for steel; †?" rivet holes in both flanges deducted. Weights of girders correspond to lengths center to center of bearings and include rivet heads, stiffeners and fillers.

# STEEL BOX GIRDERS. SAFE LOADS IN TONS, UNIFORMLY DISTRIBUTED.

Distance Center to Center of Bearings, in Feet.	<b>4</b>		30"×55" Web Plates.	16"×%" Flange Plates. 3½"×3½"×5½" Angles.	Φ	b (	33'X's" Web Plates.	30"×15" Flange Plates.
	Safe Load, includ- ing weight of girder.	Weight of girder, in tons.	Increase in safe load for 15" in- crease in thickness of flange plates.	Increase in weight of girder for 4" increase in thickness of flange plates.	Safe Load, including weight of girder.	Weight of girder, in tons.	Increase in safe load for 'F'' in- crease in thickness of flange plates.	Increase in weight of girder for 1,6" in- crease in thickness of flange plates.
20 21 22 23 24 25	97.59 92.94 88.72 84.86 81.32	2.13 2.23 2.32 2.45 2.54	5.73 5.46 5.20 4.98 4.78	.07 .07 .08 .08 .08 .09	130.2 124.0 118.3 113.2 108.5	$\frac{2.66}{2.80}$	7.95 7.58 7.22 6.90 6.62	.09 .09 .09 .10
25 26 27 28 29	84.86 81.32 78.07 75.07 72.29 69.70 67.30	2.64 $2.74$ $2.83$ $2.93$ $3.06$	4.98 4.78 4.59 4.41 4.25 4.10 3.96	.09 .09 .09 .10	93.0	3.03 $3.14$ $3.25$ $3.36$ $3.50$	6.35 6.12 5.89 5.67 5.48	.09 .10 .10 .11 .11 .12 .12 .12 .13 .13
30 31 32 33	65.06 62.96 61.00 59.14	3.16 $3.25$ $3.35$ $3.50$	3.82 3.70 3.58 3.48	.10 .11 .11	86.8 84.0 81.4 78.9	3.61 $3.72$ $3.83$ $3.95$	5.29 5.13 4.97 4.82	.14
34 35 36 37 38	55.76 54.22 52.75	3.54 3.64 3.76 3.86 3.95	3.38 3.28 3.18 3.09 3.02	.12 .12 .12 .13 .13	76.6 74.4 72.3 70.4 68.5	4.06	4.67 4.53 4.41 4.30 4.18	.14 .15 .15 .16 .16
39 40	50.04 48.80	4.05	2.94 2.86	.13	66.7	4.65 4.76	4.07 3.97	.17

The above values are founded on the moments of inertia of the sections using a maximum fiber strain of 18,000 lbs. per square inch for steel; \(\frac{1}{2}\)\s^{\pi} rivet holes in both flanges deducted. Weights of girders correspond to lengths center to center of bearings and include rivet heads, stiffeners and fillers.

STEEL BOX GIRDERS.
SAFE LOADS IN TONS, UNIFORMLY DISTRIBUTED.

Distance Center to Center of Bearings, in Feet.			#	34"×½" Flange Plates. 4"×3½"×½" Angles.	1d-				
Distance Cent Bearing	Safe Load, including weight of girder.	Weight of girder, in tons.	Increase in safe load for 14" in- crease in thickness of flange plates.	Increase in weight of girder for \( \frac{1}{4} \) increase in thickness of flange plates.	Safe Load, including weight of girder.  Weight of girder, in tons.	Increase in safe load for 14" in- crease in thickness of flange plates.	Increase in weight of girder for ½" increase in thickness of flange plates.		
201223456728901222224567289012222245672890122222222222222222222222222222222222	184.9 176.2 168.2 160.8 154.2 148.0 142.4 137.0	2.92 3.06 3.19	10.59 10.10 9.64 9.22 8.84 8.18 7.85 7.57 7.31 7.06 6.88 6.63 6.24 6.06	.10 .11 .11 .12 .13 .18 .14 .14 .15 .15 .16 .16 .17 .17 .18 .18 .19 .20	278.53.76 274.83.96 262.34.18 251.04.34	3 15.80 5 15.05 6 14.37 4 18.74 7 12.64 7 12.16 4 11.70 1 1.29	.18 .78 .14 .15 .16 .17 .17 .18 .19 .19 .20 .20 .21 .22 .23 .22 .23 .24 .24 .26		
23	160.8	3.36	9.22	.12	251.04.34	18.74	.15		
24	154.2	8.49	8.84	.12	I 940 514 51	13.17	.15		
25	148.0	8.68	8.48	.13	230.94.69	12.64	.16		
26	142.4	8.76	8.18	.18	230.94.69 222.04.89 213.85.04	12.16	.17		
27	187.0	3.89	7.85	.14	213.85.0	11.70	.17		
28	107.1	$\frac{4.03}{4.15}$	7.57	.14	206.25.2 199.05.4	11.29	.18		
20	132.1 127.6 123.3	4.10	7.51	1.10	199.05.4	11.29 11.29 10.91 10.54 10.21 9.88 9.88	10		
81	110 8	4.45	A 88	18	192.45.61 186.25.78 180.35.98	10.04	20		
82		4.60	6.63	16	180.35.9	9 88	20		
88	112.1	4.74	6.43	17	174.96.1	9.58	.21		
84	108.8	4.87	6.24	.17	169.86.2	ย ห.ณเ	.22		
85	105.7	5.00	6.06	.18	164.96.4	9.03	.22		
36	105.7 102.8	5.17	5.90 5.74 5.58 5.44	.18	160.86.6	9.03 8.78	.28		
87	100.0 97.4	5.31	5.74	.19	156.06.8	8.54 8.32 8.11	.24		
88	97.4	5.44 5.58	5.58	.19	151.96.9	8.32	.24		
89	94.9	5.58	5.44	.20	148.07.20	8.11	.25		
40	92.5	5.71	5.30	.20	144.8 7.3	7.91	.26		

The above values are founded on the moments of inertia of the sections using a maximum fiber strain of 18,000 lbs. per square inch for steel; ††" rivet holes in both fianges deducted. Weights of girders correspond to lengths center to center of bearings and include rivet heads, stiffeners and fillers.

SAFE LOAD IN TONS OF 2,000 LBS. FOR 16" LARIMER ALL STEEL COLUMNS.

 Rivets in Web and Flange. Allowed strain per square inch =  $\begin{cases} 12,000 \text{ lbs. for lengths of 90 radii} \\ 17,100-57 \frac{l}{r} \text{ for lengths over 90 radii.} \end{cases}$ 

<b>-8</b> -	C	<b>,</b>	51. 511.	51. 51.
	æ	17.4"	17 <sub>1</sub> 4" 17"	164 <b>8"</b> ·
	V	žė.	16 <sub>78</sub> " 16"	1533′′ 152″
•	32 and under.	533	210 195	179
LENGTH OF COLUMN IN FEET.	34	328	200 180 180	174 165
	98	220	198 184	169
	88	214	192 178	164 155
	40	808	186 173	160 151
Minimum Redius	Sq. in. Inches.	8.38	4.10	4. 4. 8. 83
Sectional Area of Column.	Sq. in.	<b>8</b> <b>4</b> .	88.7 88.7 8.8	8 8 1.
Weight per foot of Column without Attings.	Lbs.	131.25	121.25 111.25	15 æ. 8i æ.
Weight per foot of Filler.	Lbs.	10.5	10.5 10.5	10.5
Weight per foot of Single Beam.	Lbs.	8	\$ 3	<b>4 3</b>
Section No. of Beam.	No.	S H	77	11

SAFE LOAD IN TONS OF 2,000 LBS. FOR 13" LARIMER ALL STEEL COLUMNS.

Allowed strain per square inch –  $\begin{cases} 12,000 \text{ lbs. for lengths of 90 radii or under.} \\ 17,100 - 57 \frac{l}{r} \text{ for lengths over 90 radii.} \end{cases}$ 

Rivets in Web and Flange.

<b>►8</b>	٥		5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
<b>a</b>	Д	14 /3 " 18 <del>  4</del> "	13 ta." 13 ta."
	٧	13" 12 <b>ţ</b> "	12 <b>33</b> " 12 <b>5</b> " 124 <b>8</b> "
	24 and under	178	142 142 130
	88	178 161	157 141 180
LENGTH OF COLUMN IN FEET.	88	170 156	151 136 126
	8	164 151	146 182 122
	왏	158 145	140 127 118
	ಹ	152	135 123 113
_	88	146 135	123
	88	150 128	221 132 105
	8	134 124	119 108 101
Minimum Radius of Gyration.	Sq. in. Inches.	3.40	3.36 3.42 3.51
Bectional Area.	Sq. in.	81 88 1- 8:	8 8 a
Weight per foot of Column without fittings.	Lbs.	101.88 83.18	22 22 25 25 25 25 26 25
Weight per foot of Filler.	Lbs.	10.5	10.5 10.5 10.5
Weight per foot of Single Beam.	Lbs.	<b>å</b> 3	88 88 5. 18
Section No. of Beam.	Ž.	5.5	<b>999</b>

Web and Flange.

# BAFE LOAD IN TONS OF 2,000 LBS. FOR 11" LARIMER ALL STEEL COLUMNS.

12,000 lbs. for lengths of 90 radii or under.  $17,100 - 57 \frac{t}{r}$  for lengths over 90 radii. Allowed strain per square inch -

LENGTH OF COLUMN IN FEET.

> of Gyration. Minimum Radius of Column. Sectional Area

without Attings.

Weight per foot of Column

of Filler. Weight per foot

of Single Beam.

Weight per foot

Вевт.

Section No. of

Lbs.

Lbg.

Lbs.

Š

10.5 10.5

8 8

B-7

B-7

5	

!	4.4	a 8
B	1118"	4" Rivets in Web and Flang
4	10[" 10 <b>9</b> ["	# Web #
4 22 and under	128 107	
24	118	E I
8	113 98	TONS OF 2,000 LBS, FOR 10" LARIMER ALL STEEL COLUMNS.
88	108 24	<u>.</u>
30	<u>86</u>	R 10
왏	<b>8</b> 8 <b>8</b>	
\$	88	LBS.
88	4388	800
<b>88</b>	73	2,C
40	85	8 O
		Z
Inches	8. 8. 8. 8.	N T
3q. in. Inches	20.8	90

434

ge.	ပ	**
Web and Flange.	В	1018" 1018"
Web a	¥	92
	20 and under	108 108
	ន	101
	22	88

1		
	22	\$ &
	88	888
	88	78 78
	30	88.47
COLOMINA.	88	72
91555	28	85 æ
	<b>%</b>	88
414	Sq. fn. Inches.	2.57
	Sq. fn.	18.1
	Lbs.	61.25 53.25
	Lbs.	10.5
	Lbs.	0.12

SAFE LO! 61.25

Š.

77

SAFE LOAD IN TONS OF 2,000 LBS. FOR 9" LARIMER ALL STEEFL COLUMNS.

". Rivets in Web. Allowed strain per square inch  $-\begin{cases} 12,000 \text{ lbs. for lengths of 90 radii} \\ 17,100-57-\frac{t}{r} \text{ for lengths over 90 radii.} \end{cases}$ 

-		٥	44
		В	918 918 92
		V	
		18 and under	91 88 75
		8	865
	Ę	81	8558
	OF COLUMN FEET.	24	523
		88	74 67 61
	ENGTH	88	888
	ā	8	282
		엃	51
		\$	8824
		8	884
	Minimum Radius of Gyration.	Sq. in. Inches.	20 20 30 44 41
	Sectional Area of Column.	Sq. in.	51 52 52 4.93
	Weight per foot of Column without attings.	Lbg.	88.0 47.0 0.0
	Weight per foot of Filler.	Lbs.	0.00
	Weight per foot of Single Beam.	Lbs.	22.25 22.25 17.71
:	Soction No. of Beam.	No.	9 0 0 H H H

nge.	C	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
§" Rivets in Web and Flange.	В	20.20
₩eb •	¥	71.8"
ALL	16 and under	81 72 64
Œ	18	888
FOR 8" LARIMER	83	242
7	প্ত	282
•	\$	888
6	8	8884
LBS.	88	234
25 25	8.	<b>\$</b> 44
§2	22	4 <del>5</del> 45
F 2	22	3 % % \$
8 O	88	888
LOAD IN TONS OF 2,000 L STEEL COLUI	Lbs. Lbs. Sq. in. Inches.	2.10 2.12 2.13
AD I	Sq. in.	13.6 12.1 10.6
ב רכ	Lbs.	46.5 41.5 36.5
SAFE	Lbs.	6.0 6.0 6.0
	Lbs.	B-10 20.0 B-10 17.5 B-10 15.0
	No.	B-10 B-10

SAFE LOAD IN TONS OF 2,000 LBS. FOR 7" LARIMER ALL STEEL COLUMNS.

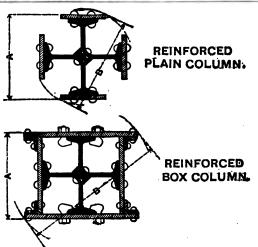
Web and Flange. Allowed strain per square inch =  $\begin{cases} 12,000 \text{ lbs. for lengths of 90 radii} \\ 17,100 - 57 \frac{l}{r} \text{ for lengths over 90 radii.} \end{cases}$ 

1	Ö	8.4°.	Web.	O	
1	æ	72"	s in Wel	æ	,,, e,
	٧	641°	" Rivets in I" Rivets in	4	518,
	14 and under.	62 54		12 and under.	<b>55</b>
	16	52	E 3	14	<b>48</b>
Z S	18	24	LARIME	16	<del>2</del> 88
Corr	&	84		<b>22</b>	#8
OF COLUMN FEET.	83	47	G	8	88 34
LENGTH	22	<b>₫%</b>	P. S	81	28
LE	8	88	OF 2,000 LBS. STEEL COLUMNS	2	88
	88	38 55	80 100 100	88	88
	8	88	EL.0	88	88
	88	32	STE	8	178
Minimum Radius of Gyration.	Inches.	1.86	TONS	Inches.	3.1.58
Sectional Area of Column.	Sq. in. Inches	10.5	N 0	Sq. in. Inches.	7.5
Weight per foot of Column without attings.	Lbs.	8 8	2	Lbs.	≅ <b>%</b>
Weight per foot of Filler.	Lbs.	• •	SAFE LOAD	Lbs.	••
Weight per foot of Single Beam.	Lbs.	14.75	-	Lbe.	82.00 57.0
Section No. of Beam.	No.	B-11 B-11		No.	8 8 81 81

# SAFE LOAD IN TONS OF 2,000 LSS. FOR REINFORCED LARIMER ALL STEEL COLUMNS.

Allowed Strain per Square Inch=12,000 Lbs.

Size of I Beam.	Weight per foot Weight per foot Weight per foot of Filler.		Weight per foot of Column.		Sectional Area of Column.	Sectional Area of Column. Safe Load of Column 36 foot and under.		Size of Column.		
In.	Lbs	Lbs		Lbs.	Sq.In.	Tons.	A	В		
15	60	101/2	4 Pl. 7½"×%"	198.17	57.13	344.2	17%"	18%"		
15	60	1014	4 Pl. 7%"×%"	211.90	60.88	365.7	17%"	19"		
15	60	1016	4 Pl. 9"×34"	226.24	65.38	393.7	17%"	19%"		
15	60	101/2	4 Pl. 9"×%"	245.70	69.88	420.7	17%"	19%"		
15	60	101/2	14L2%"X2%"X7"	279.85	80.35	482.5	16%"	26%"		
15	60	101/4	14 L214"X214" 74"	296.18	86.36	518.5	16%"	2618"		
15	60	101/2	2 Pl. 15%"×%" 2 Pl. 22%"×%" 4 L 2½"×2½"×½"	332.99	95.90	575.8	17%"	2716"		
15	60	101/4	2 Pl. 15%"×%" 2 Pl. 23%"×%" 4 L24"×24"×4"		105.55	633.7	17%"	27%"		



# SAFE LOADS, IN TONS OF 2,000 LBS., FOR

# HOLLOW CYLINDRICAL CAST IRON COLUMNS.

Outside dlam., inches.	Thickness of Metal.	LENGTH OF COLUMNS, IN FEET.								Sectional Area, inches.	ght, lbs., of nns per foot length.	
Ont	Th	8	10	12	14	16	18	20	22	24	Sect	Weight, l
66 66 66 77 77 88 88 9 9 9 9 9 100 101 111 111 112 112 113 113 113 113 114 114 114 115 115 115	11111111111111111111111111111111111111	101.4 123.8 148.7 162.7 114.8 189.9 163.5 186.7 206.6 128.0 156.4 128.0 156.4 172.8 203.7 141.2 231.6 221.6	99.6 (116.7 (130.5 (16.7	28.8 32.8 36.5 40.1 38.5 49.3 54.3 48.6 62.5 75.5 58.9 76.2	83.6 118.6 118.6 118.6 118.6 118.6 118.6 157.5 175.1 159.0 181.1 159.7 159.0 181.1 159.7 159.0 191.4 159.7 159.7 159.7 159.7 159.8 118.6 157.5 169.7 128.6 169.7 128.6 169.7 128.6 169.7 128.6	24.7.6 30.4 30.4 42.8 38.9 42.8 38.9 42.8 38.9 42.8 42.8 42.8 42.8 42.8 42.8 42.8 42.8	114 .6 84 .8 103 .3 1120 .8 1152 .6 1152 .6 1150 .2 1150 .2 1160 .4 1178 .9 118 .1 1183 .9 205 .5 1125 .9 1154 .4 1181 .7 207 .6 232 .4 1171 .5	23.0 6 33.7 41.4 49.2 41.2 41.2 41.2 41.2 41.2 41.2 41.2 41	37.3.44.9.37.5.48.4.68.7.7.6.8.6.7.7.6.8.6.7.7.6.8.6.7.7.3.4.4.85.6.7.7.3.4.10.4.1.118.3.110.5.2.11.118.3.110.5.2.11.118.3.110.5.2.11.118.3.118.3.118.	94.2 26.7 26.7 33.6 40.5 34.1 44.1 44.1 45.2 62.0 55.5 67.7 89.1 89.5 96.2 115.1 1134.3 1171.8 1171.	39.9 28.3 34.4 40.1 45.4 40.1 45.4 49.5 56.9 634.6 49.2 561.9 69.1 568.9 69.1 46.4 46.4 46.4 46.4 46.4 46.4 46.4 46	26. 98 38. 56. 49 49. 00 53. 77 55. 59 60. 68 67 60. 68 67 110. 22 110. 22 110. 24 110. 24 110. 25 110. 25 110

A N	SPAM.	Safe load 19q 11 exaups	18	14	10	œ	1
DIFFERENT	7, 0, 1	Safe load per sheet between supports.	284	808	162	128	
	SPAN.	Safe load per per square ft.	જ્ઞ	18	14	=======================================	
HEE .	% O,	Safe load per sheet between supports.	331	236	189	149	
	SPAN.	Safe load per per square ft.	37	8	21	16	
CORRUGATED	,0 A	Safe load per sheet between atropouts.	388	284	227	178	
FOR CORR	SPAN.	baof elas req square ft	57	41	ee	36	
	4, 0, 8	Safe load per sheet between supports.	497	355	288	888	
SPANS AND	SPAN.	Safe load per per square ft.	102	73	28	46	
111	3, 0,	Safe load per sheet between supports.	663	473	379	297	
FOUALLY	10	Weight Wolf of the original of the original of the original of the original	2.16	1.54	1.23	.97	-
Z C	tat.	q tdgləW tool etaupa	1.97	1.40	1.12	88.	
E LOAD	uļ	Thickness inches.	.049	.086	980.	.032	
8 7 7	.9: -3:uj:	No. by Birn ham gaug	18	8	8	22	-

Sheets are 233" inches wide before, and 28" wide after corrugating. There are 38 corrugations in a sheet.
Sheets can be rolled any length to 10' 0".
It is not advisable to use over 6' 0" clear spans on roofs.

### WOODEN BEAMS.

Table of safe quiescent loads for horizontal rectangular beams of white pine or spruce one inch broad, supported at both ends, the load being equally distributed over the span.

N.N. EES			1.7	DEPT	H OF	ВЕАМ	IN IN	CHES.	1		
SPAN IN FEET	6	7	8	9	10	11	12	13	14	15	16
5	800	1090	1420	1800	2220	2690	3200	3750	4350	5000	5690
6	670	910	1180	1500	1850	2240	2670	3130	3630	4170	4740
7	570	780	1010	1290	1590	1920	2280	2680	3110	3570	4060
8	500	680	890	1120	1390	1680	2000	2350	2720	3130	3560
9	440	600	790	1000	1210	1490	1780	2090	2420	2780	3160
10	400	540	710	900	1110	1340	1600	1880	2180	2500	2840
11	360	490	650	820	1010	1220	1450	1710	1980	2270	2590
12	330	450	590	750	930	1120	1330	1560	1810	2080	2370
13	310	420	550	690	850	1030	1230	1440	1680	1920	2190
14	290	390	510	640	790	960	1140	1340	1560	1790	2030
15	270	360	470	600	740	900	1070	1250	1450	1670	1900
16	250	340	440	560	690	840	1000	1170	1360	1560	1780
17	230	320	420	530	650	790	940	1100	1280	1470	1670
18	220			500	620	750	890	1040	1210	1390	1580
19	210		380	470	590	710	840	990	1150	1320	1500
20	200	270	360	450	560	670	800	940	1090	1250	1420
21	190	260	340	430	530	640	760	890	1040	1190	1350
22	180	250	320	410	500	610	730	850	990	1140	1290
23	170	240	300	390	480	580	700	810	950	1090	1230
24	160	230	290	370	460	560	670	780	910	1040	1180
25	160	220	280	350	440	540	640	750	870	1000	1130
26	150	210	270	340	420	520	610	720	840	960	1090
27	150	200	260	330	400	500	590	690	810	920	1050
28	140		250	320	490	480	570	670	780	890	1010
29	140	190	250	310	380	460	550	650	750	860	980
30	130	180	240	300	370	450	530	630	730	830	950

This table has been calculated for extreme fiber strain of 1000 lbs. per square inch, giving a safety of 6 in ordinary building timber of fair quality.

Oak and yellow pine will carry a load one-fourth greater.

When more accuracy is required the weight of the beam itself must be deducted.

Care must be taken to let the beams rest for a sufficient distance on their supports to guard against crushing at the ends, especially in placing very heavy loads upon short, but deep and strong beams.

# SAFE LOADS IN TONS OF 2,000 LBS. FOR SINGLE BEAM COLUMNS.

Assumed strain per square inch—12,500 lbs. Reduced by Gordon's formula.

P of	og p				LENG	er in ]	EET.					
Depth of Beam.	Weight per foot.	10	12	14	16	18	20	22	24	26	28	80
24 24	100 80	148 117	135 110	124 102	118 94	102 86	98 78	84 71	76 65	70 59		49
20 20 20	100 80 64	151 128 94	140 114 86	129 105 78	117 97 70	108 89 63	98 81 57	89 74 51	82 67 46	74 62 42		62 52
15	100	149	138 111	126	115	105	95	86	79	71	62 58	
15 15 15	80 60 42	120 87 58	80 52	102 72 46	98 66 41	85 59 <b>86</b>	77 58 32	70 48 28	48	58 89		
12 12	55 40	74 54	66 50	59 44	52 39	46 85	41 81	36 28				
12 10	811 40	42 49	97 48	88 87	29 82	26 28	28 25	20	• • •	• • •		
10	25 35	82 41	28 85	25 30	22	19 23	17		• • • •			
8	21 251	26 28.2		20 20.8	17 17.8			• • •	• • • •			• • •
8 7 7	17 <del>1</del> 20	20.9 21.2	17.9		12.8			• • • •	• • •	• • •	• • •	
6	15 17 <del>1</del>	16.6 17	15.1	11.8				• • •	• • •			
6 5	12 <del>]</del> 14 <del>]</del>	12.7 18.5	11	9 9.1				• • •				
5 4	9 <del>1</del> 101	9.2 8.7	7	6.8				• • •	• • •			
4 8	7 <u>1</u>	6.4 5.6						• • •	• • •		 	
8	7	4.2				<u> </u>	[]				<u> </u>	

### ULTIMATE STRENGTH OF STEEL STRUTS.

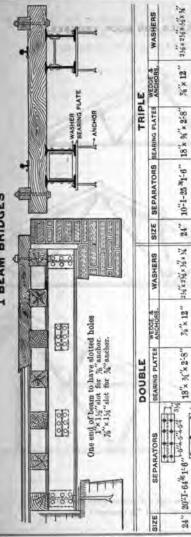
For different proportions of length in feet — 1, To least radius of gyration in inches — r. Ultimate strength in lbs. per square inch — Column — 50000 Column — 50000 Col

Column = 50000 Column = 50000 Column = 50000 Sq. Bearing 1 +  $\frac{(121)^2}{500007^2}$  Pin & S. Bear. 1 +  $\frac{(121)^2}{240007^2}$  Pin Bear. 1 +  $\frac{(121)^2}{180002^2}$ 

To obtain safe resistance. { For quiescent loads, as in buildings, divide by 4. For moving loads, as in bridges, divide by 5.

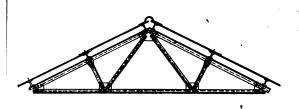
1	Ultimat per	e Strengt square in	h in lhs. ich.	1		e Strengtl square in	
r	Square.	Pin and Square.	Pin.	r	Square.	Pin and Square.	Pin.
3.0	48262	47437	46637	12.0	31725	96695	23237
3.2	48037	47100	46212	12.2	31337	26412	22825
3.4	47787	46750	45762	12.4	30962	26012	22425
3.6	47587	46387	45800	12.6	30587	25612	22025
3.8	47275	46012	44825	12.8	30212	25225	21637
4.0	46987	45625	44325	13.0	20837	24925	21250
4.2	46700	45212	43812	13.2	29462	24450	20887
4.4	46400	44800	43300	13.5	28925	23887	20850
4.6	46087	44375	42762	13.8	28375	23337	19812
4.8	45775	43925	42212		29025		10.45
5.0	45450	43475	41662	14.0	28025 27687	22975 22625	19475
5.2	45112	43025	41112	14.2 14.5	27087 27175	22020	19137 18650
5.4	44775	42562	40550	14.8	26650	21612	18162
5.6	44425	42087	39975	14.0			
5.8	44075	41600	39400	15.0	26312	21275	17962
6.0	43312	41112	38825	15.2	25987	20950	17550
6.2	43337	40625	38237	15.5	25362	20487	17112
6.4	42962	40137	37662	15.8	25025	20012	16687
6.6	42575	39637	37087	16.0	24700	19712	16400
6.8	42187	89137	36500	16.2	24387	19425	16137
7.0	41800	38637	35925	16.5	23937	18987	15737
7.2	41412	38137	35837	16.8	28487	18562	15350
7.4	41012	37637	34775				
7.6	40612	37137	34200	17.0	23187	18287	15100
7.8	40212	36687	33637	17.2	22900	18012	14850
8.0	39812	36125	38075	17.5	22475	17625	14487
8.2	39400	35625	32512	17.8	22050	17237	14150
8.4	38967	35125	31962	18.0	21775	16987	13925
8.6	38587	84625	34412	18.2	21500	16737	13700
8.8	38175	34137	30875	18.5	21100	16375	13375
9.0	37762	33650	30337	18.8	20712	16025	13062
9.2	37350	33162	29812	19.0	20462	15807	12862
9.4	36937	32675	29287	19.0	20402	15787 15582	12862
9.6	36537	32200	28785	19.5	19837	15237	12362
9.8	36125	81712	28275	19.8	19462	14912	12087
10.0	35712	31250	27775.				
10.2	35312	30787	27287	20.0	19225	14700	11900
10.4	34900	30325	26800	20.2	19000	14500	11725
10.6	34500	29862	26325	20.5	18650	14200	11462
10.8	34087	29412	25862	20.8	18312	13900	11212
11.0	33687	28962	25412	21.0	18140	13710	1104Ò
11.2	33300	28525	24950	21.2	17870	13520	10880
11.4	32900	28087	24512	21.5	17550	13250	10640
11.6	32500	27662	24087	21.8	17240	12980	10410
11.8	32112	27250	23662	1			
	·	·	·	<u> </u>	<u> </u>	<u>'</u>	

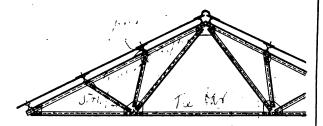


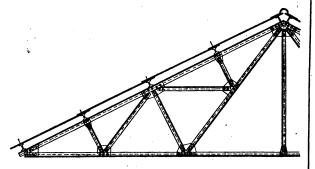


		DOUBLE					TRIPLE	E	Ø,
SIZ	SIZE SEPARATORS BEARING PLATES AMPLIAGE WASHERS SIZE SEPARATORS BEARING PLATES AMPLIAGE, WASHERS	BEARING PLATES	WEDGE &	WASHERS	SIZE	SEPARATORS	BEARING PLATES	WEDGE &	WASHERS
		100	11.0	as the art . To M	.,,	"o's as With	10,0 1,0 1,00	1,017,74	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
Ti.	20-1-91-1-9	18 × ½ × 2-8	% × 12	R K SR X SR T W SR T	12	0-1-62-1-01	10 x % x 2-0	3 × 16	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
20	20"1-6421-3"	12 × ¼ × 2-6"	%'x 12"	XxKxXxxXx	20.	10"1-25 *1'-3"	12'x %'x 2'8"	%"× 12"	2%x2%x3%x3
15	" 15"I-42" 0°11"   14   17   17   17   17   17   17   17	12'× %'× 2-0"	36"× 12"	31 × 51 × 51 × 51 × 51 × 51 × 51 × 51 ×	15"	10"1-25 *0-11"	12 × 34 × 2-6"	34 × 12 "	23/x 23/4 5/x 3
1	12" 12"1-31% 0:9" 12" 3" 3" 12" 3" 3" 12" 3" 3" 10" 2" 3" 3" 3" 3" 3" 3" 3" 3" 3" 3" 3" 3" 3"	12'× ¾'× 1-9"	3/× 10 "	%6×,8×% *,5					ikje
90	" 10"I-25"0-7"	12'× 4'× 1-6"	3,×10,	2"x 3"x N'x 25"					

STANDARD DETAILS FOR ROOF TRUSSES,







Notes; Distance from center to center of purlins should not exceed 6'0"

Roof covering generally used #20 Corrugated Steel.

Proper distance in feet, center to center of Beams.

in feet upports.		24 Inch Bran, Standard									
Distance in feet	100	95	90	85	80						
between supports.	lbs.	lbs.	1bs.	1bs.	lbs.						
10	120.8	116.8	118.2	109.6	106.0						
11	99.5	96.5	98.5	90.6	87.6						
12	88.6	81.1	78.6	76.1	78.6						
13	71.2	69.1	67.0	64.9	62.7						
14	61.4	59.6	57.8	55.9	54.2						
15	53.5	51.9	50.3	48.7	47.1						
16	46.9	45.6	44.2	42.8	41.4						
17	41.7	40.4	39.1	37.9	36.7						
18	37.1	36.0	34.9	33.8	32.8						
19	33.3	32.3	31.3	30.3	29.4						
20	30.1	29.2	28.3	27.4	26.5						
21	27.3	26.5	25.7	24.9	24.1						
22	24.8	24.1	28.4	22.6	21.9						
23	22.7	22.1	21.4	20.7	20.0						
24	20.9	20.3	19.7	19.0	18.4						
25	19.3	18.7	18.1	17.5	17.0						
26	17.8	17.2	16.7	16.2	15.7						
27	16.5	16.0	15.5	15.0	14.6						
28	15.4	14.9	14.5	14.0	13.5						
29	14.3	13.9	13.4	13.0	12.6						
30	18.4	18.0	12.6	12.2	11.8						

Proper distance in feet, center to center of Beams.

upports.		20 Inch Bi	SAM, HEAVY	SECTION.	
between supports.	100 lbs.	95 lbs.	90 lbs.	85 lbs.	80 lbs.
0	101.8	98.3	95.4	92.8	89.4
1	83.4	81.0	78.6	76.3	73.9
2	70 3	68.3	66.2	64.1	62.1
3	59.9	58.2	56.4	54.6	52.8
4	51.7	50.2	48.6	47.1	45.6
5	45.0	43.7	42.4	41.0	39.7
в	39.6	38.4	37.3	36.1	84.9
7	35.1	34.0	32.9	31.9	<b>3</b> 0.9
8	31.2	30.3	29.4	28.5	27.€
9	28.1	27.3	26.4	25.6	24.7
0	25.3	24.6	28.8	23.1	22.3
1	23.0	22.3	21.7	21.0	20.2
2	20.9	20.3	19.7	19.1	18.5
3 4	19.1	18.6	18.0	17.5	16.9
1	17.6	17.1	16.6	16.0	15.5
5	16.2	15.7	15.8	14.8	14.8
6	15.0	14.5	14.1	13.7	13.2
7	13.9	18.5	13.1	12.7	12.8
8	12.9	12.5	12.2	11.8	11.4
8 9	12.1	11.7	11.3	11.0	10.6
Ŏ	11.3	10.9	10.6	10.2	9.1

For load of 350 lbs. per square foot, divide the spacing given by 2. Maximum fiber strain, 16,000 lbs. per square inch.

Proper distance in feet, center to center of Beams.

un leet	_	20 Inch	BRAM, STA	NDARD.	
between supports.	80 lbs.	75 lbs.	70 lbs.	65 lbs.	64 lbs.
)	80.9	77.9	74.9	71.9	71.2
! }	66.8	64.4	61.9	59.4	58.9
	56.2	54.1	52.1	49.9	49.5
3	47.8	46.1	44.3	42.5	42.2
Į.	41.3	89.7	38.2	86.7	36.8
<b>i</b>	35.9	84.6	83.8	31.9	81.7
	81.6	30.4	29.3	28.1	27.8
'	27.9	26.9	25.9	24.9	24.7
3	25.0	24.1	23.1	22.2	22.0
	22.4	21.5	20.7	19.9	19.8
	20.2	19.5	18.7	17.9	17.8
	18.8	17.7	17.0	16.3	16.2
	16.7	16.1	15.5	14.9	14.7
	15.3	14.7	14.2	18.6	18.5
	14.1	13.5	13.0	12.5	12.8
i	12.9	12.5	12.0	11.5	11.4
	11.9	11.5	11.1	10.6	10.5
	11.1	10.7	10.8	9.9	9.8
	10.8	9.9	9.6	9.2	9.1
	9.6	9.3	8.9	8.6	8.5
- 1	9.0	8.6	8.3	8.0	7.9

Proper distance in feet, center to center of Beams.

in ieet upports.		15 Inch Bi	SAM, HRAVY	SECTION.	
Distance in rect	100	95	90	85	80
between supports.	lbs.	lbs.	lbs.	1bs.	1bs.
10	78.1	70.8	68.6	66.4	64.0
11	60.4	58.6	54.7	54.9	53.0
12	50.7	49.2	47.7	46.1	44.5
13	43.2	41.9	40.6	39.2	37.9
14	37.4	36.2	35.0	33.9	32.7
15	32.5	31.5	30.5	29.5	28.5
16	28.6	27.7	26.8	25.9	25.0
17	25.3	24.5	23.8	23.0	22.2
18	22.6	21.9	21.2	20.5	19.8
19	20.2	19.6	19.0	18.4	17.8
20	18.3	17.7	17.1	16.6	16.0
21	16.6	16.0	15.5	15.0	14.5
22	15.1	14.6	14.2	18.7	18.2
23	13.8	13.4	12.9	12.5	12.1
24	12.7	12.8	11.9	11.5	11.1
25	11.7	11.3	11.0	10.6	10.8
26	10.8	10.5	10.1	9.8	9.5
27	10.0	9.7	9.4	9.1	8.8
28	9 3		8.7	8.5	8.2
29	8.7	8.4	8.2	7.9	$7.6 \\ 7.1$
30	8.1	7.9	7.6	7.4	

Proper distance in feet, center to center of Beams.

e in feet supports.	15 INCH BRAM, LIGHT SECTION.									
Distance in feet	80	75	70	65	60					
between supports	1bs.	1bs.	1bs.	1bs.	1bs.					
10	58.5	56.2	54.0	51.7	49.5					
11	48.3	46.5	44.6	42.7	40.9					
12	40.6	39.0	87.5	35.9	34.3					
18	84.5	88.2	81.9	30.6	29.8					
14	29.8	28.7	27.5	26.4	25.8					
15	26.0	25.0	24.0	28.0	22.0					
16	22.8	21.9	21.1	20.2	19.8					
17	20.2	19.4	18.7	17.9	17.1					
18	18.1	17.4	16.7	15.9	15.2					
19	16.2	15.6	15.0	14.3	13.7					
20	14.6	14.1	18.5	12.9	12.8					
21	13.2	12.7	12.2	11.7	11.2					
22	12.1	11.6	11.1	10.7	10.2					
23	11.0	10.6	10.2	9.8	9.4					
24	10.2	9.8	9.4	9.0	8.6					
25	9.4	9.0	8.6	8.3	7.9					
26	8.6	8.3	8.0	7.7	7.8					
27	8.0	7.7	7.4	7.1	6.8					
28	7.4	7.1	6.9	6.6	6.3					
29	7.0	6.7	6.5	6.2	5.9					
30	6.5	6.2	6.0	5.8	5.5					

Proper distance in feet, center to center of Beams.

Distance in feet between supports.	60 1bs.	55 lbs.	50 1bs.	45	42
10		1		lbs.	lbs.
	43.9	41.7	39.5	37.3	35.9
11	36.3	34.5	32.6	30.8	29.7
12	80.5	29.0	27.4	25.9	24.9
18	26.0	24.7	23.4	22.1	21.8
14	22.5	21.3	20.2	19.0	18.8
15	19.5	18.5	17.5	16.6	15.9
16	17.1	16.3	15.4	. 14.6	14.0
17	15.2	14.5	18.7	12.9	12,4
18	18.5	12.9	12.2	11.5	11.1
19	12.2	11.5	10.9	10.8	9,9
20	11.0	10.5	9.9	9.8	9.0
21	10.0	9.5	9.0	8.5	8.1
22	9.1	8.6	8.2	7.7	7.4
23	8.8	7.9	7.5	7.0	6.8
24	7.7	7.3	6.9	6.5	6.2
25.	7.1	6.7	6.8	5.9	5.7
26	6.5	6.2	5.8	5.5	5.8
27	6.0	5.7	5.4 5.0	5.1 4.7	4.9
28	5.6	5.8	5.0	4.7	4.6
29 80	5.2 4.9	5.0 4.6	4.7	4.4	4.8 4.0

Proper distance in feet, center to center of Beams.

in feet supports.			BEAM, SECTION			Inch Bea Tandabd.	
Distance in feet	55	50	45	40	40	35	31.5
between supports.	1bs.	lbs.	lbs.	lbs.	lbs. :	lbs.	lbs.
10	82.7	80.9	29.1	27.8	24.9	28.2	21.9
11	27.0	25.5	24.1	22.6	20.6	19.1	18.1
12	22.7	21.5	20.2	19.0	17.8	16.1	15.2
18	19.4	18.3	17.2	16.2	14.8	18.7	13.0
14	16.7	15.8	14.9	13.9	12.8	11.8	11.2
15	14.5	13.7	12.9	12.1	11.1	10.8	9.8
16	12.7	12.1	11.4	10.7	9.8	9.0	8.6
17	11.3	10.7	10.1	9.4	8.6	8.0	7.6
18	10.1	9.5	9.0	8.4	7.7	7.1	6.7
19	9.1	8.6	8.1	7.5	6.9	6.4	6.1
20	8.2	7.7	7.3	6.8	6.2	5.8	5.5
21	7.4	7.0	6.6	6.2	5.7	5.3	5.0
22	6.7	6.4	6.0	5.7	5.1	4.8	4.5
28	6.2	5.8	5.5	5.1	4.7	4.4	4.2
24	5.7	5.4	5.0	4.7	4.8	4.0	8.8
25	5.3	5.0	4.7	4.8	4.0	8.7	8.5
26	4.9	4.6	4.3	4.1	8.7	3.4	8.8
27	4.5	4.2	4.0	3.8	8.4	3.2	8.0
28	4.2	3.9	3.7	3.5	8.2	3.0	2.8
29	8.9	3.7	3.5	8.3	8.0	2.7	2.6
30	8.6	8.4	8.2	<b>8.</b> 0	2.7	2.6	2.5

Proper distance in feet, center to center of Beams.

in feet			BRAM, DARD.		9 Inch Bran, Standard.					
Distance in feet	40	35	30	25	85	30	25	21		
between supports.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.		
10	19.4	17.9	16.4	14.9	15.8	13.9	12.6	11.5		
11	16.0	14.8	13.5	12.8	12.6	11.5	10.4	9.5		
12	13.4	12.4	11.4	10.8	10.6	9.7	8.7	8.0		
18	11.4	10.6	9.7	8.8	9.0	8.2	7.4	6.8		
14	9.9	9.1	8.3	7.6	7.8	7.1	6.4	5.9		
15	8.6	7.9	7.3	6.6	6.8	6.2	5.6	5.1		
16	7.5	7.0	6.4	5.7	5.9	5.4	4.9	4.5		
17	6.7	6.2	5.7	5.1	5.8	4.8	4.8	4.0		
18	6.0	5.5	5.0	4.6	4.7	4.3	8.9	8.5		
19	5.4	5.0	4.5	4.1	4.2	8.8	8.5	8.2		
20	4.9	4.5	4.1	8.7	3.8	8.5	3.1	2.9		
21	4.4	4.1	8.7	8.4	8.5	8.1	2.8	2.6		
22	4.0	8.7	8.4	3.1	3.1	2.9	2.6	2.4		
23	8.7	8.4	8.1	2.8	2.8	2.6	2.4	2.2		
24	8.4	8.1	2.9	2.6	2.6	2.4	2.2	2.0		
25	8.1	2.9	2.6	2.4	2.4	2.2	2.0	1.8		
26 27 28 29 80	2.9 2.6 2.5 2.3 2.2	2.6 2.4 2.3 2.1 2.0	2.4 2.2 2.1 1.9 1.8	2.2 2.1 1.9 1.8 1.7	2.3 2.1 1.9 1.8 1.7	2.1 1.9 1.8 1.7 1.5	1.9 1.7 1.6 1.5	1.7 1.6 1.5 1.4 1.8		

Proper distance in feet, center to center of Beams.

in feet upports.	8 Inch Bram, Standard.				7 Ince Beam, Standard.		
Distance in feet between supports.	25¼ lbs.	22% lbs.	2014 lbs.	17% lbs.	20 lbs.	171/2 lbs.	15 lbs.
5 6 7 8	41.8	39.4	87.0	34.7	29.4	27.8	25.3
6	29.1	27.4	25.7	24.1	20.5	19.0	17.5
7	21.4	20.1	18.9	17.7	15.0	13.9	12.9
8	16.3	15.4	14.5	18.5	11.5	10.7	9.8
9	12.9	12.2	11.4	10.7	9.1	8.5	7.8
10	10.5	9.9	9.8	8.7	7.4	6.9	6.3
11	8.6	8.2	7.7	7.1	6.1	5.7	5.2
12	7.8	6.9	6.5	6.0	5.1	4.7	4.4
18	6.2	5.8	5.5	5.1	4.3	4.1	8.7
14	5.8	5.0	4.7	4.4	3.8	8.5	8.2
15	4.6.	4.4	4,1	8.8	8.8	8.0	2.8
16	4.1	8.8	8.6	8.4	2.9	2.7	2.5
17	8.6	8.4	3.2	3.0	2.6	2.4	2.2
18	8.2	8.0	2.9	2.7	2.3	2.1	1.9
19	3.9	2.7	2.6	2.4	2.0	1.9	1.8
20	2.6	2.5	2.3	2.2	1.8	1.7	1.6
21	2.4	2.2	2.1	1.9	1.7	1.5	1.4
22	2.2	2.1	1.9	1.8	1.5	1.4	1.8

Proper distance in feet, center to center of Beams.

in feet supports.		Inch Brai Standard.	<b>r</b> ,	5 Inch Bram, Standard.			
Distance in feet	1714	14%	121 <u>4</u>	14%	12½	9%	
between supports.	lbs.	lbs.	lbs.	lbs.	1bs.	1bs.	
5	21.3	19.5	17.7	14.8	18.8	11.8	
6	14.8	13.5	12.8	10.8	9.2	8.2	
7	10.9	9.9	9.0	7.5	6.8	6.0	
8	8.3	7.6	6.9	5.8	5.2	4.6	
9 0 1 2	6.6	6.0	5.4	4.6	4.1	3.7	
	5.3	4.9	4.4	8.7	8.8	3.0	
	4.4	4.1	3.7	8.0	2.7	2.5	
	3.7	8.4	8.1	2.6	2.8	2.1	
3	3.1	2.9	2.6	2.2	1.9	1.7	
4	2.7	2.5	2.3	1.9	1.7	1.5	
5	2.4	2.2	1.9	1.7	1.5	1.8	
6	2.1	1.9	1.7	1.4	1.8	1.1	
7 18 19 20	1.8 1.7 1.5 1.3	1.7 1.5 1.4 1.2	1.5 1.4 1.2 1.1	1.8 1.1 1.0	1.1 1.0	1.0 0.9	
31 32	1.2 1.1	1.1 1.0	1.0 0.9				

Proper distance in feet, center to center of Beams.

Distance in feet	4 Inch Bram,				3 Inch Beam,		
etween supports.	Standard.				Standard.		
Distance	101/4	9½	8½	7½	71/3	61/ <u>6</u>	5½
between	1bs.	lbs.	lbs.	lbs.	1bs.	lbs.	lbs.
5	8.7	8.2	7.8	7.5	4.7	4.4	4.0
6	6.1	5.7	5.4	5.0	8.8	8.0	2.8
7	4.4	4.2	8.9	3.7	2.4	2.8	2.1
8	8.4	3.2	8.0	2.9	1.8	1.7	1.5
9 10 11 12	2.7 2.2 1.8 1.5	2.5 2.1 1.7 1.4	2.4 1.9 1.6 1.8	2.2 1.8 1.5 1.2	1.5 1.2 1.0	1.4 1.1	1.8
18 14 15	1.4 1.1 1.0	1.8 1.0	1.1 1.0	1.1 0.9			

Proper distance in feet, center to center of Beams.

e in feet supports.		94 Inch Beam, Standard.									
Distance in feet	100	95	90	85	80						
between supports.	lbs.	1bs.	lbs.	lbs.	lbs.						
10	140.4	186.3	132.1	127.9	123.7						
11	116.1	112.6	109.1	105.7	102.2						
12	97.5	94.6	91.7	88.8	85.9						
13	83.1	80.6	78.1	75.7	73.2						
14	71.6	69.5	67.4	65.3	63.1						
15	62.4	60.5	58.7	56.8	55.0						
16	54.7	53.2	51.6	49.9	48.3						
17	48.6	47.1	45.7	44.3	42.8						
18	43.3	42.0	40.7	39.5	38.3						
19	38.9	87.7	86.6	85.4	34.3						
20	85.1	84.1	83.0	82.0	30.9						
21	81.8	80.9	29.9	29.0	28.1						
22	29.0	28.1	27.3	26.4	25.5						
23	26.5	25.7	24.9	24.2	23.4						
24	24.4	23.7	22.9	22.2	21.5						
25	22.5	21.8	21.1	20.5	19.8						
26	20.7	20.1	19.5	18.9	18.8						
27	19.3	18.7	18.1	17.5	17.0						
28	17.9	17.4	16.9	16.8	15.8						
29	16.7	16.2	15.7	15.2	14.7						
30	15.6	15.1	14.7	14.2	18.7						

Proper distance in feet, center to center of Beams.

in feet supports.	20 Inch Bram, Heavy Section.								
Distance in feet between supports.	100 lbs.	95 lbs.	90 lbs.	85 lbs.	80 1bs.				
10	118.2	114.7	111.3	107.7	104.9				
11	97.3	94.5	91.8	88.9	86.2				
12	82.1	79.7	77.8	74.8	72.4				
13	69.9	67.9	65.8	63.7	61.7				
14	60.3	58.5	56.7	55.0	58.2				
15	52.5	51.0	49.5	47.9	46.8				
16	46.2	44.8	43.5	42.1	40.7				
17	40.9	89.7	38.5	37.3	36.1				
18	86.5	35.4	34.3	83.3	32,2				
19	32.7	81.8	<b>30</b> .8	29.9	28.9				
20	29.5	28.7	27.8	26.9	26.1				
21	26.8	26.0	25.2	24.4	23.6				
22	24.4	23.7	23.0	22.3	21.6				
23	22.3	21.7	21.0	20.4	19.7				
24	20.5	19.9	19.3	18.7	18.1				
25	18.9	18.3	17.8	17.3	16.7				
26	17.5	16.9	16.4	15.9	15.4				
27	16.2	15.7	15.8	14.8	14.8				
28	15.1	14.6	14.2	13.7	13.3				
29	14.1	18.6	13.2	12.8	12.4				
80	13.1	12.7	12.3	11.9	11.0				

Proper distance in feet, center to center of Beams.

in feet upports.	20 Inch Bran, Standard.								
Distance in feet between supports.	80 1bs.	75 lbs.	70 lbs.	65 lbs.	64 lbs.				
10	94.8	90.9	87.8	83.9	83.1				
11 12	77.9 65.5	75.1 63.1	72.2 60.7	69.3 58.2	68.7 57.7				
10	55.8	63.1 53.7	51.7	49.6	49.2				
10	55.0	33.1	***	20.0	20.20				
14	48.1	46.3	44.5	42.8	42.4				
15	41.9	40.4	38.8	37.3	36.9				
16	36.9	35.5	84.1	32.7	32.5				
17	82.6	31.4	30.3	29.0	28.8				
18	29.1.	28.1	26.9	25.9	25.7				
19	26.1	25.1	24.2	28.2	23.1				
20	23.6	22.7	21.8	20.9	20.8				
21	21.4	20.6	19.8	19.0	18.9				
22	19.5	18.7	18.1	17.3	17.2				
23	17.8	17.2	16.5	15.9	15.7				
24	16.4	15.8	15.2	14.5	14.4				
25	15.1	14.5	14.0	13.4	13.8				
26	13.9	13.4	12.9	12.4	12.8				
27	12.9	12.5	12.0	11.5	11.4				
28	12.0	11.6	11.2	10.7	10.6				
29	11.2	10.8	10.4	10.0	9.9				
30	10.5	10.1	9.7	9.8	9,2				

# JONES & LAUGHLINS, LIM

#### SPACING OF JONES & LAUGHLWE, LIMPES STEEL BEAMS, FOR UNIFORM LOAD OF 150 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.

s in feet supports.	15 Inch Bram, Heavy Section.								
Distance in feet between support	100 lbs.	95 1bs.	90 1bs.	85 1bs.	80 lbs.				
10	85.8	82.7	80.1	77.5	74.8				
11	70.5	68.8	66.1	64.0	61.8				
12	59.2	57.4	55.6	58.8	51.9				
18	50.5	48.9	47.8	45.7	44.2				
14	43.5	42.2	40.9	89.5	88.2				
15	87.9	36.7	85.6	34.4	33.3				
16	33.3	82.2	31.2	30.2	29.2				
17	29.5	28.6	27.7	26.8	25.9				
18	26.8	25.5	24.7	23.9	28.1				
19	23.6	22.9	22.2	21.5	20.7				
20	21.8	20.7	20.0	19.8	18.7				
21	19.8	18.7	18.1	17.5	16.9				
22	17.6	17.1	16.5	16.0	15.5				
23	16.1	15.6	15.1	14.6	14.1				
24	14.8	14.8	18.9	18.5	18.0				
25	18.6	13.2	12.8	12.4	12.0				
26	12.6	12.2	11.8	11.4	11.1				
27	11.7	11.8	11.0	10.6	10.8				
28	10.9	10.5	10.2	9.9	9.5				
<b>29</b>	10.1	9.8	9.5	9.2	8.9				
80	9.5	9.2	8.9	8.6	8.8				

For load of 300 lbs. per square foot, divide the spacing given by 2. Maximum fiber strain, 16,000 lbs. per square inch.

Proper distance in feet, center to center of Beams.

in feet supports.	15 Inch Bran, Light Section.								
Distance in feet between supports.	80 lbs.	75 lbs.	70 lbs.	65 lbs.	60 lbs.				
10	68.2	65.6	68.0	60.8	57.7				
11	56.3	54.2	52.1	49.9	47.7				
12	47.8	45.5	43.7	41.9	40.1				
18	40.8	38.8	87.8	85.7	84.1				
14	84.8	88.5	82.1	30.8	29.5				
15	30.3	29.1	28.0	26.9	25.7				
16	26.6	25.6	24.6	28.6	22.5				
17	28.5	22.7	21.8	20.9	20.0				
18	21.1	20.8	19.4	18.6	17.8				
19	18.9	18.2	17.5	16.7	16.0				
20	17.1	16.4	15.7	15.1	14.4				
21	15.5	14.9	14.8	18.7	18.1				
22	14.1	18.5	18.0	12.5	11.9				
28	12.9	12.4	11.9	11.4	10.9				
24	11.9	11.4	10.9	10.5	10.0				
25	10.9	10.5	10.1	9.7	9.8				
26	10.1	9.7	9.8	8.9	8.5				
27	9.8	9.0	8.6	8.8	7.9				
27 28 29	8.7	8.8	8.0	7.7	7.8				
29	8.1	7.8	7.5	7.2	6.9				
80	7.6	7.3	7.0	6.7	6.4				

Proper distance in feet, center to center of Beams.

in feet upports.	15 Inch Bram, Standard.								
Distance in feet	60	55	50	45	42				
between supports.	lbs.	1bs.	1bs.	lbs.	lbs.				
10	51.8	48.7	46.1	48.6	41.9				
11	42.4	40.2	38.1	85.9	34.6				
12	85.6	83.8	32.0	80.2	29.1				
18	30.3	28.8	27.3	25.7	24.7				
14	26.2	24.9	23.5	22.2	21.4				
15	22.8	21.6	20.5	19.8	18.6				
16	20.0	19.0	18.0	17.0	16.8				
17	17.7	16.8	15.9	15.0	14.5				
18	15.8	15.0	14.2	18.4	12.9				
19	14.2	13.5	12.7	12.1	11.6				
20	12.9	12.2	11.5	9.9	10.5				
21	11.7	11.1	10.5		9.5				
22	10.6	10.1	9.5	9.0	8.7				
28	9.7	9.2	8.7	8.2	7.9				
24	8.9	8.5	8.0	7.5	7.8				
25 26	8.3 7.6	7.8	7.4 6.8	6.9	6.7				
27	7.0	6.7	6.8	5.9	5.7				
28	6.5	6.2	5.9	5.5	5.8				
29	6.1	5.8	5.5	5.1	5.0				
80	5.7	5.4	5.1	4.8	4.6				

Proper distance in feet, center to center of Beams.

etween supports.			BEAM, SECTION	г.	12 Inch Bran, Standard.		
TOO M SON	55 lbs.	50 1bs.	45 lbs.	40 lbs.	40 lbs.	85 lbs.	311/2 lbs.
	38.1	36.1	34.0	81.9	29.1	27.1	25.0
L	31.5	29.8	28.1	26.8	24.1	22.3	21.1
}	26.5	25.1	23.6	22.1	20.2	18.8	17.
	22.6	21.3	20.1	18.9	17.8	16.0	15.
	19.5	18.4	17.8	16.8	14.9	13.8	18.
	16.9	16.0	15.1	14.1	12.9	12.0	11.4
	14.9	14.1	18.8	12.5	11.4	10.5	10.
	13.2	12.5	11.7	11.0	10.1	9.8	8.9
	11.8	11.1	10.5	9.8	9.0	8.3	7.9
	10.6	10.0	9.4	8.8	8.1	7.5	7.3
	9.5	9.0	8.5	7.9	7.8	6.7	6.4
	8.7	8.2	7.7	7.2	6.6	6.1	5.
	7.9	7.5	7.0	6.6	6.0	5.6	5.8
	7.2	6.8	64	6.0	5.5	5.1	4.9
	6.6	6.3	5.9	5.5	5.1	4.7	4.4
	6.1	5.8	5.5	5.1	4.7	4.8	4.
	5.7	5.3	5.0	4.7	4.8	4.0	8.8
	5.8	4.9	4.7	4.4	4.0	8.7	8.
	4.9	4.6	4.8	4.1	8.7	8.5	3.8
	4.5	4.8	4.1	8.8	3.5	3.2	8.
	4.2	4.0	8.7	8.5	8.2	3.0	2.9

Proper distance in feet, center to center of Beams.

in feet supports.			e Bean, dard.		9 Inch Beam, Standard.				
Distance in feet between supports.	40	35	30	25	35	30	25	21	
	1bs.	lbs.	1bs.	lbs.	lbs.	1bs.	lbs.	1bs.	
10	22.6	20.9	19.1	17.8	17.8	16.3	14.7	13.4	
11	18.7	17.8	15.8	14.8	14.7	13.4	12.1	11.1	
12	15.7	14.5	18.8	12.1	12.3	11.3	10.2	9.8	
13	13.8	12.8	11.3	10.8	10.5	9.6	8.7	7.9	
14	11. <b>5</b>	10.6	9.7	8.9	9.1	8.8	7.5	6.9	
15	10.1	9.8	8.5	7.7	7.9	7.2	6.5	5.9	
16	8.8	8.1	7.5	6.8	6.9	6.3	5.7	5.8	
17	7.8	7.2	6.6	6.0	6.1	5.6	5.1	4.7	
18	7.0	6.5	5.9	5.3	5.5	5.0	4.5	4.1	
19	6.3	5.8	5.3	4.8	4.9	4.5	4.1	3.7	
20	5.7	5.2	4.8	4.8	4.5	4.1	3.7	3.8	
21	5.1	4.7	4.3	8.9	4.1	3.7	3.8	3.1	
22	4.7	4.8	3.9	3.6	3.7	3.8	3.0	2.8	
23	4.3	8.9	3.6	3.3	3.3	3.1	2.8	2.5	
24	8.9	8.6	3.3	3.0	3.1	2.8	2.5	2.3	
25	8.6	8.8	3.1	2.8	2.9	2.6	2.3	2.1	
26	8.8	3.1	2.8	2.5	2.7	2.4	2.2	2.0	
27	3.1	2.9	2.6	2.4	2.5	2.2	2.0	1.9	
28	2.9	2.7	2.4	2.2	2.3	2.1	1.9	1.7	
29	2.7	2.5	2.3	2.1	2.1	1.9	1.7	1.6	
80	2.5	2.3	2.1	1.9	2.0	1.8	1.6	1.5	

Proper distance in feet, center to center of Beams.

e in feet supports.	,		BEAM,	7 Inch Beam, Standard.			
Distance in feet between supports.	25¼ lbs.	22% lbs.	20¼ lbs.	17% lbs.	20 lbs.	171/2 lbs.	15 lbs.
5 6 7 8	48.8	46.0	43.2	40.5	34.3	81.9	29.5
6	33.9	31.9	30.0	28.1	23.8	22.1	20.5
7	24.9	28.5	22.1	20.6	17.5	16.3	15.0
8	19.1	18.0	16.9	15.8	13.4	12.5	11.0
9	15.1	14.2	13.3	12.5	10.6	9.9	9.1
10	12.2	11.5	10.8	10.1	8.6	8.0	7.8
11	10.1	9.5	8.9	8.3	7.1	6.6	6.1
12	8.5	8.0	7.5	7.0	5.9	5.5	5.1
13	7.2	6.8	6.4	6.0	5.1	4.7	4.8
14	6.2	5.9	5.5	5.1	4.4	4.1	8.7
15	5.4	5.1	4.8	4.5	8.8	8.5	8.8
16	4.7	4.5	4.2	8.9	8.8	8.1	2.9
17	4.2	4.0	3.7	3.5	8.0	2.7	2.5
18	3.7	8.5	3.3	3.1	2.7	2.5	2.8
19	3.4	3.2	3.0	2.8	2.8	2.2	2.1
20	3.1	2.9	2.7	2.5	2.1	2.0	1.9
21	2.8	2.6	2.5	2.8	1.9	1.8	1.7
22	2.5	2.4	2.2	2.1	1.8	1.7	1.5

Proper distance in feet, center to center of Beams.

supports.		Inch Beat	,	5 Inch Beam, Standard.		
Distance in feet	17¼	14%	12¼	14%	12¼	9%
between supports	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
5	24.8	22.7	20.7	17.8	15.5	18.7
6	17.8	15.8	14.8	12.0	10.7	9.8
7	12.7	11.6	10.5	8.8	7.9	7.0
8	9.7	8.9	8.1	6.7	6.1	5.4
9	7.7	7.0	6.8	5.8	4.8	4.8
10	6.2	5.7	5.1	4.8	3.9	8.5
11	5.1	4.7	4.8	8.5	3.2	2.9
12	4.8	8.9	8.6	8.0	2.7	2.4
18	3.6	3.3	8.1	2.5	2.3	2.0
14	3.2	2.9	2.7	2.2	2.0	1.7
15	2.7	2.5	2.8	1.9	1.7	1.8
16	2.4	2.2	2.0	1.7	1.5	1.8
17 18 19 20	2.1 1.9 1.7 1.5	1.9 1.7 1.6 1.4	1.8 1.6 1.4 1.3	1.5 1.8 1.2 1.1	1.3 1.2 1.1 1.0	1.2 1.1 0.9
21 22	1.4 1.3	1.3 1.2	1.2 1.1	1.0	. <b></b>	

Proper distance in feet, center to center of Beams.

e in feet supports.		4 Inch Stani			3 Inch Beam, Standard.		
Distance in feet between supports.	10½ 1bs.	91 <u>4</u> 1bs.	81/4 1bs.	71/4 lbs.	7½ lbs.	61/4 1bs.	5½ lbs.
5	10.1	9.6	9.1	8.5	5.5	5.1	4.7
6 7 8	7.1	6.7	6.8	5.9	8.9	8.5	3.2
7	5.2	4.9	4.6	4.8	2.8	2.6	2.4
8	8.9	3.7	8.5	3.3	2.1	2.0	1.8
9	8.1	2.9	2.8	2.6	1.7	1.6	1.5
10	2.5	2.4	2.3	2.1	1.4 1.1	1.3	1.2
11	2.1	2.0	1.9	1.7	1.1	1.1	1.0
12	1.7	1.7	1.6	1.5	0.9	0.9	• • • • •
18	1.5	1.4	1.8	1.2	ll		
14	1.8	1.2	1.1	1.1	l		
15	1.1	1.1	1.0	0.9			
16	1.0	l					

Proper distance in feet, center to center of Beams.

in feet supports.	24 Inch Bram, Standard.								
Distance in feet between supports.	100 lbs.	95 1bs.	90 1bs.	85 lbs.	80 lbs.				
10	168.5	168.5	158.5	158.5	148.4				
11	139.3	135.1	181.0	126.8	122.6				
12	117.0	113.5	110.0	106.5 90.8	103.0 87.8				
13	99.7	96.7	93.7	80.0	67.8				
14	86.0	83.4	80.9	78.3	75.9				
15	74.9	72.6	70.4	68.2	66.0				
16	65.7	63.8	61.9	59.9	51.7				
17	58.8	56.6	54.8	53.1	51.3				
18	52.0	50.5	48.9	47.4	45.9				
19	46.6	45.8	48.9	42.5	41.1				
20	42.2	40.9	39.6	38.4	37.1				
21	88.2	87.1	85.9	34.8	88.7				
22	34.8	88.8	32.7	81.7	30.6				
28	31.8	80.9	29.9	29.0	28.1				
24	29.3	28.4	27.5	26.6	25.7				
25	27.0	26.2	25.4	24.6	23.8				
26	24.9	24.2	28.4	22.7	21.9				
27	28.1	22.4	21.7	21.0	20.4				
28	21.5	20.9	20.2	19.6	19.0				
29	20.0	19.4	18.8	18.2	17.7				
80	18.7	18.2	17.6	17.0	16.5				

Proper distance in feet, center to center of Beams.

Distance in feet between supports.		15 INCH BRAM, HEAVY SECTION.							
Distance between	100 lbs.	95 1bs.	90 1bs.	85 1bs.	80 lbs.				
10	102.3	99.2	96.1	98.0	89.7				
11	84.6	82.0	79.4	76.8	74.2				
12	71.0	68.9	66.7	64.5	62.8				
13	60.6	58.7	56.8	54.9	53.1				
14	52.2	50.6	49.0	47.4	45.8				
15	45.5	44.1	42.7	41.8	39.9				
16	40.0	38.7	37.5	36.3	35.0				
17	35.4	34.3	33.3	32.2	31.1				
18	31.6	30.6	29.7	28.6	27.7				
19	28.3	27.4	26.6	25.8	24.8				
20	25.6	24.8	24.0	28.2	22.4				
21	23.2	22.5	21.7	21.0	20.8				
22	21.1	20.5	19.8	19.2	18.6				
23	19.8	10.7	18.1	17.5	17.0				
24	17.7	17.2	16.6	16.1	15.6				
25	16.4	15.9	15.4	14.9	14.4				
26	15.1	14.6	14.2	18.7	18.8				
27	14.0	13.6	13.2	12.7	12.8				
28	13.0	12.6	12.2	11.8	11.4				
29	12.2	11.8	11.4	11.0	10.6				
80	11.4	11.0	10.7	10.3	10.0				

Proper distance in feet, center to center of Beams.

in feet apports.	20 Inch Bean, Standard.							
Distance in feet between supports.	80 lbs.	75 lbs.	70 lbs.	65 lbs.	64 lbs.			
10	113.2	109.0	104.8	100.6	99.8			
11	93.5	90.1	86.6	83.2	82.			
12	78.6	75.8	72.9	69.8	69.8			
18	67.0	64.5	62.0	59.5	59.6			
14	57.7	55.6	58.5	51.4	50.9			
15	50.3	48.5	46.6	44.7	44.8			
16	44.2	42.6	41.0	39.8	38.8			
17	39.1	37.7	36.2	84.8	34.			
18	85.0	38.7	32.3	31.0	30.8			
19	31.4	30.2	29.0	27.8	27.1			
20	28.3	27.3	26.2	25.1	25.0			
21	25.7	24.7	28.8	22.8	22.0			
22	23.4	22.5	21.7	20.8	20.0			
23	21.4	20.6	19.8	19.0	18.9			
24	19.7	19.0	18.2	17.4	17.3			
25	18.1	17.4	16.8	16.1	. 16.0			
26	16.7	16.1	15.5	14.9	14.			
27	15.5	15.0	14.4	13.8	13.7			
28	14.4	13.9	13.4	12.9	12.7			
29	13.4	13.0	12.5	12.0	11.8			
30	12.6	12.1	11.6	11.2	11.0			

Proper distance in feet, center to center of Beams.

Distance in feet between supports.	20 Inch Bran, Hravy Section.								
	100 1bs.	<b>95</b> lbs.	90 lbs.	85 lbs.	80 1bs.				
10	141.8	137.7	133.5	129.3	125.1				
11	117.2	113.8	110.8	106.9	103.4				
12	98.5	95.6	92.7	89.8	86.9				
13	83.9	81.4	79.0	76 5	74.0				
14	72.4	70.2	68.1	66.0	63.8				
15	68.0	61.2	59.8	57.4	55.6				
16	55.4	53.8	52.2	50.5	48.9				
17	49.1	47.6	46.2	44.7	43.3				
18	43.8	42.5	41.2	39.9	38.6				
19	39.3	38.2	37.0	35.8	34.6				
20	35.4	34.4	33.4	82.8	31. <b>8</b>				
21	32.2	81.2	30.2	29.3	28.3				
22	29.8	28.4	27.6	26.7	25.9				
23	26.8	26.0	25.2	24.5	23.7				
24	24.6	23.9	23.2	22.4	21.7				
25	22.7	22.0	21.4	20.7	20.0				
26	20.9	20.8	19.7	19.1	18.5				
27	19.4	18.9	18.3	17.8	17.2				
28	18.1	17.5	17.0	16.5	15.9				
29	16.9	16.3	15.8	15.4	14.9				
80	15.8	15.3	14.8	14.8	13.9				

Proper distance in feet, center to center of Beams.

Distance in feet between supports.	15 Inch Bram, Light Section.							
	80 1bs.	75 lbs.	70 lbs.	66 lbs.	60 lbs.			
10	81.8	78.7	75.6	72.4	69.8			
11	67.6	65.0	62.5	69.9	57.8			
12	56.8	54.6	52.5	50.3	48.1			
18	48.4	46.5	44.7	42.9	41.0			
14	41.8	40.2	88.6	37.0	85.4			
15	36.4	34.9	83.6	82.2	30.8			
16	82.0	80.7	29.5	28.3	27.0			
17	28.2	27.2	26.1	25.0	24.0			
18	25.8	24.3	23.3	22.3	21.8			
19	22.6	21.8	21.0	20.1	19.2			
20	20.5	19.7	18.9	18.1	17.8			
21	18.6	17.8	17.1	16.4	15.7			
22	16.9	16.2	15.6	15.0	14.8			
. <b>23</b>	15.4	14.9	14.3	18.7	18.1			
24	14.2	13.7	13.1	12.6	12.0			
25	18.1	12.6	12.1	11.6	11.1			
26	12.1	11.6	11.2	10.7	10.2			
27	11.2	10.8	10.8	9.9	9.5			
28	10.4	10.0	9.6	9.2	8.8			
29	9.8	9.4	9.0	8.6	8.2			
30	9.1	8.7	8.4	8.1	7.7			

Proper distance in feet, center to center of Beams.

Distance in feet between supports.	15 INCH BEAM, STANDARD								
	60 lbs.	55 1bs.	50 lbs.	45 lbs.	42 lbs.				
10	61.5	58.4	55.8	52.2	50.2				
11	50.9	48.2	45.7	43.1	41.5				
12	42.7	40.6	38.4	36.2	84.9				
13	86.4	84.6	32.7	30.9	29.8				
14	81.4	29.8	28.2	26.6	25.7				
15	27.4	25.9	24.6	23.2	22.8				
16	24.0	22.8	21.6	20.4	19.6				
17	21.8	20.2	19.1	18.0	17.4				
18	19.0	18.0	17.0	16.1	15.5				
19	17.0	16.2	15.8	14.5	13.9				
20	15.4	14.6	13.8	18.0	12.6				
21	14.0	13.8	12.6	11.8	11.4				
22 23 24 25	12.7 11.7 10.7 9.9	12.1 11.1 10.2 9.4	11.4 10.5 9.6 8.9	9.8 9.0 8.8	10.4 9.5 8.7 8.0				
26	9.1	8.6	8.2	7.7	7.4				
27	8.4	8.0	7.6	7.1	6.9				
28	7.8	7.4	7.0	6.6	6.4				
29	7.8	7.0	6.6	6.2	6.0				
30	6.8	6.5	6.1	5.8	5.6				

Proper distance in feet, center to center of Beams.

e in feet supports.		12 Ince Special	BEAM, SECTION	12 Inch Beam, Standard.			
Distance in feet between supports	55 lbs.	50 lbs.	45 lbs.	40 lbs.	40 1bs.	85 1bs.	31½ lbs.
10	45.8	43.3	40.8	38.2	35.0	32.5	30.7
11	87.8	85.8	33.7	81.6	28.9	26.8	25.4
12	81.8	30.1	28.3	26.6	24.2	22.6	21.8
18	27.1	25.6	24.2	22.6	20.7	19.2	18.2
14	23.4	22.1	20.8	19.5	17.8	16.6	15.7
15	20.8	19.2	18.1	17.0	15.5	14.4	13.7
16	17.8	16.9	15.9	15.0	13.7	12.6	12.0
17	15.8	15.0	14.1	13.2	12.1	11.2	10.6
18	14.2	13.4	12.6	11.8	10.8	10.0	9.4
19	12.7	12.0	11.3	10.6	9.7	9.0	8.5
20	11.4	10.8	10.2	9.5	8.7	8.1	7.7
21	10.4	9.8	9.2	8.6	7.9	7.4	7.0
22	9.4	8.9	8.4	7.9	7.2	6.7	6.3
28	8.6	8.2	7.7	7.2	6.6	6.2	5.8
24	7.9	7.5	7.0	6.6	6.1	5.6	5.3
25	7.4	7.0	6.6	6.1	5.6	5.2	4.9
26	6.8	6.4	6.0	5.7	5.2	4.8	4.6
27	6.2	5.9	5.6	5.8	4.8	4.5	4.2
28	5.8	5.5	5.2	4.9	4.5	4.2	3.9
29	5.4	5.2	4.9	4.6	4.1	3.8	3.7
30	5.0	4.8	4.5	4.2	3.8	3.6	3.4

Proper distance in feet, center to center of Beams.

in feet supports			BEAM.		9 Inch Bram, Standard.				
Distance in feet between supports.	40 1bs.	35 lbs.	30 lbs.	25 1bs.	35 lbs.	30 1bs.	25 lbs.	21 lbs.	
10 11	27.1 22.4	25.0 20.7	22.9 18.9	20.8 17.2	21.4 17.7	19.5 16.1	17.6 14.6	16.1 13.8	
12	18.8	17.3	15.9	14.5	14.8	13.5	12.2	11.2	
13	16.0	14.8	18.6	12.8	12.6	11.5	10.4	9.5	
14	13.6	12.8	11.7	10.6	10.9	9.9	9.0	8.2	
15	12.1	11.1	10.2	9.3	9.5	8.6	7.8	7.1	
16	10.6	9.8	9.0	8.2	8.8	7.6	6.9	6.8	
17	9.3	8.6	7.9	7.2	7.4	6.7	6.1	5.6	
18	8.4	7.7	7.0	6.4	6.6	6.0	5.4	5.0	
19	7.5	6.9	6.8	5.7	5.9	5.4	4.9	4.5	
20	6.8	6.2	5.7	5.2	5.4	4.9	4.4	4.0	
21	6.2	5.7	5.2	4.7	4.9	4.4	4.0	8.7	
22	5.6	5.2	4.7	4.8	4.4	4.0	8.6	8.8	
28	5.1	4.7	4.8	3.9	4.0	3.7	3.4	8.0	
24	4.7	4.8	4.0	8.6	3.7	3.4	8.0	2.8	
25	4.8	4.0	3.7	3.4	3.4	8.1	2.8	2.6	
26	4.0	3.7	8.4	3.0	8.2	2.9	2.6	2.4	
27	3.7	3.4	8.1	2.9	2.9	2.6	2.4	2.2	
28	3.4	3.2	2.9	2.6	2.7	2.5	2.2	2.1	
29 30	3.2 3.0	2.9	2.7 2.6	2.5 2.3	2.6 2.4	2.8 2.2	2.1 1.9	1.5	

Proper distance in feet, center to center of Beams.

in feet upports.			BEAN, DARD.	7 Inch Beam, Standard.			
Distance in feet between supports.	25½ · lbs.	22¾ lbs.	201⁄4 lbs.	17% lbs.	20 lbs.	17% lbs.	15 lbs.
5	58.6	55.2	51.8	48.5	41.2	88.8	85.4
5 6 7 8	40.7	88.8	36.0	83.7	28.6	26.6	24.6
7	29.9	28.2	26.5	24.7	21.0	19.5	18.0
8	22.9	21.6	20.8	19.0	16.1	15.0	13.8
9	18.1	17.0	16.0	14.9	12.7	11.8	10.9
10	14.6	18.8	18.0	12.2	10.3	9.6	8.8
11	12.1	11.4	10.7	10.0	8.5	7.9	7.8
12	10.2	9.6	9.0	8.4	7.1	6.6	6.2
13	8.6	8.2	7.7	7.2	6.1	5.7	5.2
14	7.4	7.0	6.6	6.2	5.3	4.9	4.5
15	6.5	6.2	5.8	5.4	4.6	4.2	3.9
16	5.7	5.4	5.0	4.7	4.0	8.7	8.4
17	5.0	4.8	4.5	4.2	3.6	8.8	3.0
18	4.5	4.2	4.0	3.8	3.2	8.0	2.7
19	4.1	3.8	8.6	3.4	2.8	2.6	2.5
20	3.7	3.4	8.2	8.0	2.6	2.4	2.2
21	3.4	3.1	2.9	2.7	2.8	2.2	2.0
22	8.0	2.8	2.6	2.5	2.2	2.0	1.8

Proper distance in feet, center to center of Beams.

in feet apports.		Inch Beat		5 Inch Beam, Standard.		
Distance in feet	171/	14%	12¼	14%	12¼	9%
between supports.	lbs.	lbs.	lbs.	lbs.	1bs.	1bs.
5	29.8	27.8	24.8	20.7	18.6	16.5
6	20.7	19.0	17.2	14.4	12.9	11.4
7	15.2	13.9	12.6	10.5	9.5	8.4
8	11.6	10.6	9.7	8.1	7.3	6.5
9	9.2	8.4	7.6	6.4	5.8	5.1
10	7.4	6.8	6.2	5.2	4.6	4.1
11	6.2	5.7	5.1	4.2	3.8	3.4
12	5.2	4.7	4.3	8.6	3.2	2.9
13	4.3	4.0	8.7	8.0	2.7	2.4
14	3.8	8.5	8.2	2.6	2.4	2.1
15	3.3	8.0	2.7	2.3	2.1	1.8
16	2.9	2.6	2.4	2.0	1.8	1.6
17	2.6	2.3	2.2	1.8	1.6	1.4
18	2.3	2.1	1.9	1.6	1.4	1.8
19	2.1	1.9	1.7	1.4	1.8	1.1
20	1.8	1.7	1.5	1.3	1.1	1.0
21	1.7	1.5	1.4	1.2	1.1	1. <b>0</b>
22	1.5	1.4	1.3	1.0		0. <b>9</b>

Proper distance in feet, center to center of Beams.

Distance in feet etween supports.			BEAM,	8 Inch Bran, Standard.			
Distance	10½	9½	81/4	71/4	71/4	6½	51/2
between	lbs.	lbs.	lbs.	1bs.	lbs.	lbs.	1bs.
5	12.2	11.5	10.9	10.2	6.6	6.1	5.6
6	8.5	8.0	7.5	7.0	4.6	4.2	8.6
7	6.2	5.8	5.5	5.2	3.4	8.2	2.9
8	4.7	4.5	4.2	4.0	2.6	8.4	2.2
9	3.7	3.5	8.8	8.1	2.1	1.9	1.8
10	3.0	2.9	2.7	2.6	1.7	1.5	1.4
11	2.5	2.4	2.2	2.1	1.4	1.8	1.2
12	2.1	2.0	1.8	1.7	1.1	1.0	0.9
18 14 15 16	1.8 1.5 1.4 1.2	1.7 1.4 1.8 1.1	1.6 1.4 1.3 1.0	1.5 1.3 1.1 0.9	1.0	0.9	0.8

Proper distance in feet, center to center of Beams.

Distance in feet between supports.	24 Inch Bran, Standard.								
	100 lbs.	95 lbs.	90 lbs.	85 lbs.	80 1bs.				
10 11	210.6 174.1	204.4 168.9	198.1 163.7	191.8 158.5	185.5 153.8				
12	146.8	141.9	187.5	133.2	128.8				
13	124.6	120.9	117.2	118.5	109.8				
14	107.5	104.8	101.1	97.9	94.7				
15	98.6	90.8	88.0	85.2	82.5				
16	82.8	79.8	77.4	74.9	72.5				
17	72.9	70.7	68.5	66.4	64.2				
18	65.0	63.1	61.1	59.2	57.4				
19	58.3	56.6	54.9	53.1	51.4				
20	52.7	51.1	49.5	48.0	46.4				
21	47.8	46.3	44.9	43.5	42.1				
22	43.5	42.2	40.9	89.6	88.8				
23	39.8	88.6	87.4	86.8	85.1				
24 .	86.6	85.5	84.4	83.8	82.2				
25	83.7	82.7	81.7	80.7	29.7				
26	81.1	80.2	29.3	28.4	27.4				
27	28.9	28.0	27.2	26.8	25.5				
28	26.9	26.1	25.8	24.5	28.7				
29 30	25.0 23.4	$24.3 \\ 22.7$	23.6 22.0	$\frac{22.8}{21.8}$	22.1 20.6				

Proper distance in feet, center to center of Beams.

in feet supports.		20 Inch Beam, Heavy Section.								
Distance in feet	100	95	90	85	80-					
between supports.	lbs.	1ъв,	lbs.	1bs.	1bs.					
10	177.3	172.1	166.9	161.6	156.4					
11	146.5	142.2	137.9	133.6	129.8					
12	123.1	119.5	115.9	112.2	108.6					
18	104.9	101.8	98.8	95.7	92.6					
14	90.5	87.8	85.1	82.5	79.8					
15	78.8	76.5	74.2	71.8	69.5					
16	69.3	67.2	65.2	63.1	61.1					
17	61.4	59.6	57.8	55.9	54.1					
18	54.7	53.1	51.5	49.9	48.3					
19	49.1	47.7	46.2	44.8	43.3					
20	44.8	43.0	41.7	40.4	39.1					
21	40.2	89.0	37.8	36.7	35.5					
22	36.6	35.5	34.5	33.4	32.3					
23	33.5	32.5	81.5	30.6	29.6					
24	30.8	29.9	29.0	28.0	27.1					
25	28.4	27.5	26.7	25.9	25.0					
26	26.2	25.4	24.7	23.9	28.1					
27	24.3	23.6	22.9	22.2	21.5					
28	22.6	21.9	21.3	20.6	19.9					
29	21.1	20.5	19.8	19.2	18.6					
30	19.7	19.1	18.5	18.0	17.4					

Proper distance in feet, center to center of Beams.

in feet supports.	20 Inch Bram, Standard.								
Distance in feet	80	75	70	65	64				
between supports.	1bs.	lbs.	1bs.	1bs.	lbs.				
10	141.5	136.8	131.0	125.8	124.7				
11	116.9	112.6	108.3	104.0	103.1				
12	98.3	94.6	91.0	87.3	86.6				
18	83.7	80.6	77.5	74.4	78.8				
14	72.2	69.5	66.9	64.2	63.6				
15	62.9	60.6	58.2	55.9	55.4				
16	55.3	53.2	51.2	49.1	48.7				
17	48.9	47.1	45.3	43.5	48.2				
18	43.7	42.1	40.4	88.8	88.5				
19	89.2	87.7	36.3	84.8	84.6				
20	35.4	34.1	32.7	81.4	31.2				
21	32.1	30.9	29.7	28.5	28.8				
22	29.2	28.1	27.1	26.0	25.8				
	26.7	25.7	24.8	23.8	23.6				
23 24 25	24.6 22.6	23.7 21.8	22.8 20.9	21.8 20.1	21.7 20.0				
26	20.9	20.1	19.4	18.6	18.4				
27	19.4	18.7	18.0	17.8	17.1				
28	18.0	17.3	16.7	• 16.0	15.9				
29	16.8	16.2	15.6	15.0	14.8				
30	15.7	15.1	14.6	14.0	18.9				

Proper distance in feet, center to center of Beams.

in feet apports.	15 Inch Bram, Heavy Section.								
Distance in feet	100	95	90	85	80				
between supports.	lbs.	lbs.	lbs.	lbs.	lbs.				
10	127.9	124.0	120.1	116.2	112.2				
11	105.7	102.5	99.2	96.0	92.7				
12	88.8	86.1	83.4	80.7	77.9				
18	75.7	78.4	71.0	68.6	66.4				
14	65.3	68.8	61.8	59.3	57.8				
15	56.9	55.1	53.4	51.6	49.9				
16	50.0	48.4	46.9	45.4	43.8				
17	44.3	42.9	41.6	40.2	38.8				
18	39.5	38.3	37.1	35.8	84.7				
19	35.4	34.3	33.3	32.2	81.1				
20	82.0	31.0	30.0	29.0	28.0				
21	29.0	28.1	27.2	26.3	25.4				
22	26.4	25.6	24.8	24.0	23.2				
23	24.2	28.4	22.7	21.9	21.2				
24	22.2	21.5	20.8	20.2	19.5				
25	20.5	19.8	19.2	18.6	18.0				
26	18.9	18.8	17.7	17.1	16.6				
27	17.5	17.0	16.5	15.9	15.4				
28	16.3	15.8	15.8	14.8	14.3				
29	15.2	14.7	14.8	13.8	13.3				
80	14.2	18.8	18.8	12.9	12.5				

Proper distance in feet, center to center of Beams.

in feet upports.		15 Inch Bran, Light Section.									
Distance in feet between supports	80 1bs.	75 lbs.	70 lbs.	65 1bs.	60 lbs.						
10	102.8	98.4	94.5	90.5	86.6						
11	84.5	81.8	78.1	74.8	71.6						
12 13	71.0 60.3	68.8 58.2	65.6 55.9	62.9 53.6	60.1 51.2						
19	00.5	96.2	99.8	55.6	01.7						
14	52.2	50.2	48.2	46.2	44.2						
15	45.5	43.7	42.0	40.8	38.5						
16	40.0	38.4	86.9	85.4	33.8						
17	85.8	34.0	39.7	81.8	80.0						
18	31.6	80.4	29.2	27.9	26.7						
19	28.3	27.3	26.2	25.1	24.0						
20	25.6	24.6	23.6	22.6	21.6						
21	23.2	22.3	21.4	20.5	19.6						
22	21.1	20.3	19.5	18.7	17.9						
23	19.3	18.6	17.8	17.1	16.4						
24	17.8	17.1	16.4	15.7	15.0						
25	16.4	15.7	15.1	14.5	18.9						
26	15.1	14.5	14.0	13.4	12.8						
87	14.0	18.5	12.9	12.4	11.9						
28	13.0	12.5	12.0	11.5	11.0						
59	12.2	11.7	11.8	10.8	10.8						
30	11.4	10.9	10.5	10.1	9.6						

Proper distance in feet, center to center of Beams.

Distance in feet between supports.	15 Inch Beam, Standard.								
Distanc between	60 lbs.	55 lbs.	50 lbs.	45 1bs.	42 ibs.				
10	76.9	78.0	69.1	65.2	62.8				
11	68.6	60.8	57.1	58.9	51.9				
12	58.4	50.7	48.0	45.8	43.6				
18	45.5	43.2	40.9	88.6	87.2				
14	89.8	87.3	85.8	83.8	<b>3</b> 2.1				
15	84.2	82.4	30.7	29.0	27.8				
16	80.0	28.5	27.0	25.5	24.				
17	26.6	25.8	28.9	22.5	21.7				
18	23.7	22.5	21.8	20.1	19.4				
19	21.8	20.2	19.1	18.1	17.4				
20	19.3	18.3	17.8	16.8	15.7				
21	17.5	16.6	15.7	14.8	14.2				
28	15.9	15.1	14.8	18.5	13.0				
28	14.6	13.8	18.1	12.8	11.8				
24	13.4	12.7	12.0	11.8	10.9				
25	12.4	11.7	11.1	10.4	10.0				
26	11.4	10.8	10.2	9.7	9.8				
27	10.5	10.0	9.5	8.9	8.6				
28	9.8	9.3	8.8	`8.8	8.0				
29	9.1	8.7	8.2	7.7	7.8				
80	8.5	8.1	7.7	7.2	7.0				

Proper distance in feet, center to center of Beams.

Distance in feet between supports.		15 Inch Bram, Light Section.									
	80 lbs.	75 lbs.	70 lbs.	65 1bs.	60 lbs.						
10	102.3	98.4	94.5	90.5	86.6						
11	84.5	81.8	78.1	74.8	71.6						
12	71.0	68.3	65.6	62.9	60.1						
13	60.3	58.2	55.9	53.6	51.2						
14	52.2	50.2	48.2	46.2	44.2						
15	45.5	43.7	42.0	40.3	38.5						
16	40.0	38.4	86.9	85.4	33.8						
17	35.8	34.0	39.7	81.8	80.0						
18	31.6	80.4	29.2	27.9	26.7						
19	28.3	27.3	26.2	25.1	24.0						
20	25.6	24.6	23.6	22.6	21.6						
21	23.2	22.3	21.4	20.5	19.6						
22	21.1	20.3	19.5	18.7	17.9						
23	19.3	18.6	17.8	17.1	16.4						
23 24	17.8	17.1	16.4	15.7	15.0						
25	16.4	15.7	15.1	14.5	18.9						
26	15.1	14.5	14.0	18.4	12.8						
27	14.0	18.5	12.9	12.4	11.9						
28	13.0	12.5	12.0	11.5	11.0						
29	12.2	11.7	11.8	10.8	10.8						
30	11.4	10.9	10.5	10.1	9.6						

Proper distance in feet, center to center of Beams.

in feet upports.	15 INCH BEAM, STANDARD.								
Distance in feet	60	55	50	45	42				
between supports.	lbs.	lbs.	lbs,	lbs.	ibs.				
10	76.9	78.0	69.1	65.2	62.8				
11	68.6	60.3	57.1	58.9	51.9				
12	58.4	50.7	48.0	45.8	43.6				
18	45.5	43.2	40.9	88.6	87.2				
14	89.3	87.3	85.8	88.8	32.1				
15	84.2	82.4	80.7	29.0	27.9				
16	80.0	28.5	27.0	25.5	24.5				
17	26.6	25.8	28.9	22.5	21.7				
18	28.7	22.5	21.8	20.1	19.4				
19	21.3	20.2	19.1	18.1	17.4				
20	19.8	18.3	17.8	16.8	15.7				
21	17.5	16.6	15.7	14.8	14.2				
29	15.9	15.1	14.8	18.5	18.0				
28	14.6	13.8	18.1	12.8	11.9				
24	13.4	12.7	12.0	11.8	10.9				
25	12.4	11.7	11.1	10.4	10.0				
26 27 28 29	11.4 10.5 9.8 9.1 8.5	10.8 10.0 9.3 8.7 8.1	10.9 9.5 8.8 8.2 7.7	9.7 8.9 8.8 7.7 7.2	9.8 8.6 8.0 7.5 7.0				

Proper distance in feet, center to center of Beams.

s in feet supports.			BRAM,	7 Inch Bran, Standard.			
Distance in feet between supports	25¼ lbs.	22% lbs.	2014 lbs.	17% 1bs.	20 lbs.	1714 1bs.	15 lbs.
5	78.2	69.0	64.8	60.7	51.5	47.8	44.8
6 7	50.9	47.9	45.0	42.1	35.8	88.2	80.7
7	87.4	85.2	83.1	80.9	26.3	24.4	22.5
8	28.6	27.0	25.3	23.7	20.1	18.7	17.2
9	22.6	21.3	20.0	18.7	15.9	14.8	18.6
10	18.3	17.8	16.2	15.2	12.9	12.0	11.0
11	15.1	14.8	18.4	12.5	10.6	9.9	9.1
12	12.7	12.0	11.8	10.5	8.9	8.8	7.7
18	10.8	10.2	9.6	9.0	7.6	7.1	6.5
14	9.8	8.8	8.3	7.7	6.6	6.1	5.6
15	8.1	7.7	7.2	6.7	5.7	5.8	4.9
16	7.1	6.7	6.3	5.9	5.0	4.7	4.8
17	6.8	6.0	5.6	5.2	4.5	4.1	8.8
18	5.6	5.8	5.0	4.7	4.0	8.7	8.4
19	5.1	4.8	4.5	4.2	8.5	8.8	8.1
20	4.6	4.8	4.0	8.8	8.2	8.0	2.8
21	4.2	8.9	8.7	8.4	2.9	2.7	2.5
22	8.8	8.6	8.8	8.1	2.7	2.5	2.8

Proper distance in feet, center to center of Beams.

in feet apports.	1	Inch Brai Standard		5 Inch Bran, Standard.			
Distance in feet	17%	14%	1214	14%	123 <u>4</u>	9%	
between supports.	lbs.	lbs.	lbs.	lbs.	1ba.	lbs.	
5	87.2	84.1	81.0	25.9	28.2	20.6	
6	25.9	28.7	21.5	18.0	16.1	14.8	
7	19.0	17.4	15.8	18.2	11.9	10.5	
8	14.5	18.8	12.1	10.1	9.1	8.0	
9	11.5	10.5	9.5	8.0	7.2	6.4	
10	9.8	8.5	7.7	6.5	5.8	5.2	
11	7.7	7.1	6.4	5.8	4.8	4.8	
12	6.5	5.9	5.4	4.5	4.0	8.6	
18	5.4	5.0	4.6	3.8	8.4	8.0	
14	4.8	4.4	4.0	8.8	8.0	2.6	
15	4.1	8.8	8.4	2.9	2.6	2.8	
16	8.6	8.8	8.0	2.5	2.8	3.0	
17	8.2	2.9	2.7	2.2	2.0	1.8	
18	2.9	2.6	2.4	2.0	1.8	1.6	
19	2.6	2.4	2.1	1.8	1.6	1.4	
20	2.8	2.1	1.9	1.6	1.4	1.8	
21	2.1	1.9	1.8	1.5	1.8	1.2	
22	1.9	1.8	1.6	1.3	1.2	1.1	

Proper distance in feet, center to center of Beams,

in feet supports.			BEAM,	3 Inch Beam, Standard.			
Distance in feet	101/2	91/2	81/2	7½	71/4	61/4	51/4
between supports.	lbs.	lbs.	1bs.	lbs.	lbs.	1bs.	1bs.
5	15.2	14.4	13.6	12.7	8.8	7.7	7.0
6	10.6	10.0	9.4	8.8	5.8	5.8	4.9
7	7.8	7.8	6.9	6.5	4.3	4.0	8.6
8	5.9	5.6	5.8	5.0	3.2	8.0	2.7
9	4.7	4.4	4.2	3.9	2.6	2.4	2.2
10	8.8	3.6	8.4	8.2	2.1	1.9	1.8
11	8.1	8.0	2.8	2.6	1.7	1.6	1.5
12	2.6	2.5	2.3	2.2	1.4	1.8	1.2
13 14 15 16	2.2 1.9 1.7 1.5	2.1 1.8 1.6 1.4	2.0 1.7 1.5 1.8	1.9 1.6 1.4 1.2	1.2 1.1 0.9	1.1 1.0 0.9	1.0 0.9 0.8
17 18 19	1.8 1.2 1.1	1.2 1.1 1.0	1.2 1.0 0.9	1.1 1.0 0.8			

#### GIRDERS IN BUILDINGS.

In the design of a building cases may occur where a single Beam Girder will not answer. It may be found desirable to increase the lengths of the spans so as to reduce the number of supporting columns to a minimum, or, it often occurs, that heavy concentrated loads, such as vaults, brick walls, etc., will render single beam girders inadequate. Various forms of girders may be used in such cases. Where the ends of the girders rest upon the wall, bearing plates should be used to distribute the pressure over a greater surface, and thereby prevent the crushing of the material in the wall directly under the girder.

The allowed pressure per square foot for brick work should not exceed six tons, and for stone twelve to twenty tons, according to its character.

For spaning openings in brick walls, girders composed of two or more I-beams connected by bolts and separators are most commonly used.

The probable line of rupture where the bricks have been laid regularly, if the girders should fail, will be found to be inside the sides of an isosceles triangle, whose base is the span, and whose height is one third of the span. In order to be entirely on the safe side, the weight of wall between vertical lines directly over the girder for a height equal to that of the triangle is frequently adopted as the load to be carried. It should be noted, however, that for green walls, or walls having openings, this rule does not apply.

Placing the weight of brick work at 112 lbs. per cubic foot, the weights for superficial foot for different walls are as follows:

For	9"	wall		-	-	-	84	lbs.
"	13''	"	-	-	-	-	121	"
66	18"	"	-	-	-	-	168	"
"	22"	"	-	-	-	-	205	"
"	26''	6 6	_	•		-	243	"

# EXPLANATION OF TABLES. JONES & LAUGHLINS, LIMITED, SECTIONS.

These tables have been in most cases calculated for the lightest weights to which each section can be rolled. Heavier weights can be rolled in the same grooves by separating the rolls, but they are not kept in stock, and can only be obtained by special rolling.

The tables on pages 77 to 87, for Beams, give the loads which a Beam will carry safely (distributed uniformly over its length) for the distances between supports indicated. These loads include the weight of the Beam, which must be deducted in order to arrive at the net load which the Beam will carry. On pages 88 to 124 will also be found the safe loads for other sections and girders.

The values given are based on a maximum fibre strain of 16,000 lbs. per square inch for Beams and Channels, while for other shapes, 12,000 lbs. has been used.

It has been assumed in these tables that proper provision is made for preventing the compression flanges of the Beams from deflecting sideways. They should be held in position at distances not exceeding twenty times the width of the flange, otherwise the strain allowed should be reduced as per table, page 175.

In some instances deflection, rather than absolute strength, may become the governing consideration in determining the size of beam to be used. For Beams carrying plastered ceilings, for example, it has been found by practical tests that, if the deflection exceeds \$\frac{1}{26}\$ of the distance between supports, or \$\frac{1}{26}\$ of an inch per foot of the distance, there is danger of the ceiling cracking. This limit is indicated in the following tables by cross times, beyond which the Beams should not be used, if intended to carry plastered ceilings, unless the allowable loads given in the tables are reduced. There is an element of safety not taken into account in the tables, viz., the fact that the dead load of the floor is carried by the Beams before the plaster is

applied; consequently, only the deflection due to the live load is liable to cause damage to the plaster. The following method can be used to obtain the reduced loads:

Multiply the load given immediately above the cross line by the square of the corresponding span, and divide by the square of the required span; the result will be the required load. See example III on page 175.

A table of deflection of Jones & Laughlins, Limited, sections is given on page 76. It may generally be assumed, both for rolled and built Beams, that the above limit is not exceeded so long as the depth of the Beam is not less than  $\frac{1}{10}$  of the distance between supports (# inch per foot).

Inasmuch as the carrying capacity of Beams increases largely with their depth, and it is therefore economical to use the greatest depth of Beam consistent with the other conditions to which it is necessary to conform (as clear height, etc.), the above cases of extreme deflection will rarely be met with in practice.

As the deflection of Beams is not very uniform either in Iron or Steel, the question of the relative deflection of Iron and Steel Beams can be decided only from the average results of a large number of tests. Such experiments as have been made, though insufficient in number to be conclusive, indicate that a Steel Beam will deflect slightly less than an Iron Beam of the same section, under the same load, in about the inverse ratio of the moduli of elasticity for these materials as generally assumed, or say as 14 to 15.

The tables on pages 127 to 170, inclusive, for Beams, give the proper spacing, center to center of Beams, for loads varying from 100 to 175 lbs., per square foot, and for spans ranging in length from 5 to 80 feet. The spacing of Beams is inversely proportionate to the loads; therefore, for a load not given in the table, as, for instance, 200 lbs. per square foot, divide the space given for 100 lbs. per square foot by 2, etc.

# EXAMPLES OF APPLICATION OF TABLES.

I. What will be the most economical arrangement of floor Beams and Girders for carying a load of 150 lbs., including weight of floor, assuming the floor to be supported by brick arches resting between the Beams and carrying a plastered ceiling below?

ANSWER: The spacing of floor Beams for brick arches, as stated above, should not exceed 6 feet. Referring to page 145, we find the deepest Beam corresponding to this space (above horizontal cross lines) to be a 9" Beam, 21 lbs., with a length of span of 15 feet. The girders to which the floor Beams are framed should, therefore, be spaced 15 feet apart, and from the table we find that a 15" Beam, 50 lbs., 18 feet long, will answer. The relative cost must be determined by the circumstances of the case, i. e., length of columns, etc. The headroom required may render it necessary to use a double girder of shallower beams, say two 10" Beams, 25 lbs., 15 feet long.

II. What size and weight of Beam 19'6" long in clear between walls, and therefore 20 feet long between centers of supports, will be required to carry safely a uniformly distributed load of 16 tons, the weight of the Beam included?

Answer: From the table for safe loads of Beams, a 15"
Beam, 42 lbs., will carry safely, for a span of 20 feet, 15.71
tons, or .29 tons less than required in this case. Therefore,
a beam of this size and weight will be sufficient to carry the
load. Otherwise use Beam weighing 45 lbs., which will
carry 16.29 tons.

III. What load uniformly distributed, including its own weight, will a 15" Beam, weighing 50 lbs. per foot, carry for a span of 30 feet, without deflecting sufficiently to endanger a plastered ceiling?

Answer: From the table for safe loads of Beams we find, at the limit indicated for plastered ceilings, that a 15", 50 lb. Beam will carry safely a uniform load of 13.82 tons over a span of 25 feet. In order not to give rise to undue deflection, the safe load for a 30 foot span, according to the rule given on page 173, will be

$$\frac{13.82\times25^{8}}{80^{8}}$$
 = 9.60 tons.

# BEAMS WITHOUT LATERAL SUPPORT.

L	ength of	Beam.	forming a		safe load.
20 ti	imes fla	nge width	Whole	tabula	r load.
30	"	"	9/10	"	"
40	66	"	8/10	"	46 <sub>e</sub> .
50	"	"	7/10	"	"
60	66	66	6/10	• 6	. 66
70	"·	66	5/10	66	64

# GENERAL FORMULAS ON THE FLEXURE OF BEAMS OF ANY CROSS-SECTION.

Let A = area of section, in square inches.

l = length of span, in inches.

W = load, uniformly distributed, in lbs. M = bending moment, in inch-pounds.

h = height of cross-section, out to out, in inches.

n = distance of center of gravity of section, from top or from bottom, in inches.

s = strain per square inch in extreme fibers of beam, either top or bottom, in lbs., according as n relates to distance from top or from bottom of section.

D = maximum deflection, in inches.

I = moment of inertia of section, neutral axis through center of gravity.

I'= moment of inertia of section, neutral axis parallel to above, but not through center of gravity.

d = distance between these neutral axes.

R = moment of resistance.

r = radius of gyration, in inches.

E = modulus of elasticity (for wrought iron, assume 27,000,000, for steel, 29,000,000).

Then: 
$$R = \frac{I}{n}$$
  $r = \sqrt{\frac{I}{A}}$ 

$$M = \frac{sI}{n} = sR$$

$$s = \frac{Mn}{I} = \frac{M}{R}$$

$$W = \frac{8sI}{\ln} = \frac{8s}{I}$$

$$s = W\ln = WI$$

 $I' = I + Ad^2$ 

 $D = \frac{5 \text{ Wl}^3}{884 \text{ EI}} \text{ for beam supported at both ends and uni-}$ 

 $D = \frac{Pl^{\mathfrak{p}}}{48 \, EI} \quad \text{for beam supported at both ends and}$  loaded with a single load P at middle.

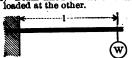
 $D = \frac{Wl^{s}}{8 EI}$  for beam fixed at one end and unsupported at the other and uniformly loaded.

 $D = \frac{Pl^{3}}{3 EI}$  for beam fixed at one end and unsupported at other, and loaded with a single load P at the latter end.

# MENDING MOMENTS AND DEFLECTIONS OF BEAMS UNDER VARIOUS SYSTEMS OF LOADING.

W=total load. l = length of beam.

(1) Beam fixed at one end and

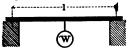


Safe load=1/4 that given in tables. Maximum bending moment at point of support = Wl.

Maximum shear at point of support = W.

Deflection =  $\frac{Wl^{\bullet}}{}$ 8 EI

(8) Beam supported at both ends, single load in the middle.

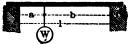


Safe load  $= \frac{1}{4}$  that given in tables. Maximum bending moment at middle of beam=

Maximum shear at points of support=1/2 W. W72

Deflection = 48 ET

Beams supported at both (5) énds, single unsymmetrical load.



Safe load=that given in tables | Safe load=that given in tables

Max. bending moment under load \_ Wab

Maximum shear: at support near  $a = \frac{Wb}{l}$ ; at other support  $= \frac{Wa}{l}$  Maximum shear between load

Maximum deflection

$$= \frac{Wab(2l-a)}{9EIl} \sqrt{\frac{1}{16}a(2l-a)}$$

I = moment of inertia. E = modulus of elasticity.

(2) Beam fixed at one end, and uniformly loaded.



Safe load=¼ that given in tables.

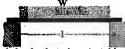
Maximum bending moment at

point of support=

Maximum shear at point of support = W.  $Wl^3$ 

Deflection =

(4) Beam supported at both ends and uniformly loaded.



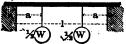
Safe load=that given in tables.

Maximum bending moment at middle of beam=

Maximum shear at points of support=1/2 W. W!

Deflection = 76.8EI

(6) Beam supported at both ends, two symmetrical loads.

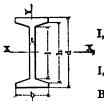


Maximum bending moment between loads=14 Wa.

and nearer support  $=\frac{1}{2}$  W.

Max. Deflect. =  $\frac{Wa}{48 E I}$  (3l<sup>2</sup>-4a<sup>2</sup>).

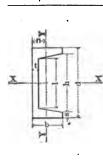
# VALUES OF MOMENTS OF INERTIA



I, axis X-X=
$$\frac{b d^8 - \frac{1}{4r}(\hbar^4 - l^4)}{12}$$

I, axis Y-Y=
$$\frac{b^{2}(d-h)+lt^{2}+\frac{r}{4}(b^{4}-t^{4})}{12}$$

Batter= $r=\frac{h-l}{h-l}$ 



I, axis X-X= 
$$\frac{b d^3 - \frac{1}{8r}(h^4 - l^4)}{12}$$

I, axis Y-Y

$$= \frac{2 s b^{3} + l t^{3} + \frac{r}{2} (b^{4} - t^{4})}{3} - An^{2}$$

$$n = [b^{3} s + \frac{h t^{2}}{2} + \frac{r}{3} (b - t)^{3} (b + 2t)] + A$$

$$n = [b^2 s + \frac{h t^2}{2} + \frac{r}{3}(b-t)^2(b+2t)] + A$$

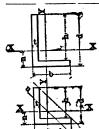
Area = 
$$A = 2bs+ht+\frac{h-l}{2}(b-t)$$

Batter = 
$$r = \frac{h-l}{2(b-t)}$$



I, axis X-X=
$$\frac{b n^{3}+t (d-n)^{3}-(b-t) (n-f)^{3}}{3}$$
  
I, axis Y-Y= $\frac{f b^{3}+(d-f) t^{3}}{12}$ 

$$n = \frac{b f^2 + t (d^2 - f^2)}{2 (h t + b f)}$$



I, axis X-X=
$$\frac{b n^{3}+t(d-n)^{3}-(b-t)(n-t)^{3}}{3}$$
, for uneven and even angles.  
I, axis Y-Y= $\frac{d n^{3}+t(b-n)^{3}-(d-t)(n-t)^{3}}{3}$ ,

for uneven angles.

I, axis U-U= $\frac{2n^4-2(n-t)^4+t[b-(2n-\frac{t}{2})]^8}{------}$ 

for even angles.  $t = \frac{t(2h+b)+h^2}{t}$ , for uneven and even a

2(h+b)even angles.

# VALUES OF MOMENTS OF INERTIA-CONTINUED.

I=Moment of Inertia.

R=Moment of Resistance.

Sections.	I	R
X X X Y	For axis X-X= $\frac{b h^s}{12}$ For axis Y-Y= $\frac{b h^s}{8}$	b h2 6
- b-1	$\frac{b\ (h^{8}-h_{1}^{8})}{12}$	$\frac{b(h^8-h_1^8)}{6\ h}$
X, X	$\frac{b  h^{s} - b_{1} h_{1}^{s}}{12}$	$\frac{bh^8-b_1h_1^8}{6h}$
X b X	For axis X-X= $\frac{b h^3}{36}$ For axis Y-Y= $\frac{b h^3}{12}$	$Min.=\frac{bh^2}{24}$
X X	$\frac{\pi d^4}{64}$	$\frac{\pi d^2}{32}$
x Oxi	$\frac{\pi (d^{4}-d_{1}^{4})}{64}$	$\frac{\pi(d^4-d_1^4)}{32\ d}$
	- π b h <sup>3</sup> 64	π b h <sup>2</sup> 32
A MARINA	$\frac{bh^{8} - (b - b_{1})h_{1}{}^{8}}{12}$	2 I
hs. h	$\frac{b  h^{s} - (b - b_{1})  h_{1}^{s} - (b_{1} - b_{2})  h_{2}^{s}}{12}$	2 I
	$\frac{\frac{b  h^{3-}(b-b_1)  h_1^{3-}(b_1-b_2)  h_2^{3-}(b_2-b_3)  h_2^{3}}{12}$	2 I

# STEEL COLUMNS IN FIRE-PROOF BUILDINGS.

The construction of steel frame fire-proof buildings, though of recent date, is becoming general in large and important cities. In the business centers of our great cities no other form can be used to advantage, and the architects who are keeping pace with improvements recognize the desirability of the improved construction. This change has been facilitated in no small degree by the great improvements made in the art of fire-proof construction, ensuring not only a higher degree of efficiency, but a considerable reduction in cost, as compared with methods formerly practiced.

The old style of solid brick or stone arch, at one time so common, has been almost wholly supplanted by the modern forms of hollow tile and terra cotta, and roofs, ceilings and partition walls are now largely constructed of these refractory materials.

The substitution of steel for iron in beams has hastened this radical improvement. Our patterns of beams and channels, having the highest efficiency, are well adapted for this purpose.

For some time past another change which has gradually taken place has been the substitution of steel for cast iron in the composition of columns, cast iron being a material so uncertain in character that its use in bridge construction has long since been abandoned. In buildings the loads are generally quiescent, and the liability of sudden shocks is more remote than in bridges; yet, on the other hand, the columns seldom receive their loads as favorably as in bridges. In many cases there exists considerable eccentricity, that is, the loads on one side of the column are heavier than on the other side, and the bending strains arising therefrom increase the strains from direct compression materially.

The following are some of the contingencies which may arise in the manufacture of castings, and which preclude anything approaching uniformity in the product:

In the case of hollow cast iron columns, while the metal is yet in a molten state, the buoyancy of the central core tends to cause it to rise, thereby reducing the thickness of the metal above and increasing the same below. When columns are of such lengths as to make it necessary to pour the metal into the moulds from both ends, it sometimes occurs that the iron becomes too much chilled on the surface to properly mix and unite, thus creating a weak seam at the very point where the greatest strength will be needed. The presence of confined air, producing "blowholes" and "honey-comb," and the collection of impurities at the bottom of the mould, may be further mentioned as frequent sources of weakness in cast iron.

The most critical condition, however, is that due to the unequal contraction of the metal during the process of cooling, thereby giving rise to initial strains, at times of sufficient force to produce rupture in the column or in its lugs on the slightest provocation. In many cases the trouble can be ascribed to faulty designing or carelessness in the execution of the work, yet even under favorable conditions it is so difficult to secure equal radiation from the moulds in all directions, that castings, entirely exempt from inherent shrinkage strains, are probably seldom produced.

As a protection against these contingencies, resort must be had either to the crude or uncertain expedient of a high safety factor, not less than 8 or 10, or a material, such as rolled steel, must be adopted, of a more uniform and reliable character than cast iron.

Steel columns fail either by deflecting bodily out of a straight line, or by buckling of the metal between rivets or other points of support. Both actions may take place at the same time, but if the latter occurs alone, it may be an indication that the rivet spacing or the thickness of the metal is insufficient.

The rule has been deducted from actual experiments upon Steel Columns, that the distance between centers of rivets should not exceed, in the line of strain, sixteen times the thickness of metal of the parts joined, and that the distance between rivets or other points of support, at right angles to the line of strain, should not exceed thirty-two times the thickness of the metal.

On page 63 are shown sections of some of the most common forms of built columns. Figures 4 and 6 are known as closed columns. As it is impracticable to repaint the inner surface of such columns, it is preferable to use them only for interior work where the changes in temperature are not considerable and the air is dry. In places exposed to the extremes of temperature and unprotected from rain, the paint on the inner surface of the column will sooner or later cease to be a protection. Corrosion will set in and, once begun, will continue as long as there is unoxidized metal left in the column. The remaining figures on this page represent columns with open sections or latticed columns, which admit of repainting and are suitable for out-of-door work.

On pages 17, 18 and 19 are shown sections of the Larimer column, which has recently been placed on the market. Its claims for superiority over any other steel or iron column are based mainly on the following qualities:

1st. Economy of and Promptness of Manufacture.

It has only one row of rivets, while two or more rows are required by other columns, and being made of beams, special shapes do not have to be rolled, as the beams can be taken from stock, saving the time necessary for rolling special sections.

2nd. High Ultimate Resistance to Compression.

Actual tests show that the resistance to compression for the Larimer column is greater than for any other of equal weight and sectional area.

3rd. Adaptability for Connections with Beams, etc.

When used in buildings for supporting floor beams, either single or double, these qualities are of the greatest importance. Connections can be readily made to the Larimer columns at any point and from any angle. For details of connections, see pages 64 and 65.

# JONES & LAUGHLINS,

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4TH. INSPECTION AND PURCHISOR HILLORE

When columns are used for out-door work of in places exposed to dampness and not covered permanently with fireproofing, this column can be more readily inspected and repainted than any other form, there being less hidden surface.

When it is desired to carry unusually heavy loads, as is frequently the case for the lower stories of very high buildings, the Larimer columns can be reinforced to the required strength, either by plates riveted to each flange, or by plates forming a box entirely covering the Larimer column. See page 119.

Cast and steel bases are shown on page 63. Complete tables giving the safe loads in tons for Larimer columnsmay be found on pages 114 to 119.

# STANDARD SPECIFICATIONS

GOVERNING THE

# PHYSICAL PROPERTIES OF STRUCTURAL AND SPECIAL OPEN-HEARTH PLATE AND RIVET STEEL

AS ADOPTED BY

# THE ASSOCIATION OF AMERICAN STEEL MANUFACTURERS.

#### STRUCTURAL STEEL.

Process of Manufacture.

- (1) Steel may be made by either the open hearth or Bessemer process.
- Test Pieces.
- (2) All tests and inspections shall be made at place of manufacture prior to shipment.
  - (3) The tensile strength, limit of elasticity and ductility shall be determined from a standard test piece cut from the finished material and planed, milled or turned parallel. The elongation shall be measured on an original length of eight inches, except when the thickness of the finished material is fa inch or less, in which case the elongation shall be measured in a length equal to sixteen times the thickness; and except in rounds of a inch or less in diameter, in which case the elongation shall be measured in a length equal to eight times the diameter of section tested. Two test pieces shall be taken from each melt or blow of finished material, one for tension and one for bending.
  - (3a) Material which is to be used without annealing or further treatment is to be tested in the condition in which it comes from the rolls. When material is to be annealed or otherwise treated before use, the specimen representing such material is to be similarly treated before testing.
  - (4) Every finished piece of steel shall be stamped with the blow or melt number, and steel for pins shall have the blow or melt number stamped on the ends. Rivet and lacing steel, and small pieces for pin plates and stiffeners, may be shipped in bundles securely wired together, with the blow or melt number on a metal tag attached.

Finish.

(5) Finished bars must be free from injurious seams, flaws or cracks, and have a workmanlike finish.

### GRADES OF STEEL.

(6) Steel shall be of three grades, Rivet. Soft and Medium.

# Rivet Steel.

(7) Ultimate strength, 48,000 to 58,000 pounds per square inch. Elastic limit, not less than one-half the ultimate strength. Elongation, 26 per cent. Bending test, 180 degrees flat on itself, without fracture on outside of bent portion.

# Soft Steel.

(8) Ultimate strength, 52,000 to 62,000 pounds per square inch. Elastic limit not less than one-half the ultimate strength. Elongation 25 per cent. Bending test, 180 degrees flat on itself, without fracture on outside of bent portion.

#### Medium Steel.

(9) Ultimate strength, 60,000 to 70,000 pounds per square inch. Elastic limit not less than one-half the ultimate strength. Elongation, 22 per cent. Bending test, 180 degrees to a diameter equal to thickness of piece tested, without fracture on outside of bent portion.

# Pin Steel.

(10) Pins made from either of the above mentioned grades of steel shall, on specimen test pieces cut at a depth of one inch from surface of finished material, fill the physical requirements of the grade of steel from which it is rolled, for ultimate strength, elastic limit, and bending, but the required elongation shall be - decreased 5 per cent.

# Eye-Bar Steel.

(11) Eye-bar material, 11/2 inches and less in thickness, made of either of the above-mentioned grades of steel. shall, on test pieces cut from finished material, fill the requirements of the grade of steel from which it is rolled. For thickness greater than 11/4 inches, there will be allowed a reduction in the percentage of elongation of one per cent. for each 1/4 of an inch increase of thickness, to a minimum of 20 per cent, for medium steel and 22 per cent. for soft steel.

# Full Size Eye-Bars.

(12) Full size test of steel eye-bars shall be required Test of Steel to show not less than 10 per cent. elongation in the body of the bar, and tensile strength not more than 5,000 pounds below the minimum tensile strength required in specimen tests of the grade of steel from which they are rolled. The bars will be required to break in the body, but should a bar break in the head, but develop 10 per cent, elongation and the ultimate strength specified, it shall not be cause for rejection, provided not more than one-third of the total number of bars tested break in the head; otherwise the entire lot will be rejected.

# Variation in Weight.

(13) The variation in cross-section or weight of more than 2½ per cent. from that specified will be sufficient cause for rejection, except in the case of sheared plates ordered to gauge, when there will be permitted an excess of weight, over that corresponding to the dimensions on the order, equal in amount to that specified in the following table:

Table of Allowances for Overweight for Rectangular Plates.

THICKNESS OF PLATE.	WIDTH OF PLATE.								
THICKNESS OF THATE.	Up to 75 in.	75 in. to 100 in.							
inch.	10 per cent.	14 per cent.							
Å "	8 "	12 "							
g "	7 "	10 "							
7 "	6 ''	8 "							
i	5 "	7 "							
16 "	41 "	64 "							
	4 "	6 "							
Over # . "	81 "	5 "							

## Specifications for Structural Cast iron.

(i) Except where chilled iron is specified, all castings shall be tough gray iron, free from injurious co d-shuts or blow-holes, true to pattern, and of a workmanlike finish. Sample pieces one inch square, cast from the same heat of metal in sand moulds, shall be capable of sustaining, on a clear span of 4 feet 8 inches, a central load of 500 pounds when tested in the rough bar.

# SPECIAL OPEN-HEARTH PLATE AND RIVET STEEL.

# Test Pieces.

- (1) All tests and inspections shall be made at place of manufacture prior to shipment.
- (2) The tensile strength, limit of elasticity and ductility, shall be determined from a standard test piece cut from the finished material and planed, milled or turned parallel. The elongation shall be measured on an original length of 8 inches, except when the thickness of the finished material is  $\frac{1}{16}$  inch or less, in which case the elongation shall be measured in a length equal to sixteen times the thickness; and except in rounds of  $\frac{1}{8}$  inch or less in diameter, in which case the elongation shall be measured in a length equal to eight times the diameter of section tested. Four test pieces shall be taken from each melt of finished material; two for tension and two for bending.

- (2a) Material which is to be used without annealing or further treatment is to be tested in the condition in which it comes from the rolls. When material is to be annealed or otherwise treated before use, the specimen representing such material is to be similarly treated before testing.
- (3) Every finished piece of steel shall be stamped with the melt number. Rivet steel may be shipped in bundles securely wired together, with the melt number on a metal tag attached.

# GRADES OF STEEL.

## Extra Soft Steel.

(4) Ultimate strength, 45,000 to 55,000 pounds per square inch. Elastic limit, not less than one-half the ultimate strength. Elongation, 28 per cent. Cold and Quench bends, 180 degrees flat on itself without fracture on outside of bent portion.

# Fire Box Steel.

(5) Ultimate strength, 52,000 to 62,000 pounds per square inch. Elastic limit, not less than one-half the ultimate strength. Elongation, 26 per cent. Cold and Quench bends, 180 degrees flat on itself, without fracture on outside of bent portion.

# Flance er

(6) Ultimate strength, 52,000 to 62,000 pounds per Boiler Steel. square inch. Elastic limit, not less than one-half the ultimate strength. Elongation, 25 per cent. Cold and Quench bends, 180 degrees flat on itself, without fracture on outside of bent portion.

### **Boiler Rivet** Steel.

(7) Steel for the boiler rivets shall be made of the extra soft quality specified in paragraph No. 4.

For all plates ordered to gauge, there will be permitted an excess of weight over that corresponding to the dimensions on the order equal in amount to that specified in the following table:

Table of	1
Allowances for Over-	
weight for Rectangular	
Plates.	

THICKNESS OF PLATE.	WIDTH OF PLATE.							
HICKNESS OF PLATE.	Upt	to 75 in.	75 in. to 100 in.					
inch.	10 p	er cent	14 per cent.					
16 "	8	**	12	44				
* "	7	**	10	**				
18 "	6	4.	8	**				
i "	5	**	7	44				
, . · ·	43	44	61	**				
	4	44	6	**				
Over & "	31	••	5	**				

5	Radius of Gyrstion, Mentral Axis as before.	<b>3</b> 4.	1.28 1.39 1.39 1.13 1.32 1.33 1.33 1.01
12	Moment of In- ertis, Neutral Axis Coinci- dent with Center Line of Web.	ľ	488 45.32 45.32 83.32 41.43 41.53 41
11	Coefficient of Strength for Fiber Strain of 12500 Lbs. per Sq. In. Used for Bridges.	C,	1,645,600 1,484,500 1,385,300 1,122,000 1,105,300 999,300 876,800 779,200 676,700 601,100
10	Coefficient of Strength for Fiber Strein of 16000 Lbs. per Sq.In. Used for Buildings.	۵	2,106,300 1,855,300 1,773,300 1,414,200 1,547,500 1,247,500 1,279,200 1,122,300 1,122,300 1,032,000 1,032,
0	Radius of Gyration, Neutral Axis as before.	ı	99 7.7.7.7.00 7.00 7.00 7.00 7.00 7.00 7
8	Section Factor, Neutral Axis as before.	R	197.5 178.9 146.6 116.8 116.95 1179.93 105.2 105
7	Moment of In- ertla, Weutral Axis perpen- dicular to Web at center.	I	2369.6 2087.3 1662.3 1466.8 1326.4 1169.4 719.3 609.0 541.0
•	Width of Flange.	Inches.	6.393 6.853 6.853 6.853 6.853 6.853 6.853 6.853
ю	Thickness of Web.	Inches.	. 746 . 894 . 735 . 735 . 738 . 983 . 983 . 769 . 769
4	Area of Section.	Sq. In.	29.2 29.2 29.6 29.6 29.4 29.4 29.4 29.4 11.0 11.0 11.0 12.4 12.4 12.4 13.4 14.0 15.4 15.4 15.4 16.4 17.4 17.4 17.4 17.4 17.4 17.4 17.4 17
8	Weight per Foot.	Lbs.	100 100 100 100 100 100 100 100 100 100
8	Рерth of Веаш.	Inches.	<b>44 88 88 5555</b>
-	Section,	No.	71 2

								_	_							_						
	13	1.04	1.08	.6	1.01	<b>.</b>	.97	₹.	œ	ထ္	<b>%</b>	.74	2.	8	22.	<b>.</b>	3	.57	20	82	53	C or C'=Ll-8 M
NTINCED	12	17.54	18.81	10.95	9.2	9.51	<b>6</b> .89	7.4	5.16	4.78	3.78	3.24	2.67	2.36	1.85	1.71	1.23	1.01	E.	19:	94.	Cor C.
BEAMS-CONTINUED.	11	447,100	373,600	341,400	289,800	264,800	203,500	208,600	157,200	143,000	118,500	100,600	86,200	72,800	60,500	50,500	40,300	29,800	24,900	16,200	13,800	M-CorC';
STEEL B	10	572,300	478,100	437,000	383,700	338,900	260,500	267,000	201,300	183,100	151,700	128,700	110,400	93,100	77,400	64,700	51,600	38,100	31,800	008'08	17.600	L-Corc';
- 1	ø	4.45	4.77	4.57	4.83	3.68	4.07	3.31	8.7	3.04	8.31	2.68	2.87	2.27	2.46	1.87	2.02	1.52	1.65	1.15	1.23	
LIMI	6	53.6	44.8	41.0	98.0	81.8	24.4	25.0	18.9	17.3	14.2	12.1	10.4	8.7	7.3	6.1	4.8	9.8	8.0	1.9	1.7	t given a
LAUGHLINS, LIMITED,	7	821.	268.95		215.81	158.85	122.1	112.68	84.92	68.64	28.99	42.23	36.23	26.2	21.79	15.15	12.09	7.14	26.92	2.93	2.48	1-span in feet C and C'-Coefficient given above
& LAU	8	5.618	5.25	5.208	٠.	5.1	4.66	4.787	4.33	4.276	4.	3.87	3.68	3.575	8.83 88.	8.294		88.8	2. 80. 80.	2.526	2.33	l-span Cand C
JONES	w			.558	33.	.75	ᇏ.	747	83	546	22	.46	33	.475	.23	35	12.	.41	.19	386	.17	
OF JC	4	16.25	11.84	11.76	8.8	11.69	7.35	10.29	6.31	7.43	5.33	5.88	4.42	5.07	3.61	4.34	2.87	3.09	2.21	2.21	1.63	nly distroct-lbs
RTIES	9	55.	9	6	31.5	9	35.	35.	я: :	25.25	17.75	8	15.	17.25	12.25	14.75	9.75	10.5	7.5	•	5.5	. unifor
PROPERTIES	2	13	13	13	12	10	9	6	6	æ	œ	<u>.</u> -	<u>}-</u>	9	9	20	20	4	4	က	က	ad in lbs
•	-	P- 5	P 5	P 6	# <del>6</del>	~ 占	P 7	8-8	B-8	B-9	B- 8	B-10	B-10	B-11	B-11	B-13	B-13	B-13	B-13	B-14	B-14	L-Safe Load in lbs. uniformly distributed. M-Moment of Forces in foot-lbs

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7	Distance of Gen- ter of Gravity from Outside from Outside	Inches.	88.5.	22	52	89. 19.	88.	L1−8 M.
5	Radius of Gyration, Meutral Axis Sefore,	<b>Դ</b>	.87 19.	5. 18:		2.6	8.8	C or C'-LI
4	Moment of In- ertia, Neutral Axis Coinci- dent with Center Line of Web.	ľ			. 2.88 .30		2.87 1.83	Corc'
=	Coefficient of Strength for Fiber Strain of 13500 Lbs. per Sq. In. Used for Bridges.	ć	482,100 847,200	273,500	193,200	130,800 87,600	100,000 67,300	CorC' M
0	Coefficient of Strength for Fiber Strain of 16000 Lbs. per Sq. In. Used for Buildings.	C	617,100 444,500	350,100 227,800	247,300 142,700	167,500	128,000 86,100	above { L-
۰	Radius of Gyration, Meutral Axis as before.	-	5.15	4.09	3.85 3.87		2.76 3.11	ts ofven
8	Section Factor, Meutral Axia as before.	æ	57.85 41.67		28.18 13.38	15.70 10.52		eet.
1	Moment of In- ertla, Neutral Axis perpen- dicular to Web at center.	I	433.88 312.56	196.93 128.11	115.90 66.88	70.65	47.99 82.30	1—Span in feet.
•	Width of	Inches.	8.831 3.4	3.418 2.94	3.188 2.6	2.814	2.628 2.26	fbuted.
ю	Thickness of Web.	Inches.					.28 28 28	mly distr
•	Area of Section.	8q. In.	16.37	11.76 6.03	10.34	æ-4		L-Safe Load in lbs., uniformly distributed.
6	Weight per Foot.	Lbs.			35. 15.	8 E		ad in lbs
N	Depth of	I.	15.55	22	22	00	<b>20 20</b>	le L
-	Section.	No.	23	င်္ဂ လူလူ	အ ပ ပ	33	, , , ,	L-Sal

					-
ò	=	Distance of Cen- ter of Gravity from Outside from Outside	Inches.	878 7878 7878 7878 788 788 788 788 788	
TINUE	5	Radius of Gyration, Neutral Axis as before.	'n	25. 25. 25. 25. 25. 25. 25. 25. 25. 25.	
CHANNELS—CONTINUED.	21	Moment of In- ertis, Meutral Axis Coinci- dent with Center Line of Web.	ľ	88. 81. 88. 88. 89. Pro	
	=	Coefficient of Strength for Fiber Strain of 12500 Lbs. per 12501 Lbs. per Sq. In. Used for Bridges.	ý	78,800 50,200 54,500 84,100 84,700 19,100 15,800 11,500 9,100	
D, STEEL	5	Coefficient of Strength for Fiber Strain of 16000 Lbs. per 5q. In. Used for Buildings.	C	100, 900 64, 300 68, 700 46, 700 81, 800 11, 800 11, 600	,
LIMITED,	۰	Radius of Gyration, Meutral Axis as before.		2.39 2.72 2.07 2.07 2.07 2.07 1.75 1.95 1.95 1.08 1.108	
1		Section Factor, Mentral Axia as before.	æ	9.46 6.03 6.03 6.54 4.33 7.23 7.23 1.39 1.09	
LAUGHLINS,	7	Moment of In- ertis, Meutral Axiw perpen- dicular to Web at center.	I	38.10 9.46 2.39 100, 21.09 6.03 2.72 64, 13.00 4.33 2.34 46, 10.48 4.19 1.75 44, 7.42 2.29 1.46 24, 8.79 1.90 1.56 2.08 1.38 1.08 1.4, 1.64 1.09 1.17 11, 11, 11, 11, 11, 11, 11, 11, 11, 1	,
ES &	•	Width of Flange.	Inches.	2.51 2.09 2.288 1.92 2.044 1.75 1.75 1.75 1.68 1.606	
F JONES	ю	Thickness of Web.	Inches.	.68 .21 .268 .284 .19 .19 .327 .386 .366 .17	
ES OF	4	Area of Section.	Sq. In.	C-6 7 19 75 5.79 .63 2.51 C-7 6 15.5 4.59 .568 2.286 C-7 6 15.5 4.59 .568 2.286 C-8 5 11.5 3.42 .484 2.044 C-8 5 10.5 1.95 .19 1.75 C-9 4 7.25 2.14 .327 1.75 C-9 4 5.25 1.55 .18 1.68 C-10 3 6. 1.78 .366 1.606 C-10 3 4. 1.19 .17 1.41 L-Safe Load in Ibs., uniformly distributed.	
PROPERTIES	6	Weight per Foot.	Lbs.	19.75 9.75 15.5 8. 11.5 6.5 7.35 7.35 6. 6. 4.	101
5	N	Дерtр об Сраппед	념	5-5-80 70 74 4 88 old	1
•	-	Section.	No.	00 00 00 00 00 00 00 00 00 00 00 00 00	

# PROPERTIES OF JONES & LAUGHLINS, LIMITED, TEES. TEES.

			•
18	Coefficient of strength for floor square inch, Neutral per square inch, Neutral Axis as before.	ď	22840 20880 18880 14580 12850 9220 7880 6810
13	Coefficient of strength for for all the period for period and the period for the	Ö	28800 24440 22440 17490 11680 11080 9570 8170
11	Redius of Gyration, Mentral Axis as before.	'n	0000 0000 58888 8855 5655
01	Moment of Resist- ance, Meutral Axis as before.	R'	1.58 1.68 1.58 1.58 1.81 0.97 0.97
0	Moment of Inertia, Ventral Axia thro' center of Gravity, co- incident with Stem.	ľ	88.88 89.88 89.89 9.61 11.44 11.44 11.44
•	Radius of Gyration, as alx A lender Merce.	H	1.54 1.38 1.38 1.21 1.22 1.04 0.101
	Section Factor, Mentral Axis as before.	R	3.35 3.05 3.76 3.19 1.93 1.93 1.03
•	Moment of Inertia, Neutral Axia thro Center of Gravity, parallel to Flange.	I	11.55 9.99 8.57 6.12 5.42 8.09 8.09
ю	Dist. of Center of Gravity from out- side of Flange.	Inches.	1.55 1.48 1.39 1.20 1.10 0.10 0.91
4	Area of Section.	Sq. Inch.	4444 88888 5841 88884
<b>6</b> 0	Weight per Foot.	Pounds.	16.00 15.50 15.00 15.00 10.00 10.40 10.40 10.80 9.80
œ	Size Flange by Stem.	Inches.	4444 4888 ×××× ×××× 4444 4888 **********************************
-	SECTION.	No.	HHHH HHHH 88.1 88.48

18	5900 8980 7780 5970	5130 4060 3480 2120	2670 2170 1700 1290	1288 258 266 266 266 266 266 266 266 266 266 26	564.88 0188
13	7070 10770 9830 7160	6150 4870 4170 2540	3200 2610 2040 1540	1530 1020 1100 1100	780 880 970 970
11	6.00 87.00 88.00 40.00	0000 84200 84200	0.48 0.48 0.58	0.0 0.38 0.33 0.33	0.28 0.27 0.22 0.21
01	0.84 0.63 0.63	0.52 0.43 0.36 0.34	0.28 0.28 0.18 0.29	0.14 0.10 0.10 0.077	0.072 0.064 0.085 0.024
6	1.47 1.08 0.93 0.93	0.78 0.54 0.45	0.32 0.25 0.18 0.37	0.12 0.092 0.076 0.058	0.045 0.034 0.017 0.018
•	0.84 1.05 1.03 0.91	0.92 0.75 0.75 0.57	0.67 0.67 0.59 0.48	0.51 0.48 0.44 0.47	0.87 0.89 0.80
7	0.88 1.35 1.17 0.89	0.77 0.61 0.52 0.33	0.40 0.33 0.25 0.19	0.19 0.13 0.14 0.11	0.097 0.073 0.047 0.084
8	1.88.89 8.89.89 8.89.89	20.1.08 0.98.04.0	0.68 0.37 0.37	0.24 0.16 0.18 0.13	0.080 0.062 0.083 0.084
10	0.75 0.98 0.89	0.87 0.79 0.74 0.54	0.68 0.67 0.56 0.44	0.51 0.50 0.46 0.47	0.42 0.40 0.33 0.30
•	8888 8888	1.98 1.58 1.59 1.59	1.38	0.88 0.69 0.77 0.56	0.57 0.45 0.86 0.26
8	9888	8.8.4. 8.8.9. 8.9.8	4.68 8.50 8.50 8.90	88.83 1.883 9.98	0.125
æ	######################################	######################################	**** **** *****	#### ×××× ####	****** *****
-	HHHH 48850	924 884 88	4410 4110 7211	EEEE	1116 118 118

# ANGLES. PROPERTIES OF JONES & LAUGHLINS, LIMITED, ANGLES.

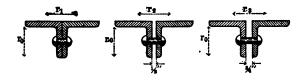
					ANGLES	ES WITH		UNEQUAL LEGS.					
-	æ	8	4	19	8	2	8	6	10	11	18	18	14
.1		.88	.100£		Perpendicular distance from centre of gravity to back of flanges.	erpendicular distances from centre of gravity to back of flanges.	Moments o	Moments of Inertia. I	Section Factor. B	Factor.	Redi	Radius officyration F	g
KOITOES	.ezi8	Тріскпе	Weight per	98 to 891A	To hack of longer flange.	To back of shorter dange.	Neutral Axis of parallel to longer flange.	Neutral Axia parallel to shorter flange.	Montral Axis perallel to longer flange.	Mentral Axis parallel to shorter flange.	Meutral Axis parallel to longer flange.	Mentral Axis of letrarq shorter flangs.	, saiber teach. Leachait sixa
No.	Inches,	Inches	Pounds.	Sq. Inch.	Inches.	Inches.	1	ľ	æ	R,	H	ľ	E
A 13	8 X:	<b>*</b> #	12.80 25.40	8.61	1.10	2.1° 2.1° 3.1°	4.90 9.14	18.47 25.95	1.60 3.15	8.8 6.88	1.14	1.90	0.92
A 13	6 X: X: 4.	********	24.00 24.00 21.00 20.00	3.42 7.08 8.23 6.17	0.79 1.08 1.17	2.04 1.53 1.67	8.34 6.15 8.09	13.86 24.69 8.14 14.35	2.23 1.57 2.86 8.86	8. 8. 8. 4. 8. 8. 8. 8. 8. 8. 8. 8.	0.98	1.98 1.59 1.59	9.000 9.88.89.89
A 14 A 15	5 × × × × × × × × × × × × × × × × × × ×	• • • • • • • • • • • • • • • • • • •	10.40 19.80 9.70 18.50		80.00 80.58 80.54	1.75 1.76 1.84	8.18 2.45 40.45 74.	7.78 13.70 7.37 18.04			0.00	1.69 1.61 1.61 1.61	9.000 85.58

14	0.74 0.73 0.67 0.65	0.00	0000 88844	0.47 9.46 0.46 0.46	0.43 0.43 0.21	0.15
18	1.25 1.15 1.35 1.16	01.19	0.98 8.88 8.88	0.97 0.97 0.97 0.91	0.79	0.32
81	1.06 0.97 0.87 0.80	0.38 0.88 0.81	0.74 0.67 0.68	0.59 0.58 0.58	0.60	0.17
11	2.78 1.48 2.66	2.1.26 2.1.09 2.08 2.08	0.75 1.46 0.56 1.08	0.51 0.84 1.00	0.29	0.088
91	1.18 2.13 0.85 1.56	0.66 1.18 0.88 1.52	0000 48.00 87.00 87.00	0.8 0.8 0.8 0.8 0.4 7	0.19	0.012
6	4.18 7.26 8.88 6.85	3.16 4.68 4.65	1.80 8.13 1.17 2.06	2.38 0.88 1.98	0.51	0.019
80	2.99 5.13 1.88 3.24	2.15 3.15 3.11	0.78 1.32 1.28 1.28	0.83 0.68 0.31 0.67	0.29 0.64 0.016	0.0028
2	1.32 1.38 1.43	2.1.2. 2.8.1. 2.8.2. 2.8.2.	1.38	11.99	0.47	0.32
•	0.96 1.09 0.78 0.92	0.68 0.83 0.98	0.61 0.86 0.75	0.46 0.57 0.47 0.58	0.51 0.63 0.22	0.13
10	2.08 2.48 69	8.3.4.8. 8.3.9. 8.9.9.	2.50 2.50 3.50	0.97 2.38 0.91 2.26	0.81 2.00 0.25	0.19
*	9.10 17.20 8.50 15.90	7.7 14.30 15.80	8.4.9.8 8.50.80 8.50.00	3.30 8.10 3.10 7.70		0.63
80	ब्यंक ब्यंत ब्यंक ब्यंत	ब्यंक ब्यंच ब्यंक ब्यंच	rto-to-to-to	****	especial impo	-#
æ	4 × 34 × × 34 × × 3	8 × 5 8 × 5	8 × 23 × 8	8 % % 8	X: X	1 ×
-	A 28 A 16	A 37	A 18 A 19	A 28 A 28	8. B	A 51

ANGLES.
PROPERTIES OF JONES & LAUGHLINS, LIMITED,
ANGLES WITH EQUAL LEGS.

Section.	Size.	Thickness.	Weight per foot.	Area of Section.	Distance of center of grav.to back of flange.	Moment of inertian neutral axis through center of grav. parallel to flange.	Section factor neutral axis as before.	Radius of gyration neutral axis as be- fore.	Least radius of gyration nen- tral axis through center of gravity at angle of 45 °.
No.	Inches.	In.	Lbs.	Sq. in.	In.	I	R	r	r'
A 1 A 21	6 ×6 5 ×5	7 16 7 8 8 8	17.2 33.1 11.3 23.1	$9.74 \\ 3.32$	$\frac{1.82}{1.37}$	17.68 31.92 8.13 15.74	4.07 7.64 2.22 4.52	1,88 1.78 1.55 1.39	1.25 1.17 1.03 0.93
A 2 A 3	4 ×4 3½×3½	क्षेत्र अंध्य क्षेत्र व्यक्त	9.7 18.5 8.5 17.0	2.86 5.44 2.48 5.00	1.27 $1.01$	4.36 7.66 2.87 4.77	1.52 2.81 1.15 2.03	1.24 1.14 1.07 0.96	$0.83 \\ 0.76 \\ 0.72 \\ 0.64$
A 22 A 4	34×34 3 ×3	acrete de con	7.8 14.7 4.83 12.20	2.29 4.32 1.45 3.66	$\frac{1.08}{0.84}$	2.27 2.96 1.24 2.62	0.99 1.36 0.58 1.30	0.99 0.79 0.92 0.84	0.66 0.53 0.61 0.56
A 23 A 5	2½×2½ 2½×2½	4-4-4-4	4.5 8.5 4.0 7.7	1.32 2.50 1.19 2.25	$0.87 \\ 0.72$	0.70	0.48 0.89 0.40 0.73	$0.84 \\ 0.80 \\ 0.76 \\ 0.72$	$0.56 \\ 0.53 \\ 0.51 \\ 0.48$
Λ 24 Λ 6	2½×2½ 2 ×2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3.6 6.8 1.7 5.3	1.06 $2.00$ $0.48$ $1.56$	$0.74 \\ 0.55$	0.87	0.32 0.58 0.15 0.40	0.69 0.64 0.67 0.57	0.46 0.43 0.45 0.38
A 7 A 8	1½×1½ 1½×1½	187 16 188 188 188 188	1.4 4.6 1.2 3.3	$0.42 \\ 1.30 \\ 0.36 \\ 0.99$	$0.59 \\ 0.42$			0.57 0.48 0.48 0.42	0.38 0.32 0.32 0.28
À 9 À 10	1½×1½ 1 ×1	18 14 18 16	1.0 1.9 0.8 1.2	$0.30 \\ 0.56 \\ 0.24 \\ 0.34$	$0.40 \\ 0.30$	$\begin{array}{c} 0.044 \\ 0.077 \\ 0.022 \\ 0.029 \end{array}$	0.049 0.090 0.031	0.38 0.36 0.30 0.28	0.25 0.24 0.20 0.19
A 11	4× 4	1 8 1 1 6	0.6	$0.17 \\ 0.25$	$0.23 \\ 0.26$	$0.009 \\ 0.012$		$0.22 \\ 0.21$	0.15 0.14

# RADII OF GYRATION FOR TWO EQUAL LEGGED ANGLES, PLACED BACK TO BACK.



Size,	Thick- ness,	Weight per foot of Single	B.	ADII OF	<b>GYRATI</b> O	n.
Inches.	Inches.	Angle. Lbs.	ro	r <sub>1</sub>	r,	r,
6 ×6	7 16 8	17.20 33.10	1.88 1.78	2.51 2.55	2.68 2.78	$\frac{2.77}{2.83}$
5 ×5	11	11.25 23.60	1.55 1.39	2.07 2.13	2.24 2.31	2.33 2.41
4 ×4	# #	9.70 18.50	1.24 1.14	1.68 1.71	1.86 1.90	1.95 2.00
81×81	# #	8.50 17.00	1.07 0.96	1.47 1.50	1.66 1.69	1.75 1.80
8½ × 8½	8 8 8	7.80 14.70	0.99 0.79	1.87 1.41	1.56 1.61	1.65 1.71
8 ×8	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4.90 11.40	0.92 0.84	1.25 1.29	1.43 1.48	1.53 1.59
21 × 21	1	4.50 8.50	0.84 0.80	1.15 1.18	1.34 1.38	1.44 1.48
21×21	‡ 1	4.00 7.70	0.76 0.72	1.05 1.08	1.24 1.27	1.34 1.38
21 × 21	1	8.60 6.80	0.69 0.64	0.96 0.98	1.14 1.18	1.24 1.29

# RADII OF GYRATION FOR TWO UNEQUAL LEGGED ANGLES, PLACED WITH LONGER LEGS BACK TO BACK.







Size.	Thick- ness, .	Weight per foot of Single	R	ADII OF	GYRATIO	м.
Inches.	Inches.	Angle. Lbs.	r <sub>o</sub>	r <sub>1</sub>	r,	r <sub>s</sub>
4 ×6	# 18	12.30 25.40	1.90 1.83	1.48 1.54	1.65 1.78	1.74 1.83
$3\frac{1}{2} \times 6$	# 18	11.60 24.00	1.93 1.86	1.26 1.33	1.43 1.52	1.53 1.62
4 ×5	*	11.00 21.00	1.59 1.48	1.58 1.62	1.75 1.81	1.85 1.91
$8\frac{1}{4} \times 5$	- # - #	10.40 19.80	1.60 1.48	1.33 1.37	1.51 1.56	1.60 1.66
3 ×5		9.70 18.50	1.61 1.50	1.10 1.14	1.27 1.33	1.87 1.43
$3\frac{1}{4} \times 4$	#	9.10 17.20	1.25 1.15	1.43 1.46	1.60 1.65	1.70 1.75
3 ×4	1 2	8.50 15.90	1.25 1.16	1.17 1.22	1.85 1.42	1.44
2§ × 3§	# #	7.70 14.30	1.19 1.10	1.02 1.06	1.20 1.27	1.30 1.37
3 ×31	8 4	7.80 15.80	1.08 0.99	1.21 1.26	1.39 1.46	1.48 1.56
$2\frac{1}{2} \times 3\frac{1}{2}$	1	4.90 9.40	1.12 1.05	0.96 0.98	1.13	1.23 1.27
2 <del>]</del> × 3	1 1	4.50 8.50	0.92 0.86	0.99 1.01	1.17 1.21	1.27
2 ×3 <del>1</del>	16	3.19 8.10	1.07	0.75 0.77	0.92	1.02
2 ×3	16	3.10 7.70	0.97	0.75	0.98	1.08
2 × 21	14	2.80 6.80	0.79	0.79 0.85	0.97 1.05	1.07 1.15

# RADII OF GYRATION FOR TWO UNEQUAL LEGGED ANGLES, PLACED WITH SHORTER LEGS BACK TO BACK.



Size,	Thick- ness,	Weight per foot of Single	R.	ADII OF	GYRATIO	n.
Inches.	Inches.	Angle, Lbs.	r <sub>o</sub>	r <sub>1</sub>	r,	r,
4 ×6	# 18	12.30 25.40	1.14 1.08	2.71 2.78	2.90 2.97	2.99 3.07
$3\frac{1}{2} \times 6$	12	11.60 24.00	0.98 0.98	2.81 2.88	8.00 3.08	3.09 3.18
4 ×5	8	11.00 21.00	1.20 1.11	2.20 2.23	2.88 2.43	2.48 2.53
81×5		10.40 19.80	1.02 0.98	2.27 2.29	2.45 2.49	2.55 2.58
8 ×5	‡ ‡	9.70 18.50	0.85 0.77	2.35 2.37	2.52 2.57	2.62 2.67
31×4	# #	9.10 17.20	1.06 0.97	1.74 1.76	1.92 1.96	2.02 2.06
8 ×4	8 8	8.50 15.90	0.87 0.80	1.79 1.83	1.97 2.08	2.07 2.13
24 × 34	8 8 8	7.70 14.30	0.75 0.69	1.72 1.76	1.90 1.96	2.00 2.06
3 ×81	- 8 - 8 - 4	7.80 -15.80	0.88 0.81	1.52 1.56	1.71 1.76	1.80 1.87
$2\frac{1}{2} \times 3\frac{1}{2}$	1 1	4.90 9.40	0.74 0.68	1.58 1.60	1.76 1.80	1.86 1.90
21×8	1 1	4.50 8.50	0.78 0.68	1.29 1.32	1.48 1.52	1.58 1.62
2 ×81	10	3.19 8.10	0.59 0.52	1.58 1.54	1.72 1.74	1.82 1.84
2 ×3	100	3.10 7.70	0.58 0.54	1.88 1.41	1.56 1.61	1.66 1.72
2 ×21	10	2.80 6.80	0.60 0.58	1.10 1.17	1.28 1.37	1.89 1.48

# SHEARING AND BEARING VALUE OF RIVETS.

Diam. of Rivet in inches, (		Area of	Single Shear at 6.000 lbs.	Bei	aring V	alue for (=Dian	differen	lue for different Thicknesses of Plate at 13,000 lbs. per (—Diameter of Rivet X Thickness of Plate X 12,000 lbs.)	nesses o Thickne	f Plate a	t 12,000 ] ate × 12,	Bearing Value for different Thicknesses of Plate at 18,000 lbs. per square inch. (=Diameter of Rivet X Thickness of Plate X 12,000 lbs.)	quare in	ср.
Fraction Decimal		Rivet.	per sq. fn.	<i>,,</i> ‡	**	<b>`#</b>	<b>**</b> **	*	,**	`*	**	**	<b>#</b>	3/,
ador-jo	.875 .4875	.1104	900 800 800 800	1130 1810	1640							-		
- <b>*</b> - <b>*</b> - <b>*</b> -	.5625	.1 <b>963</b>	1180	1500	1880 2110	2550 2530	2950							
-=	.625 .6875	.30 <b>6</b> 8	1840 2280	2060	28.60 28.60 28.60	2810 8090	8280 3610	4130						
44	.75 .8125	.4418 .5185	2650 8110	2250	2810 3050	3880	8940 4260	4500 4880	5060	0609				
**	875 875	.6908 .6908	<b>3610</b> <b>414</b> 0	2680 2810	8280 3520	8940 4220	4590	5250 5630	5910 6830	7080	7730			
14,	1.0625	.7854 8888	4710 5820	3000 3190	3750 3980	4500 4780	5250 5580	0000 08880 08880	6750 7190	7500 7970	8250 8770	000 828 828	10360	
##	1.125	.125 . <b>994</b> 0 .18751.1075	2860 8850	8380 8560	4830	5060 5340	5910 6230	6750 7180	7590 8020	8440 8910	9880	10180 10690	10970 11580	11810 1 <b>24</b> 70

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RIVETS
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Diam.	Diam. of Rivet in inches.	A rea of	Area of Shear at	8	Bearing Value for different Thicknesses of Plate at 15,000 lbs per square inch. (—Diameter of Rivet X Thickness of Plate X 15,000 lbs.)	alue for (-Diaz	neter of	Rivet	the for underent functionsess of risks at rayout the per ( $-$ Diameter of Rivet $\times$ Thickness of Plate $\times$ 15,000 lbs.	ses of Pl	ate X 15	,000 lbs.)	dame	ncp.
Fraction	Fraction Decimal		per sq. in.	1,4	1,91	solu.	1,21	**	1/8	1/4	/#H	**	**	1,48
<b>⇔-∤</b> 2	.4875	.1104	828 1130	1410	2050									
+~ <u>\</u>	.5625	.2485	1470	1880 2110	2840	2810 3160	3690							
<b>+</b> #	.625 .6875	.3068	2300	2340	2930	3520 3870	4100 4510	5160						
**	.75 .8125	.5185	3890 3890	2810 3050	3520	4220 4570	4920 5330	5630	6330	7620				
**	878. 3788.	.6908	4510 5180	3280 3520	4100	4920	5740 6150	6560	7380	8200	9670			
1. 1.	1.0625	.8866	5890 6650	8750 3980	4690 4980	2620	6560 6970	7500 7970	8440 8960	0886	10910 10960	11250	12950	
° ##	1.125	.125   .9940 .1875 1.1075	74 <b>60</b> 8310	4220 4450	5270 5570	88 88 88 88 88 88	7880	8440 8910	10020	10550 11180	11600	12 <b>66</b> 0 13860	18710 14470	14770 15590

Aluminum Bronze,

Zınc,

# STRENGTH OF MATERIALS.

# ULTIMATE RESISTANCE TO TENSION.

IN LBS. PER SQUARE INCH.

# METALS AND ALLOYS.

10 per cent Al. and 90 per cent. Copper, . 85000	)
11 " " 981 " " 28000	)
Brass, cast,	)
" wire, 49000	)
Bronze or gun metal,	)
Copper, cast,	)
" sheet,	)
'4 bolts,	)
" wire, unannealed, 60000	)
Iron, cast, 13,400 to 29,000,	)
" wrought, round or square bars of 1 to 2 inch	
diameter, double refined, 50000 to 54000	)
" wrought specimens 1 inch square, cut from	
large bars of double refined iron, 50000 to 53000	)
" wrought, double refined, in large bars of about	
7 square inches section, 46000 to 47000	)
" wrought, universal mill plates, angles and	
other shapes,	)
" wrought plates over 86" wide, . 46000 to 50000	
wrong no punios over ou wrong . 20000 to court	
The modulus of elasticity of double refined bar iron is 25,000,000 to 27,000,000.	3
Iron wire 70000 to 100000	)
" wire ropes,	
Lead, sheet,	-
Steel, 65000 to 120000	-
Tin, cast,	
	-

7000 to 8000

82000 to 145000

86000 to 40000

# STRENGTH OF MATERIALS-CONTINUED.

# TIMBER, SEASONED, AND OTHER ORGANIC FIBER.

Taken largely from Trautwine's pocket book (edition of 1888).

Taken largely from Trautwine's pocket book (edition of 1888).
AVERAGE
Ash, English,
" American, 16000
Beach, "
Birch,
Cedar of Lebanon,
" American, red,
" American, red,
Hempen Ropes,
Hickory, American,
Mahogany, 8000 to 21800
Oak, American white, 10000 to 18000
Oak, European, 10000 to 19800
Pine, American white, red and pitch, Memel, Riga, 10000
" " long leaf yellow, 12600 to 1920
Poplar,
Silk fiber,
Walnut, black, 16000
STONE, NATURAL AND ARTIFICIAL.
Brick and Cement,
Glass,
Glass,
Mortar, ordinary,
ULTIMATE RESISTANCE TO COMPRESSION.
METALS.

Iron,

wrought,

# WEIGHTS OF FLAT ROLLED STEEL:

# PER LINEAL FOOT.

For thicknesses from & in. to 2 in. and widths from 1 in. to 12% in.

Thick- ness in inches.	1"	11,"	1}"	14"	2''	21''	21"	24''	12"
16	.638 .850	.797 1.06	.957 1.28	1.11 1.49	1.28 1.70				7.65 10.20
8	1.49	1.33 1.59 1.86 2.12	1.59 1.92 2.23 2.55	1.86 2.23 2.60 2.98	2.98	2.87 3.85	3.19 3.72	8.51 4.09	12.75 15.30 17.85 20.40
<del>11</del>	2.12 2.84	2.39 2.65 2.92 3.19	2.87 3.19 3.51 8.88	3.35 3.72 4.09 4.47		4.78 5.26	5.84	5.84 6.43	22.95 25.50 28.05 30.60
₹ 14	2.98 3.19	3.45 3.72 3.99 4.25	4.14 4.47 4.78 5.10	4.84 5.20 5.58 5.95	5.53 5.95 6.38 6.80	6.69 7.18	7.44 7.97	8.18 8.77	33.15 35.70 38.25 40.80
1 1 8 1 1 8	$\frac{3.83}{4.04}$	4.52 4.78 5.05 5.31	5.42 5.74 6.06 6.38	6.82 6.70 7.07 7.44	7.22 7.65 8.08 8.50	8.61 9.09	9.57 10.10	11.11	45.90
18 178	4.67 4.89	5.58 5 84 6.11 6.38	6.69 7.02 7.84 7.65	8.56	9.35 9.78	10. <b>04</b> 10.52 11.00 11.48	11.69 12.22	12.85 13.44	56.10. 58.65
18 111	5.52	6.64 6.90 7.17 7.44	7.97 8.29 8.61 8.98	10.04	11.05 11.47	11.95 12.43 12.91 13.40	13.81 14.84	15.19 15.78	66.80 68.85
1 } 1 }	6.59	7.70 7.97 8.24 8.50	9.24 9.57 9.88 10.20	11.15	12.75 13.18	14.83	15.94 16.47	17.53 18.12	76.50 79.05

# WEIGHTS OF FLAT ROLLED STEEL.

# PER LINEAL FOOT.

Thick- ness in inches.	8′′	81''	3 <u>1</u> ′′	84''	4′′	41"	41''	45"	12"
3 16	1.91 2.55	2.07 2.76					2.87 3.83		7.65 10.20
16 8 7 16	3.19 3.88 4.46 5.10	4.15 4.88	4.47 5.20	4.78 5.58	5.10 5.95	5.42 6.32	5.74 6.70	6.06 7.07	12.75 15.30 17.85 20.40
76 116 116	5.74 6.38 7.02 7.65	6.22 6.91 7.60	6.70 7.44 8.18	7.17 7.97 8.76	7.65 8.50 9.35	8.18 9.08 9.98	8.61 9.57 10.52 11.48	9.09 10.10 11.11	22.95 25.50 28.05
18 18 18 18	8.29 8.93 9.57	8.98 9.67 10.36	9.67 10.41 11.16 11.90	10.36 11.16 11.95	11.05 11.90 12.75	11.74 12. <b>65</b> 18.55	12.43 13.89 14.34	18.12 14.18 15.14	88.15 35.70 88.25
11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	11.48 12.12	$12.43 \\ 18.12$	12.65 13.39 14.13 14.87	14.84 15.14	15.30 16.15	16.26 17.16	$17.22 \\ 18.17$	18.17 19.18	45.90 48.40
1# 1-7	14.08 14.66	15.20 15.88	15.62 16.36 17.10 17.85	17.58 18.83	18.70 19.55	19.87 20.77	21.04 21.99	22.21 23.22	56.10 58.6
1# 1##	16.58 17.22	17.96 18.65	18.60 19.84 20.08 20.83	20.72 21.51	22.10 22.95	23.48 24.38	24.87 25.82	26.25 27.26	66.80 68.85
1# 1##	19.13	20.72 21.41	21.57 22.81 23.06	23.91 24.70	25.50 26.35	27.10 28.00	28.69 29.64	30.28 31.29	76.50 79.00

# WEIGHTS OF FLAT ROLLED STEEL

# PER LINEAL FOOT.

Thick- ness in inches.	5''	5 <del>[</del> "	51"	54"	6"	61′′	61′′	61″	12"
16	8.19 4.25	3.35 4.46		8.67 4.89	8.88 5.10			4.30 5.74	
56 8 76	5.31 6.38 7.44	6.69 7.81	7.02 8.18	7.34 8.56	7.65 8.93	7.97 9.29	8.29 9.67	7.17 8.61 10.04	15.30 17.85
9 16	9.57	10.04	9.35 10.59	11.00	11.48	11.95	12.48	11.48 12.91 14.34	22.95
18	11.69 12.75	12.27 18.39	12.85 14.08	13.44 14.67	14.08 15.30	14.61 15.94	15.20 16.58	15.78 17.22	28.05 30.60
78	14.87 15.94	$15.62 \\ 16.74$	16.36 17.58	$17.10 \\ 18.83$	17.85 $19.18$	18.60 19.92	19.84 $20.72$	18.65 20.08 21.51 22.95	35.70 38.25
118 18 18 18 18 18	19.18 20.19	20.08 21.20	21.04 22.21	21.99 23.22	$22.95 \\ 24.23$	$28.91 \\ 25.23$	24.87 26.24	24.39 25.82 27.25	45.90 48.45
1 5 1 8	22.32 23.38	28.48 24.54	24.54 25.71	25.66 26.88	26.78 28.05	27.90 29.22	29.01 30.39	28.69 80.12 81.56 82.99	58.55 56.10
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	25.50 26.57	26.78 27.89	28.05 29.22	29.33 30.55	80.60 81.88	81.88 88.20	33.15 84.53	84.48 85.86	61.20 63.75
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	28.69 29.75	80.12 81.24	81.55 82.78	32.99 34.22	84.43 85.70	35.86 87.19	37.30 38.68	87.29 88.73 40.17	68.85 71.40
17 175	$81.87 \\ 82.94$	33.47 34.59	85.06 86.28	86.65 87.88	38.25 39.53	39.85 41.17	41.44 42.82	41.60 43.03 44.46 45.90	76.50 79.65

# WEIGHTS OF FLAT ROLLED STEEL.

# PER LINEAL FOOT.

Thick- ness in inches.	7''	71"	73′′	72"	8′′	81"	81.,	84"	12''
_	4 48	4.62	1 72	4 04	E 10	5.26	E 40	5.58	77 05
16	5.95					7.01			
<b>T</b> .	0.90	0.10	0.00	0.00	0.00	7.01	7.22	7.45	10.20
	N 44		~ ~~	0.00	0 -0				
10	7.44	7.70	7.97	8.25	8.00	8.70	8.08	9.29	12.75
8	8.98	9.25	9.57	9.88	10.20	10.52	10.84	11.16	15.30
16 16	10.41	10.78	11.16	11.53	11.90	12.27	12.64	13.02	17.85
*	11.90	12.82	12.75	13.18	13. <b>6</b> 0	14.03	14.44	14.87	20.40
_	1		l	ļ			ļ .	1	
<u> 16</u>	13.39	13.86	14.84	14.82	15.30	15.78	16.26	16.74	22.95
#	14.87	15.40	15.94	16.47	17.00	17.53	18.06	18.59	25.50
11	16.36	16.94	17.53	18.12	18.70	19.28	19.86	20.45	28.05
£	17.85	18.49	19.13	19.77	20.40	21 04	21 68	22 32	30 60
_							~1.00	~~.	00.00
11	19.84	20.03	20 72	21 41	22 10	22 70	28 48	94 17	99 1K
<del>1</del> 8	20 83	21.57	22 32	28 05	22 80	94 55	25 90	08 04	95 70
18	99 99	28.11	99 01	94 70	95 50	00 00	07 10	07 00	00.10
1	00 00	24.65	05 50	04.10	07.00	20.00	27.10	21.08	30.20
•	20.00	Ø¥.00	20.00	20.50	27.20	20.00	20.50	29.70	40.80
11	05 00	00 10	07 10			00 00			40.00
110	20.29	26.19	27.10	28.00	28.90	29.80	80.70	81.61	43.35
14	20.78	27.73	28.68	29.64	30.60	31.56	32.52	33.47	45.90
178	28.26	29.27	30.28	31.29	32.80	33.81	34.32	35.33	48.45
11	29.75	30.81	31.88	32.94	34.00	35.06	36.12	37.20	51.00
		1.	1	l		l		ł	
15	81. <b>2</b> 8	32.85	33.48	34.59	35.70	36.81	37.93	39.05	53.55
18	132.72	83.89	85.06	36.28	37.40	38.57	89.74	40 91	56 10
$1\frac{7}{16}$	34.21	35.44	<b>136.66</b>	<b>137.88</b>	139.10	40.82	41 54	42 77	58 A5
14	35.70	<b>36.9</b> 8	38.26	39.53	40.80	42.08	48.85	44.63	61 20
-		ļ					20.00		01.70
14	37.19	38.51	39.84	41.17	42.50	48.88	45 18	48 40	88 75
14	88.67	40.05	41 44	42 82	44 20	45 58	48 08	18 84	88 80
īij	40 16	41.59	AR OR	44 A7	45 00	47 89	18 78	KA 90	80 OF
116	41 A5	43.14	14 69	48 10	47 BO	40.00	50.10	EO 00	71 40
~T	¥1.00	10.14	T2.00	TU. 12	±1.00	±8.08	<b>50.00</b>	02.07	11.40
112	12 14	44 60	48 00	AP 70	40 90	E0 04	FO 90	FO 00	70 AF
178	43.14	44.00	40.22	41.70	49.80	00.84	02.38	08.92	75.95
13	44.03	46.22	47.82	49.40	51.00	52.60	54.20	55.79	76.50
118	46.12	47.76	49.41	51.05	52.70	54.85	56.00	57.64	79.05
2	47.60	49.30	[51.00]	52.70	[54.40]	<b>56.1</b> 0	[57.80]	59.50	81.60

# WEIGHTS OF FLAT ROLLED STEEL.

# PER LINEAL FOOT.

Thick- ness in inches.	9"	91"	91′′	94″	10"	101"	101″	104"	12"
ľ				6.22 8.29					7. <b>65</b> 10.20
16 8 16	11.48 18.40	11.80 13.76	12.12 14.14	10.86 12.44 14.51 16.58	12.75 14.88	18.07 15.25	18.89 15.62	13.71 15. <b>99</b>	15.30 17.85
16	17.22 19.13 21.04	17.69 19.65 21.62	18.18 20.19 22.21	18.65 20.72	19.14 21.25 23.88	19.61 21.78 23.96	20.08 22.82 24.54	20.56 22.85 25.18	22.95 25.50 28.05
1	24.86 26.78 28.69 30.60	27.52 29.49	28.26 30.28	29.01 31.08	29.75 31.88	30.50 82.67	31.24 33.48	31.98 <b>34.2</b> 8	85.70 38.25
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	32.52 34.43 36.34 38.26	35.38 37.35	36.34 38.36	37.29 39.37	38.25 40.88	89.21 41.39	40.17 42.40	41.12 48.40	45.90 48.45
1 g 1 -7 g	40.16 42.08 44.00 45.90	43.25 45.22	44.41 46.44	45.58 47.66	46.75 48.88	47.92 50.10	49.08 51.82	$50.25 \\ 52.54$	56.10 58.65
1# 1##	47.82 49.73 51.64 53.56	51.10 58.07	52.49 54.51	53.87 55.94	55.25 57.88	56.63 58.81	58.02 60.24	59.40 61.68	66.80 68.85
17 1 <del>11</del>	55.46 57.38 59.29 61.20	58.97 60.94	60.56 62.58	$62.16 \\ 64.28$	63.75 65.88	65.85 $67.52$	<b>66.94</b> <b>6</b> 9.18	68.53 70.83	76.50 79.05

# WEIGHTS OF FLAT ROLLED STEEL.

# PER LINEAL FOOT.

Thick- ness in inches.		11‡"	111	114"	12"	121"	121"	124"
16 1	7.02 9.34	7.17 9.57			7.65 10.20			
5 16 8 7 16	$14.03 \\ 16.36$	11.95 14.35 16.74 19.13	$\frac{14.68}{17.12}$	14.99 17.49	15.30 17.85	15.62 18.23	15.94 18.60	16.26 18.97
9 16 8 11 16 84	$\frac{23.38}{25.70}$	21.51 23.91 26.30 28.68	24.44 26.88	24.97 $27.47$	25.50 $28.05$	26.03 $28.64$	26.56 $29.22$	27.09 29.80
18 16 78 15 16 1	$\frac{32.72}{35.06}$	31.08 33.47 35.86 38.25	34.21 36.66	$\frac{34.95}{37.46}$	35.70 38.25	36.44 $39.05$	37.19 39.84	37.93 40.64
11	44.42	43.04	$\frac{44.00}{46.44}$	$\frac{44.94}{47.45}$	$\frac{45.90}{48.45}$	$\frac{46.86}{49.46}$	$47.82 \\ 50.46$	48.77 51.48
1 1 8 1 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	53.76	50.20 52.59 54.99 57.37	53.76 56.21	54.93 $57.43$	56.10 58.65	57.27 59.87	58.44 61.10	59.60 $62.32$
159 15 15 111 116 14	60.78 63.10	59.76 62.16 64.55 66.93	$63.54 \\ 65.98$	$64.92 \\ 67.42$	66.30 68.85	67.68 70.29	69.06 $71.72$	70.44 $73.15$
1 1 8 1 7 6 1 7 8 1 1 5 6 2 2	70.12	69.33 71.72 74.11 76.50	73.31 75.76	74.90 77.41	$\frac{76.50}{79.05}$	78.09 80.70	79.69 82.34	81.28 83.99

#### WEIGHTS AND AREAS OF SQUARE AND ROUND STEEL, ALSO CIRCUMFERENCE OF ROUND BARS.

Thickness or Diameter in Inches.	Weight of Square Bar 1 ft. long.	Weight of Round Bar 1 ft. long.	Area of Square Bar in Square Inches.	Area of Round Bar in Square Inches.	Circum- ference of Round Bar in Inches.
18	.120	.094	. 0352	.0276	.5890
\$ 5 16 8 8 7 16	.213 .832 .478 .651	.167 .261 .875 .511	.0625 .0977 .1406 .1914	.0491 .0767 .1104 .1508	.7854 .9817 1.1781 1.3744
10	.851	.668	.2500	.1963	1.5708
10	1.076	.845	.3164	.2485	1.7671
11	1.329	1.044	.3906	.3068	1.9635
11	1.608	1.263	.4727	.3712	2.1598
‡	1.914	1.508	.5625	.4418	2.3562
<del>18</del>	2.246	1.764	.6602	.5185	2.5525
<del>1</del> 5	2.605	2.046	.7656	.6018	2.7489
<del>15</del>	2.990	2.348	.8789	.6903	2.9452
1	3.402	2.672	1.0000	.7854	8.1416
16	3.841	8.017	1.1289	.8866	8.8379
8	4.306	8.382	1.2656	.9940	8.5348
8	4.798	3.768	1.4102	1.1075	8.7806
1 8 16 8 7	5.816 5.861 6.482 7.080	4.175 4.608 5.052 5.521	1.5625 1.7227 1.8906 2.0664	1.2272 1.3530 1.4849 1.6230	3.9270 4.1233 4.3197 4.5160
1	7.655	6.012	2.2500	1.7671	4.7124
16	8.306	6.524	2.4414	1.9175	4.9087
8	8.984	7.056	2.6406	2.0789	5.1051
11	9.688	7.609	2.8477	2.2365	5.3014
‡	10.419	8.183	8.0625	2.4053	5.4978
<del>}</del>	11.177	8.778	8.2852	2.5802	5.6941
<del>}</del>	11.961	9.394	8.5156	2.7612	5.8905
<del>}</del>	12.772	10.081	8.7539	2.9483	6.0868

# WEIGHTS AND AREAS OF SQUARE AND ROUND STEEL,

#### ALSO CIRCUMFERENCE OF ROUND BARS.

Note	2832 4795 8722
or Diameter in Inches.         of Square Bar in Inches.         of Square Bar in Inches.         Round Bar in Square Inches.         Round Inches.         Round Bar in Square Inches.         Round Bar in Square Inches.         Round Bar inches.         Round Inches. <t< td=""><td>of und r in hes. 2832 4795 6759</td></t<>	of und r in hes. 2832 4795 6759
Diameter   Bar   Irt. long.   Round   Bar   Inches.	2832 4795
1	2832 4795 6759
18   18   18   18   18   18   18   18	2832 4795 6759
16         14.47         11.36         4.2589         8.3410         6.           1         15.36         12.06         4.5156         3.5466         6.           1         16.28         12.79         4.7852         3.7583         6.           1         17.22         18.52         5.0625         3.9761         7.           1         18.19         14.29         5.3477         4.2000         7.           1         19.19         15.07         5.6406         4.4801         7.           20.21         15.87         5.9414         4.6664         7.           1         21.26         16.70         6.2500         4.9087         7.           23.344         17.55         6.5664         5.1572         8.           34.257         19.30         7.2227         5.6727         8.           4.257         19.30         7.2227         5.6727         8.           4.25.73         20.21         7.5625         5.9896         8.           18.24.57         21.14         7.9102         6.2126         8.           28.12         22.09         8.2656         6.4918         9.           18.29.36	4795 6759
16         14.47         11.36         4.2589         8.3410         6.           1         15.36         12.06         4.5156         3.5466         6.           1         16.28         12.79         4.7852         3.7583         6.           1         17.22         18.52         5.0625         3.9761         7.           1         18.19         14.29         5.3477         4.2000         7.           1         19.19         15.07         5.6406         4.4801         7.           20.21         15.87         5.9414         4.6664         7.           1         21.26         16.70         6.2500         4.9087         7.           23.344         17.55         6.5664         5.1572         8.           34.257         19.30         7.2227         5.6727         8.           4.257         19.30         7.2227         5.6727         8.           4.25.73         20.21         7.5625         5.9896         8.           18.24.57         21.14         7.9102         6.2126         8.           28.12         22.09         8.2656         6.4918         9.           18.29.36	4795 6759
1     17.22     18.52     5.0625     3.9761     7.       1     18.19     14.29     5.3477     4.2000     7.       1     19.19     15.07     5.6406     4.4801     7.       1     20.21     15.87     5.9414     4.6664     7.       1     21.26     16.70     6.2500     4.9087     7.       22.34     17.55     6.5664     5.1572     8.       3     23.44     18.41     6.8906     5.4119     8.       1     24.57     19.30     7.2227     5.6727     8.       2     25.78     20.21     7.5625     5.9896     8.       1     28.12     22.09     8.2656     6.4918     9.       1     29.36     23.06     8.6289     6.7771     9.       3     30.62     24.05     9.3789     7.3662     9.       1     31.91     25.06     9.3789     7.3662     9.       3     33.23     26.10     9.7656     7.6699     9.       1     34.57     27.15     10.160     7.9798     10.	6759
1     17.22     18.52     5.0625     3.9761     7.       1     18.19     14.29     5.3477     4.2000     7.       1     19.19     15.07     5.6406     4.4801     7.       1     20.21     15.87     5.9414     4.6664     7.       1     21.26     16.70     6.2500     4.9087     7.       22.34     17.55     6.5664     5.1572     8.       3     23.44     18.41     6.8906     5.4119     8.       1     24.57     19.30     7.2227     5.6727     8.       2     25.78     20.21     7.5625     5.9896     8.       1     28.12     22.09     8.2656     6.4918     9.       1     29.36     23.06     8.6289     6.7771     9.       3     30.62     24.05     9.3789     7.3662     9.       1     31.91     25.06     9.3789     7.3662     9.       3     33.23     26.10     9.7656     7.6699     9.       1     34.57     27.15     10.160     7.9798     10.	
1     17.22     18.52     5.0625     3.9761     7.       1     18.19     14.29     5.3477     4.2000     7.       1     19.19     15.07     5.6406     4.4801     7.       1     20.21     15.87     5.9414     4.6664     7.       1     21.26     16.70     6.2500     4.9087     7.       22.34     17.55     6.5664     5.1572     8.       3     23.44     18.41     6.8906     5.4119     8.       1     24.57     19.30     7.2227     5.6727     8.       2     25.78     20.21     7.5625     5.9896     8.       1     28.12     22.09     8.2656     6.4918     9.       1     29.36     23.06     8.6289     6.7771     9.       3     30.62     24.05     9.3789     7.3662     9.       1     31.91     25.06     9.3789     7.3662     9.       3     33.23     26.10     9.7656     7.6699     9.       1     34.57     27.15     10.160     7.9798     10.	8722
1     17.22     18.52     5.0625     3.9761     7.       1     18.19     14.29     5.3477     4.2000     7.       1     19.19     15.07     5.6406     4.4801     7.       1     20.21     15.87     5.9414     4.6664     7.       1     21.26     16.70     6.2500     4.9087     7.       22.34     17.55     6.5664     5.1572     8.       3     23.44     18.41     6.8906     5.4119     8.       1     24.57     19.30     7.2227     5.6727     8.       2     25.73     20.21     7.5625     5.9896     8.       1     28.12     22.09     8.2656     6.4918     9.       1     29.36     23.06     8.6289     6.7771     9.       3     30.62     24.05     9.3789     7.3662     9.       1     31.91     25.06     9.3789     7.3662     9.       1     33.23     26.10     9.7656     7.6699     9.       1     34.57     27.15     10.160     7.9798     10.	
19.19     15.07     5.6406     4.4801     7.       1 20.21     15.87     5.9414     4.6664     7.       1 21.26     16.70     6.2500     4.9087     7.       1 22.34     17.55     6.5664     5.1572     8.       1 23.44     18.41     6.8906     5.4119     8.       1 24.57     19.30     7.2227     5.6727     8.       2 25.73     20.21     7.5625     5.9896     8.       1 3 28.12     22.09     8.2656     6.4918     9.       1 4 29.86     23.06     8.6289     6.7771     9.       8 30.62     24.05     9.0000     7.0686     9.       1 31.91     25.06     9.3789     7.3662     9.       1 33.28     26.10     9.7656     7.6699     9.       1 34.57     27.15     10.160     7.9798     10.	
19.19     15.07     5.6406     4.4801     7.       1 20.21     15.87     5.9414     4.6664     7.       1 21.26     16.70     6.2500     4.9087     7.       1 22.34     17.55     6.5664     5.1572     8.       1 23.44     18.41     6.8906     5.4119     8.       1 24.57     19.30     7.2227     5.6727     8.       2 25.73     20.21     7.5625     5.9896     8.       1 3 28.12     22.09     8.2656     6.4918     9.       1 4 29.86     23.06     8.6289     6.7771     9.       8 30.62     24.05     9.0000     7.0686     9.       1 31.91     25.06     9.3789     7.3662     9.       1 33.28     26.10     9.7656     7.6699     9.       1 34.57     27.15     10.160     7.9798     10.	0686
19.19     15.07     5.6406     4.4801     7.       1 20.21     15.87     5.9414     4.6664     7.       1 21.26     16.70     6.2500     4.9087     7.       1 22.34     17.55     6.5664     5.1572     8.       1 23.44     18.41     6.8906     5.4119     8.       1 24.57     19.30     7.2227     5.6727     8.       2 25.73     20.21     7.5625     5.9896     8.       1 3 28.12     22.09     8.2656     6.4918     9.       1 4 29.86     23.06     8.6289     6.7771     9.       8 30.62     24.05     9.0000     7.0686     9.       1 31.91     25.06     9.3789     7.3662     9.       1 33.28     26.10     9.7656     7.6699     9.       1 34.57     27.15     10.160     7.9798     10.	2649
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4618
16	6576
16	OF 40
\$\frac{1}{16}\$         23.44         18.41         6.8906         5.4119         8.           \$\frac{1}{16}\$         24.57         19.30         7.2227         5.6727         8.           \$\frac{1}{16}\$         25.73         20.21         7.5625         5.9896         8.           \$\frac{1}{16}\$         26.91         21.14         7.9102         6.2126         8.           \$\frac{1}{16}\$         29.36         23.06         8.2656         6.4918         9.           \$\frac{1}{16}\$         31.91         25.06         9.3789         7.3662         9.           \$\frac{1}{16}\$         33.28         26.10         9.7656         7.6699         9.           \$\frac{1}{16}\$         34.57         27.15         10.160         7.9798         10.	
16         24.57         19.30         7.2227         5.6727         8.           4         25.73         20.21         7.5625         5.9396         8.           18         26.91         21.14         7.9102         6.2126         8.           4         28.12         22.09         8.2656         6.4918         9.           18         29.86         23.06         8.6289         6.7771         9.           8         30.62         24.05         9.0000         7.0686         9.           16         31.91         25.06         9.3789         7.3662         9.           16         33.28         26.10         9.7656         7.6699         9.           18         34.57         27.15         10.160         7.9798         10.	2467
16     25.78     20.21     7.5625     5.9896     8.       18     26.91     21.14     7.9102     6.2126     8.       18     28.12     22.09     8.2656     6.4918     9.       18     29.86     23.06     8.6289     6.7771     9.       3     30.62     24.05     9.0000     7.0686     9.       16     31.91     25.06     9.3789     7.3662     9.       16     38.23     26.10     9.7656     7.6699     9.       16     34.57     27.15     10.160     7.9798     10.	
18	<del>44</del> 00
18	6394
3         28.12         22.09         8.2656         6.4918         9.418           16         29.86         23.06         8.6289         6.7771         9.771           3         30.62         24.05         9.0000         7.0686         9.73662         9.3789         7.3662	8857
16     29.86     28.06     8.6289     6.7771     9.       8     30.62     24.05     9.0000     7.0686     9.       16     31.91     25.06     9.3789     7.3662     9.       18     33.28     26.10     9.7656     7.6699     9.       18     34.57     27.15     10.160     7.9798     10.	0321
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2284
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
33.28 26.10 9.7656 7.6699 9. 34.57 27.15 10.160 7.9798 10.	4248
	6211
	8175
1 05 04 00 00 10 500 0 0050 140	014
	210
\$\frac{1}{4}\$   \$35.94   \$28.23    \$10.563   \$8.2958    \$10.563    \$37.33    \$29.32    \$10.973    \$8.6179    \$10.563    \$10.973    \$	407
	603
40.20 31.57 11.816 9.2806 10.	799
16 20.20 01.01 11.010 0.2000 10.	
<b>1</b> 41.68 32.74 12.250 9.6211 10.	996
	192
	388
11. 46.26 36.33 13.598 10.680 11.	585
48 04 08 88 44 000 44 045 44	<b>MO1</b>
	781
10   74 00   40 40   47 040   44 700   40	977
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	174 370

#### WEIGHTS AND AREAS OF SQUARE AND ROUND STEEL, ALSO CIRCUMFERENCE OF ROUND BARS.

Thickness or Diameter in Inches.	Weight of Square Bar 1 ft. long.	Weight of Round Bar 1 ft. long.	Area of Square Bar in Square Inches.	Area of Round Bar in Square Inches.	Circum- ference of Round Bar in Inches.
4	54.45	42.77	16.000	12.566	12.566
1	57.90	45.47	17.016	13.364	12.959
1	61.47	48.28	18.063	14.186	13.352
8	65.13	51.15	19.141	15.038	13.744
1 1 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	69.81	54.88	20.250	15.904	14.187
	72.79	57.17	21.391	16.800	14.530
	76.78	60.80	22.568	17.721	14.923
	80.87	63.52	23.766	18.665	15.815
5 1 1 4 8	85.08 89.38 93.80 98.31	66.82 70.20 78.67 77.21	25.000 26.266 27.563 28.891	19.635 20.629 21.648 22.691	15.708 16.101 16.493 16.886
1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	102.94	80.85	30.250	28.758	17.279
	107.67	84.56	31.641	24.850	17.671
	112.52	88.37	33.063	25.967	18.064
	117.45	92.25	34.516	27.109	18.457
6	122.51	96.22	86.000	28.274	18.850
1	127.66	100.26	87.516	29.465	19.242
1	132.94	104.41	89.068	30.680	19.685
8	138.30	108.62	40.641	31.919	20.028
1 5 5 8 4 7 8 8 4 7 8 8	143.78	112.92	42.250	83.183	20.420
	149.85	117.30	43.891	84.472	20.813
	155.05	121.78	45.563	35.785	21.206
	160.84	125.32	47.266	87.122	21.598
7	166.75	180.97	49.000	88.485	21.991
1	172.75	135.68	50.766	39.871	22.384
1	178.87	140.48	52.563	41.282	22.777
8	185.08	145.86	54.391	42.718	23.169
1 50 s 4 7 5	191.42	150.84	56.250	44.179	23.562
	197.85	155.89	58.141	45.664	28.955
	204.39	160.58	60.063	47.178	24.847
	211.08	165.74	62.016	48.707	24.740

### WEIGHTS AND AREAS OF SQUARE AND ROUND STEEL,

#### ALSO CIRCUMFERENCE OF ROUND BARS.

Thickness or	Weight of Square	Weight of Round	Area of Square Bar in	Area of Round Bar in	Circum- ference of
Diameter	Bar	Bar	Square	Square	Round
in Inches.	1 ft. long.	1 ft. long.	Inches.	Inches.	Bar in Inches.
8.	217.78	171.04	64.000 66.016	50.265	25.133
ţ	224.64	176.48		51.849	25.525
† *	231.61	181.91	68.063	58.456	25.918
ŧ	238.68	187.46	70.141	55.088	26.311
1	245.86	198.10	72.250	56.745	26.704
1 4 5 8 H 6 7 7 8	258.14	198.82	74.891	58.426	27.096
#	260.54	204.63	76.598	60.132	27.489
ŧ	268.08	210.51	78.766	61.862	27.882
9	275.64	216.49	81.000	68.617	28.274
1	283.34	222.54	83.266	65.397	28.667
† *	291.16	228.68	85.568	67.201	29.060
ŧ	299.08	234.90	87.891	69.029	29.452
1	307.11	241.20	90.250	70.882	29.845
#	815.24	247.59	92.641	72.760	80.238
1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	323.49	254.07	95.063	74.662	30.631
ŧ	331.83	260.62	97.516	76.589	81.023
10	840.29	267.16	100.00	78.540	81.416
1	348.85	273.99	102.52	80.516	31.809
14 8	857.52	280.80	105.06	82.516	82.201
8	366.29	287.68	107.64	84.541	82.594
1	875.17	294.66	110.25	86.590	82.987
- <del>1</del> 30 sp	884.15	801.71	112.89	88.664	83.379
- <del>1</del>	393.25	308.86	115.56	90.763	83.772
7	402.44	316.08	118.27	92.886	84.165
11	411.75	323.39	121.00	95.083	84.558
1	421.16	330.78	123.77	97.205	34.950
1 1 4	430.68	338.26	126.56	99.402	85.848
#	440.30	845.81	129.89	101.62	85.739
1	450.03	353.45	132.25	108.87	36.128
\$ \$ \$	459.87	361.18	135.14	106.14	36.521
1	469.81	<b>36</b> 8.99	138.06	108.43	36.914
ŧ	479.86	376.88	141.02	110.75	37.306

# AVERAGE WEIGHT OF ROUND HEADED RIVETS PER 100.

#### LENGTH FROM UNDER HEAD.

	1			Dia	ameter.			
Length. Inches.	%	1/6	%	×	%	1	11%	11%
11			21.9				98.8	
14			24.2				100.4	
1₹			26.3				107.1	
2	7.9	16.9	28.4	38.7	56.7	83.2	114.2	158.0
21			30.6				121.4	
$2\frac{1}{4}$			32.8				128.5	
28			35.0				135.7	
8	11.0	22.5 !	37. 1	51.2	73.7	105.1	142.8	187.7
8 <del>1</del>			39.4				149.9	
8 <del>₫</del>			41.5				157.1	
8 <del>4</del>			43.7				164.2	
4	14.1	28.1	45.9	63.8	90.8	127.5	170.3	222.4
41			48.0		95.1			
41			50.2		99.3			
48			52.4		104.0			
5	17.2	83.7	54.6	76.8	108.1	149.9	198.9	258.1
5 <del>1</del>			56.7		112.2			
5 <del>₫</del> .			58.9		116.3			
5 <u>‡</u>			61.1		120.4			
6	20.4	39.3	63.2	88.7	124.4	172.4	227.5	292.7
61	21.9	42.0	67.6	95.1	133.6	183.6	240.7	810.1
7					141.8			
7 <u>1</u>					149.9			
8	26.6	50.4	80.6	114.2	159.1	217.3	283.6	362.1
81					167.8			
9					176.5			
91	31.3	58.8	93.6	132.6	184.6	249.9	325.4	410.1
10	32.8	61.5	98.0	138.7	192.8	261.1	889.7	481.
Heads	. 1.8	5.8	11.1	18.7	22.6	38.8	58.1	83.6

# AVERAGE WEIGHT OF SQUARE HEAD MACHINE BOLTS PER 100.

Length.		DIAMETER.										
	*	ı.	%	18	1/2	%	*	*	1			
11%	4.0	6.8	10.6	15.0	23.9	40.5	70.0		<b> </b>			
11/4 13/4	4.4	7.8	11.8	16.1	25.1	42.7	78.1					
2	4.7	7.8	12.0	17.2	26.3	44.8	76.2	<b></b> .				
21/4	5.1	8.4	12.6	18.2	27.7	47.0	79.8					
21/2	5.4	8.9	18.8	19.2	29.0	49.2	82.4	190.5				
214	5.8	9.5	14.0	20.2	30.4	51.4	85.5	194.7				
8	6.1	10.0	14.7	21.2	81.8	58.5	88.7	128.9	185.0			
81/2	6.8	11.1	16.0	28.2	34.7	57.9	95.0	187.4	196.0			
4	7.5	12.2	17.4	25.2	87.5	62.8	101.2	145.8	207.0			
41/4	8.2	18.2	18.7	27.2	40.2	66.7	107.5	159.2	218.0			
5	8.9	14.8	20.0	29.1	48.0	71.0	118.7	167.7	229.0			
51/2	9.6	15.4	21.4	31.2	45.7	75.4	120.0	176.1	240.0			
6	10.8	16.5	22.8	88.1	48.4	79.8	126.2	184.6	251.0			
61/2	11.0	17.6 18.6	24.1 25.9	35.1 37.1	51.2 54.0	84.1	182.5	198.0 201.4	262.0			
7	11.7 12.4	19.7	27.7	89.1	56.7	88.5 92.9	188.7 145.0	209.9	278.0 284.0			
71/2	18.1	20.8	29.5	41.0	59.4	97.2	151.2	218.8	295.0			
8	10.1	æ0.0	83.1	45.0	64.8	106.0	163.7	240.2	317.0			
10			86.7	49.0	70.8	114.7	176.2	257.1	889.0			
ii	• • • • • • •		40.4	53.0	75.8	128.5	188.7	273.9	360.0			
12		• • • • • • •	44.0	57.0	81.8	182.2	201.0	290.0	382.0			
18	••••	•••••	41.0	31.0	86.7	140.7	213.4	807.7	404.0			
14	•••••				92.2	149.2	225.9	824.5	426.0			
15				l	97.7	157.6	238.8	841.4	448.0			
16		• • • • • •			103.1	166.1	250.8	858.3	470.0			
17		•			108.6	174.6	263.2	375.2	492.0			
18				l	114.1	183.1	275.6	392.0	514.0			
19	l		l	l	119.5	191.5	288.1	408.9	596.0			
20					125.0	900.0	800.5	425.8	558.0			
Per inch ad-	1.4	2.2	8.6	4.0	5.5	8.5	12.4	16.9	22.0			

# APPROXIMATE WEIGHT OF NUTS AND BOLT HEADS, IN POUNDS.

Diam. of Bolt in inches,	14	*	%	176	1/6	%	*
Weight of Hexagon Nut   and Head	.017	.042	.057	.109	.128	.267	.43
Weight of Square Nut	.021	.049	.069	.120	.164	.820	.55
Diam. of Bolt in inches.	%	1	11/4	11/2	1%	2	21/2
Weight of Hexagon Nut )	.73	1.10	2.14	8.78	5.6	8.75	17.0
Weight of Square Nut	.88	1.81	2.56	4.42	7.0	10.5	21.0

### SIZES AND WEIGHTS OF HOT PRESSED SQUARE NUTS, UNITED STATES STANDARD SIZES.

Both weights and sizes are for unfinished nuts.

Width.	Thick- ness.	Size o	of Hole.	Size of Bolt.	Weight of 100 Nuts.	Number of Nuts in 100 lbs.
19 19 10 10 10 10 10 10 10 10 10 10 10 10 10	16 16 8 7 16	0.185 0.240 0.294 0.844	16 scant.	16 16 8 7	1.4 2.2 4.3 6.1	7270 4700 2350 1630
7 81 11 12 12	16 6 8	0.400 0.454 0.507 0.620	18 scant. 28 scant. 28 full. 5 scant.	9 15 8	9.0 11.2 15.6 26.3	1120 890 640 380
1 7 6 1 5 1 5 8 2	1 1 1 1 1	0.731 0.837 0.940 1.065	$\frac{47}{67}$ scant. $\frac{1}{16}$ full. $1_{16}$ "	1 1 1 1 1	85.7 58.8 76.9 104.2	280 170 130 96
2 1 8 2 8 2 1 8 2 1 8 2 8 2 8 2 8 2 8 2	18 11 15 14	1.160 1.284 1.389 1.491	$1\frac{5}{88}$ full. $1\frac{9}{88}$ " $1\frac{85}{84}$ scant. $1\frac{1}{4}$ "	18 13 18 18	142.8 172.4 227.8 294.1	70 58 44 84
215 31 31 316 316 31	17 2 21 21 21	1.616 1.712 1.836 1.962	15 scant. 188 '' 187 '' 187 '' 188 ''	1 <del>1</del> 2 2 <del>1</del> 2 <del>1</del>	870.4 416.7 500.0 588.2	27 24 20 17

### SIZES AND WEIGHTS OF HOT PRESSED HEXAGON NUTS, UNITED STATES STANDARD SIZES.

Both weights and sizes are for unfinished Nuts.

Wie	đth.	Thick- ness.	Size o	f Hole.	Size of Bolt.	Weight of 100 Nuts.	Number of Nuts in 100 lbs.
1		16 18 16	0.185 0.240 0.294 0.344	* scant.	16 16 8 7	1.8 1.9 3.3 5.0	7615 5200 3000 2000
. 1 1	7 8 1 1 6	1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0.400 0.454 0.507 0.620	18 scant. 25 full. 5 scant.	15 15 8	7.0 9.1 13.5 22.2	1480 1100 740 450
1 1 1 2	7 16 8 18	1 1 1 1 1 1	0.781 0.837 0.940 1.065	\$7 scant. \$7 '' \$8 full. 116 ''	1 1 1 1 1 1	32.4 46.3 67.6 90.1	309 216 148 111
2 2 2 2	8 16 8 9 16 8	18 11 18 18 18	1.160 1.284 1.389 1.491	$1\frac{5}{88}$ full. $1\frac{9}{88}$ " $1\frac{3}{88}$ scant. $1\frac{1}{2}$ "	18 11 18 18	117.5 147.1 178.6 250.0	85 68 56 40
2 3 3	15 18 5 16	17 2 21 21 21	1.616 1.712 1.836 1.962	15 scant. 185 '' 187 '' 187 '' 188 ''	1 <del>1</del> 2 2 <del>1</del> 2 <del>1</del> 2 <del>1</del>	285.7 344.8 384.6 434.8	85 29 26 28

#### UPSET SCREW ENDS, FOR ROUND AND SQUARE BARS.

Dia. of	RC	DUND	BAI	RS.	SQUARE BARS.				
Round or Side of Square Bar. Inches.	Dia. of Upset Screw End. Inches.	Dia. of Screwat Root of Thread. Inches.	Threads per Inch No.	Exces of Effective Area of ScrewEnd over Bar. Per Cent.	Dia. of Upset Screw End. Inches.	Dia of Screw at Root of Thread. Inches.	Threads per inch. No.	Excess of Effective Area of ScrewEnd over Bar Per Cent	
1	ŧ	.620	10	54	#	. <b>620</b>	10	21	
18		.620	10	21	7	.781	9	33	
# 11	1	.781 .837	9 8	37 48	1	837 .837	8	41 17	
‡ 18	1 11	.837 .940	8	25 34	1 <del>1</del> 1 <del>1</del>	.940 1.065	77	23 35	
7 18	1 <del>1</del> 1 <del>1</del>	1.065 1.065	77	48 29	1	1.160 1.160	6 6	38 20	
1	18	1.160	6	35	1 <del>1</del>	1.284	6	29	
1 1 1 6	18	1.160	6	19	1 <del>8</del>	1.389	5₃	34	
11	1 <del>1</del>	1.284	6	30	1 <del>§</del>	1.389	5 <u>1</u>	20	
11	11	1.284	6	17	1 <del>§</del>	1.490	5	24	
11	14	1.389	5 <u>1</u>	23	1 <del>7</del>	1.615	5	31	
15	14	1.490	5	29	1 <del>7</del>	1.615	5	19	
18	1 <del>1</del>	1.490	5	18	2	1.712	4 <u>1</u>	22	
17	1 <del>1</del>	1.615	5	26	21	1.837	4 <u>1</u>	28	
11/2	2	1.712	4)	30	21	1.837	4)	18	
1/4	2	1.712	4)	20	21	1.962	4)	24	
1 <del>§</del>	21	1.837	414	28	28	2.087	4 <u>1</u>	30	
1 <del>11</del>	21	1.837		18	28	2.087	4 <u>1</u>	20	
1 <del>1</del>	2 <del>1</del>	1.962	41	26	2±	2.175	4	21	
1 <del>11</del>	2 <del>1</del>	1.962	41	17	2±	2.300		26	
1 <del>1</del> 1 <del>1</del> 5	28 21	2.087 2.175	4 <u>1</u>	24 26	24 24	2.800 2.425	4	18 23	
2 21 216	2 <del>1</del> 2 <del>1</del>	2.175 2.300	4	18 24	2 <del>1</del> 2 <del>1</del> 2 <del>1</del> 2 <del>1</del> 8	2.550 2.550		28 20	
$\frac{21}{216}$	24 24	2.300 2.425		17 28	3 31	2.629 2.754		20 24	

UPSET SCREW ENDS-CONTINUED.

Dia. of	RC	DUND	BA	RS.	sq	UARE	ВА	RS.
Round or Side of Square Bar. Inches.	Dia. of Upset Screw End. Inches,	Dia. of Screw at Root of Thread. Inches.	Threads per Inch. No.	Excess of Effective Area of SorewEnd over Bar. Per cent.	Dia. of Upset Screw End. Inches.	Dia. of Screw at Root of Thread. Inches.	Threads per inch, No.	Excess of Effective Area of ScrewEnd over Bar. Per Cent.
9 <u>1</u> 2 <u>5</u>	2 <del>7</del> 2 <del>7</del>	2.550 2.550		28 22	31 31	2.754 2.879	3 <del>1</del> 31	18 22
$2\frac{8}{8} \ 2\frac{7}{16}$	3 31	2.629 2.754		28 28	38 38	3.004 3.004	3 <del>1</del> 81	26 19
$2\frac{1}{2}$ $2\frac{9}{16}$	31 31	2.754 2.879		21 26	3 <del>1</del> 3 <del>1</del>	3.100 3.225	8 <del>1</del> 8 <del>1</del>	21 24
24 2 <del>11</del>	3 <del>1</del> 38	2.879 8.004		20 25	3 <del>4</del> 34	3.225 3.317	3 <del>1</del> 3	19 20
2 <del>1</del> 2 <del>11</del>	3 <del>§</del> 3‡	3.004 3.100		19 22	3 <del>7</del> 3 <del>7</del>	3.442 3.442	_	28 18
27 218	34 34	3.225 3.225		26 21	4 44	3.567 3.692		21 24
8 8 <del>1</del>	3 <del>1</del> 3 <del>1</del>	8.817 3.442		22 21	41 48	3.692 3.928		19 24
3 <del>1</del> 3 <del>8</del>	4 41	8.567 3.692		20 20	41 48	4.028 4.158		21 19
8 <del>1</del> 8 <del>4</del>	44 44	3.798 4.028		18 23				
8‡ 8‡	45 45	4.158 4.255		28 21				

REMARKS.—As upsetting reduces the strength of iron, bars having the same diameter at root of thread as that of the bar, invariably break in the screwend, when tested to destruction, without developing the full strength of the bar. It is therefore necessary to make up for this loss in strength by an excess of metal in the upset screwends over that in the bar.

The screw threads in above table are the Franklin Institute standard.

To make one upset end for 5" length of thread allow 6" length of rod additional.

#### STANDARD SCREW THREADS, NUTS AND BOLT HEADS.

Recommended by Franklin Institute Dec. 15, 1864. And adopted by Navy Dept. of the U.S. By the R.R. Master Mechanics and Master Car-Builders Associations. By Messrs, Jones & Laughlins, Limited, and by many other of the prominent engineering and mechanical establishments of the country.



Angle of thread 60° Flat at top and bottom % of pitch.

Diam. of Screw.	Threads per inch.	Diam. at root of Thread.	Diam, of Screw.	Threads per inch.	Diam. at root of Thread.
145 6 128 7 1 1 1 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	20 18 16 14 13 12 11	.185 .240 .294 .844 .400 .454 .507	2 21 21 22 3 3 81 31 32	41 41 4 4 81 81 81	1.712 1.962 2.176 2.426 2.629 2.879 8.100 8.317
1 1	9 8 7	.731 .837 .940	4 41 41 41 5	3 3 2 <del>7</del> 2 <del>8</del> 2 <del>8</del>	8.567 8.798 4.028
1½ 1 <del>§</del> 1½ 1%	7 6 6 5 <u>1</u>	1.065 1.160 1.284 1.389	5 <del>1</del> 51	2 <del>8</del> 2 <del>1</del> 2 <del>8</del> 2 <del>8</del> 2 <del>8</del>	4.258 4.480 4.780 4.958
1# 1#	5 5	1.491 1.616	5 <u>\$</u>	2 <del>8</del> 21	5.203 5.423

Nuts and Bolt Heads are determined by the following rules, which apply to Square and Hexagon Nuts both:

Short diameter of rough nut = 1½ × diam. of bolt + ½ in.

Short diameter of finished nut = 1½ × diam. of bolt + ½ in.

Thickness of rough nut = diam. of bolt.

Thickness of finished nut = diam. of bolt  $-\frac{1}{16}$  in.

Short diameter of rough head =  $1\frac{1}{4} \times \text{diam.}$  of bolt +  $\frac{1}{4}$  in. Short diameter of finished head =  $1\frac{1}{2} \times \text{diam}$ , of bolt  $+\frac{1}{16}$  in. Thickness of rough head =  $\frac{1}{2}$  short diam, of head.

Thickness of finished head = diam, of bolt —  $\frac{1}{12}$  in. The long diameter of a hexagon nut may be obtained by multiplying the short diameter by 1.155, and the long diameter of a square aut by multiplying the short diameter by 1.414.

### SHEET IRON AND STEEL

#### WEIGHT OF SUPERFICIAL FOOT, BIRMINGHAM GAUGE.

GAUGE.	WEIGHT	IN LBs.	GAUGE.	Weight in Lbs	
	Iron.	Steel.	GZ CGZ.	Iron.	Steel.
No. 1=.3 " 2=.284 " 3=.259 " 4=.238 " 5=.22 " 6=.208 " 7=.18 " 8=.165 " 9=.148 " 10=.134 " 11=.12 " 12=.109 " 18=.095 " 14=.083	12.12 11.48 10.47 9.62 8.89 8.20 7.27 6.67 5.98 5.42 4.85 4.41 8.84	12.36 11.71 10.68 9.81 9.07 8.36 7.42 6.80 6.10 5.53 4.95 4.50 3.92 3.42	No. 16=.065 " 17=.058 " 18=.049 " 19=.042 " 20=.035 " 21=.032 " 22=.028 " 24=.022 " 25=.02 " 26=.018 " 27=.016 " 28=.013	2.63 2.34 1.98 1.76 1.40 1.25 1.12 1. .9 .8 .72 .64	2.68 2.39 2.02 1.73 1.59 1.43 1.28 1.14 1.02 .92 .82 .73 .65
" 15=.072	2.91	2.97	· 30=.012	.5	.51

## TANK IRON AND STEEL. WEIGHT OF SUPERFICIAL FOOT.

THICKNESS IN	WEIGHT	IN LBS.	THICKNESS IN	Weight in Lbs.		
Inches.	Iron.	Steel.	Inches.	Iron.	Steel.	
1 = .09125 1 = .0625 1 = .09375 1 = .125 1 = .15625 1 = .1875 1 = .21875 1 = .25 1 = .28128	1.27 2.52 3.79 5.05 6.32 7.58 8.84 10.10 11.88	1.80 2.57 3.87 5.15 6.45 7.73 9.02 10.80 11.61	\$\frac{1}{6} = .3125\$ \$\frac{1}{8} = .375\$ \$\frac{1}{76} = .4875\$ \$\frac{1}{8} = .5625\$ \$\frac{1}{8} = .6625\$ \$\frac{1}{2} = .75\$ \$\frac{1}{2} = .875\$ \$1 = 1.	12.63 15.16 17.68 20.21 22.73 25.26 80.81 85.87 40.42	12.88 15.46 18.08 20.61 23.19 25.77 30.92 86.08 41.28	

The low temperature (as compared with Iron) at which Steel Plates have to be finished, causes a slight springing of the rolls, leaving the plate thicker in the center. This, combined with greater density, causes Steel Plates, if kept up to full thickness on the edges, to weigh more than Iron. Both Iron and Steel over 72 inches wide are liable to run even heavier than the weights given above.

#### WEIGHT OF A CUBIC FOOT OF SUBSTANCES.

NAMES OF SUBSTANCES. W	erage eight. Lbs.
Aluminum	162
Anthracite, solid, of Pennsylvania	93
" broken, loose	54
" moderately shaken	58
" heaped, bushel, loose	(80)
Ash, American white, dry	38
Asphaltum	87
Brass, (Copper and Zinc,) cast	504
" rolled	524
Brick, best pressed	150
" common hard	125
" soft, inferior	100
Brickwork, pressed brick	140
" ordinary	112
Cement, hydraulic, ground, loose, American, Rosendale	56
" " Louisville	50
" " Louisville " English, Portland	90
Cherry, dry	42
Chestnut, dry	41
Clay, potters', dry	119
" in lump, loose	63
Coal, bituminous, solid	84
" broken, loose	49
" heaped bushel, loose	(74)
Coke, loose, of good coal	26
" heaped bushel	(40)
Copper, cast	542
" rolled	<b>548</b>
Earth, common loam, dry, loose	76
" " moderately rammed	95
" as a soft flowing mud	108
Ebony, dry	76
Elm, dry	35
Flint	162

#### WEIGHT OF SUBSTANCES-CONTINUED.

NAMES OF SUBSTANCES.	verage Veight. Lbs.
Glass, common window	. 157
Gneiss, common	. 168
Gold, cast, pure, or 24 carat	
" pure, hammered	. 1217
Granite	. 170
Gravel, about the same as sand which see.	
Gypsum, (plaster of paris)	. 142
Hemlock, dry	
Hickory, dry	
Hornblende, black	. 203
Ice	
Iron, cast	. 450
" wrought, purest	. 485
" " average	. 480
Ivory	. 114
Lead	. 711
Lignum Vitæ, dry	. 83
Lime, quick, ground, loose, or in small lumps	
" " thoroughly shaken	. 75
" " per struck bushel	. (66)
Limestones and Marbles	. 168
" loose, in irregular fragments	. 96
Magnesium	. 109
Mahogany, Spanish, dry	
" Honduras, dry	. 35
Maple, dry	. 49
Marbles, see Limestones.	
Masonry, of granite or limestone, well dressed	. 165
" " mortar rubble	. 154
" " dry " (well scabbled)	. 138
" sandstone, well dressed	. 144
Mercury, 32° Fahrenheit	. 849
Mica	
Mortar, hardened	
Mud, dry, close 80	

#### WEIGHT OF SUBSTANCES-CONTINUED.

NAMES OF SUBSTANCES.	Average Weight. Lbs.
Mud, wet, fluid, maximum	120
Oak, live, dry	59
" white, dry	50
" other kinds	
Petroleum	55
Pine, white, dry	25
" yellow, Northern	
" " Southern	
Platinum	1343
Quartz, common, pure	165
Rosin	69
Salt, coarse, Syracuse, N. Y	45
" Liverpool, fine, for table use	49
Sand, of pure quartz, dry, loose	90 to 106
" well shaken	99 to 117
" perfectly wet 1	20 to 140
Sandstones, fit for building	151
Shales, red or black	162
Silver	655
Slate	175
Snow, freshly fallen	5 to 12
" moistened and compacted by rain	15 to 50
Spruce, dry	
Steel	490
Sulphur	
Sycamore, dry	37
Tar	62
Tin, cast	
Turf or Peat, dry, unpressed	<b>20</b> to 30
Walnut, black, dry	
Water, pure rain or distilled, at 60° Fahrenheit	621
<sup>64</sup> 868	64
Wax, bees	60.5
Zinc or Spelter	437.5
Green timbers usually weigh from one-fifth to one-half more than d	ry.

For Diameters from to 100, advancing by Tenths.

Diam.	Area.	Circum.	Diam.	Area.	Circum.
0.0			4.0	12.5664	12.5664
.1	.007854	.81416	.1	13.2025	12.8805
.2 .3	.031416 .070686	.62832 .94248	.2	$13.8544 \\ 14.5220$	13.1947 13.5088
.4	.12566	1.2566	.4	15.2053	13.8230
.5	.19635	1.5708	.5	15.9043	14.1872
.6	.28274	1.8850	.6	16.6190	14.4518
.7	.88485	2.1991	.7	17.8494	14.765
.8 .9	.50266 .63617	2.5133 2.8274	.8 .9	18.0956 18.8574	15.0796 15.3938
1.0 .1	.7854	3.1416 3.4558	5.0	19.6350 20.4282	15.7080 16.0221
.2	.9503 1.1810	3.7699	2	21.2872	16.3363
.3	1.8278	4.0841	.3	22.0618	16.6504
.4	1,5894	4.3982	.4	22.9022	16.9646
.5	1.7671	4.7124	.5	23.7583	17.2788
.6	2.0106	5.0265	.6	24.6301	17.5929
.7 .8	2.2698	5.8407	.7	25.5176	17.9071
.9	2.5447 2.8353	5.6549 5.9690	.8 .9	26.4208 27.8897	18.2212 18.5354
2.0	3.1416	6.2832	6.0	28.2743	18.8496
.1	3.4686	6.5973	.1	29.2247	19.1637
.2	3.8013	6.9115	.2	30.1907	19.4778
.3	4.1548	7.2257	.3	31.1725	19.7920
.4	4.5239	7.5398	.4	32.1699	20.1062
.5 .6	4.9087	7.8540	.5	33.1831	20.4204
.7	5.3093 $5.7256$	8.1681 8.4828	.6 .7	84.2119 85.2565	20.7340 21.0487
.8	6.1575	8.7965	8.	36.3168	21.3628
.9	6.6052	9.1106	.9	37.3928	21.6770
8.0	7.0686	9.4248	7.0	38.4845	21.991
.1	7.5477	9.7889	.1	89.5919	22.3058
.2	8.0425	10.0531 10.3673	.2	40.7150 41.8539	22.6195 22.9336
.4	8.5530 9.0792	10.6814	.3 .4	41.8039	23.2478
.5	9.6211	10.9956	.5	44.1786	28.5619
.6	10.1788	11.3097	.6	45.3646	23.876
.7	10.7521	11.6239	7	46.5663	24.1908
.8	11.8411	11.9381	.8	47.7836	24.5044
.9	11.9459	12.2522	.9	49.0167	24.8186

Diam.	Area.	Circum.	Diam.	Area.	Circum.
8.0	50.2655	25,1327	12.0	113.0973	87.6991
.1	51. <b>5</b> 800	25.4469	.1	114.9901	88.0133
.2	52.8102	25.7611	.2	116.8987	88.8274
.8	54.1061	26.0752	.8	118.8229	38.6416
.4	55.4177	26.3894	.4	120.7628	<b>3</b> 8.9557
.5	56.7450	26.7035	.5	122.7185	39.2699
.6	58.0880	27.0177	.8	124 6898	39.5841
.7	59.4468	27.3319	.7	126.6769	39.8982
.8	60.8212	27.6460	.8	128.6796	40.2124
.9	62.2114	27.9602	.9	130.6981	40.5265
9.0	63.6173	28.2743	13.0	132.7323	40.8407
.1	65.0388	28.5885	.1	134.7822	41.1549
.2	66.4761	28.9027	.2	136.8478	41.4690
.3	67.9291	29.2168	.8	138.9291	41.7832
.4	69.3978	29.5310	.4	141.0261	42.0973
.5	70.8822	29.8451	.5	143.1388	42.4115
.6	72.3823	30.1598	.6	145.2672	42.7257
.7	78.8981	80.4784	.7	147.4114	43.0398
.8	75.4296	30.7876	.8	149.5712	43.8540
.9	76.9769	31.1018	.9	151.7468	43.6681
10.0	78.5898	81.4159	14.0	153.9380	43.9823
.1	80.1185	31.7301	.1	156.1450	44.2965
.2	81.7128	32.0442	.2	158.3677	44.6106
.3	83.3229	32.3584	.3	160.6061	44.9248
.4	84.9487	32.6726	.4	162.8602	45.2389
.5	86.5901	32.9867	.5	165.1300	45.5531
.6	88.2478	33.3009	.6	167.4155	45.8673
.7	89.9202	33.6150	.7	169.7167	46.1814
.8	91.6088	33.9292	.8	172.0836	46.4956
.9	93.3132	84.2434	.9	174.8662	46.8097
11.0	95.0332	84.5575	15.0	176.7146	47.1239
.1	96.7689	34.8717	.1	179.0786	47.4380
.2	98.5203	85.1858	.2	181.4584	47.7522
.8	100.2875	85.5000	.3	183.8539	48.0664
.4	102.0703	85.8142	.4	186.2650	48.3805
.5	103.8689	36.1283	.5	188.6919	48.6947
.6	105.6832	36.4425	.6	191.1845	49.0088
.7	107.5132	36.7566	.7	193.5928	49.8230
.8	109.3588	87.0708	.8	196.0668	49.6372
. 9	111.2202	37.3850	.9	198.5565	49.9513

Diam.	Area.	Circum.	Diam.	Area.	Circum.
16.0	201.0619	50.2655	20.0	314.1593	62.8319
.1	203.5831	50.5796	1.1	317.3087	63.1460
.2	206.1199	50.8938	.2	320.4739	63.4602
.3	208.6724	51.2080	.3	323.6547	63.7743
.4	211.2407	51.5221	.4	326.8513	64.0885
.5	213.8246	51.8363	.5	330.0636	64.4026
.6	216.4248	52.1504	.6	323.2916	64.7168
.7	219.0397	52.4646	.7	336.5353	65.0310
.8	221.6708	52.7788	.8	839.7947	65.3451
.9	224.3176	53.0929	.9	343.0698	65.6593
17.0	226.9801	53.4071	21.0	346.3606	65.9734
.1	229.6583	53.7212	.1	349.6671	66.2876
.2	232.3522	54.0354		352.9894	66.6018
.3	235.0618 237.7871	54.3496 54.6637	.3 .4	356.8273 359.6809	66.9159 67.2301
		1	li l		
.5	240.5282	54.9779 55.2920	.5 .6	363.0503 366.4354	67.5442 67.8584
.6	243.2849 246.0574	55.6062	.7	369.8361	68.1726
.7	248.8456	55.9203	.8	373.2526	68.4867
.9	251.6494	56.2345	.9	376.6848	68.8009
18.0	254.4690	56.5486	22.0	380.1327	69.1150
10.0	257.3043	56.8628	.1	383.5963	69.4292
.2	260.1553	57.1770	.2	387.0756	69.7434
.3	268.0220	57.4911	.3	390.5707	70.0575
.4	265.9044	57.8053	.4	394.0814	70.8717
.5	268.8025	58.1195	.5	397.6078	70.6858
.6	271.7164	58.4336	.6	401.1500	71.0000
.7	274.6459	58.7478	.7	404.7078	71.8142
.8	277.5911	59.0619	.8	408.2814	71.628
.9	280.5521	59.3761	.9	411.8707	71.9425
19.0	283.5287	59.6903	23.0	415.4756	72.2566
.1	286.5211	60.0044	.1	419.0963	72.5708
.2	289.5292	60.3186	.2	422.7327	72.8849
.3	292.5530	60.6327 60.9469	.3	426.3848 430.0526	73.1991 73.5138
- 1	295.5925		.4		
.5	298.6477	61.2611	.5	483.7861	73.8274
.6	301.7186	61.5752	.6	437.4354	74.1416
.7	304.8052	61.8894 62.2035	.7	441.1503 444.8809	74.4557 74.7699
.8	307.9075 311.0255	62.5177	.8	444.6009	75.0841
.8	911.0209	02.0177	ษ.	240.0215	10.0041

Diam.	Area.	Circum.	Diam.	Area.	Circum.
24.0	452.8893	75.3982	28.0	615.7522	87.9646
.1	456.1671	75.7124	.1	620.1582	88.2788
.2	459.9606	76.0265	.2	624.5800	88.5929
.8	463.7698	76.8407	.8	629.0175	88.9071
.4	467.5947	76.6549	.4	633.4707	89.2212
.5	471.4352	76.9690	.5	637.9897	89.5854
.6	475.2916	77.2832	.6	642.4243	89.8495
.7	479.1636	77.5973	.7	646.9246	90.1637
.8	483.0513	77.9115	.8	651.4407	90.4779
.9	486.9547	78.2257	.9	655.9724	90.7920
25.0	490.8739	78.5398	29.0	660.5199	91.1062
.1	494.8087	78.8540	.1	665.0830	91.4203
.2	498.7592	79.1681	.2	669.6 <b>619</b>	91.7845
.8	502.7255	79.4823	8.	674.2565	92.0487
.4	506.7075	79.7965	.4	678.8668	92.3628
.5	510.7052	80.1106	.5	<b>683.4928</b>	92.6770
.6	514.7185	80.4248	.6	688.1345	92.9911
.7	518.7476	80.7389	.7	692.7919	93.3053
.8	522.7924	81.0531	.8	697.4650	93.6195
.9	526.8529	81.3672	.9	702.1588	93.9336
26.0	530.9292	81.6814	80.0	706.8583	94.2478
.1	5 <b>8</b> 5.0211	81.9956	.1	711.5786	94.5619
.2	539.1287	82.3097	.2	716.8145	94.8761
.3	543.2521	82.6239	.8	721.0662	95.1903
.4	547.8911	82.9380	.4	725.8336	95.5044
.5	551.5459	83.2522	.5	780.6167	95.8186
.6	555.7163	88.5664	.6	785.4154	96.1827
.7	559.9025	83.8805	.7	740.2299	96.4469
.8	564.1044	84.1947	.8	745.0601	96.7611
.9	568.3220	84.5088	.9	749.9060	97.0752
27.0	572.5553	84.8280	81.0	754.7676	97.3894
1.	576.8048	85.1872	.1	759.6450	97.7035
.2	581.0690	85.4518	.2	764.5880	98.0177
.3	585.8494	85.7655	.8	769.4467	98.8319
.4	589. <b>645</b> 5	86.0796	.4	774.8712	98.6460
.5	593.9574	86.8988	.5	779.8118	98.9602
.6	598.2849	86.7080	.6	784.2672	99.2743
.7	602.6282	87.0221	7	789.2388	99.5885
.8	606.9871	87.8363	.8	794.2260	99.9026
.9	611.8618	87.6504	9	799.2290	100.2168

Diam.	Area.	Circum.	Diam.	Area.	Circum.
82.0	804.2477	100.5310	36.0	1017.8760	113.0978
.1	809.2821	100.8451	.1	1023.5387	113.4115
.2	814.3322	101.1593	.2	1029.2172	113.7257
.8	819.8980	101.4734	.8	1034.9118	114.0398
.4	824.4796	101.7876	.4	1040.6212	114.8540
.5	829.5768	102.1018	.5	1046.8467	114.668
.6	834.6898	102.4159	.6	1052.0880	114.982
.7	839.8185	102.7801	.7	1057.8449	115.296
.8	844.9628	103.0442	.8	10 <b>63.617</b> 6	115.6100
.9	850.1229	103.3584	.9	1069.4060	115.9248
83.0	855.2986	103.6726	87.0	1075.2101	116.2389
.1	860.4902	103.9867	.1	1081. <b>0299</b>	116.553
.2	865.6978	104.3009	.2	1086.8654	116.867
.8	870.9202	104.6150	.8	1092.7166	117.1814
.4	876.1588	104.9292	.4	1098.5835	117.4950
.5	881.4181	105.2434	.5	1104.4662	117.809
.6	886.6831	105.5575	.6	1110.8645	118.128
.7	891.9688	105.8717	.7	1116.2786	118.4386
.8	897.2708	106.1858	.8	1122. <b>208</b> 3	118.752
.9	902.5874	106.5000	.9	1128.1538	119.066
<b>84</b> .0	907.9208	106.8142	38.0	1134.1149	119.380
.1	913.2688	107.1283	.1	1140.0918	119.694
.2	918.6831	107.4425	.2	1146.0844	120.008
.8	924.0131	107.7566	.3	1152.0927	120.323
.4	929.4088	108.0708	.4	1158.1167	120.637
.5	934.8202	108.8849	.5	1164.1564	120.951
.6	940.2473	108.6991	.6	1170.2118	121.265
.7	945.6901	109.0133	.7	1176.2830	121.579
.8	951.1486	109.8274	.8	1182.8698	121.893
.9	956.6228	109.6416	.9	1188.4724	122.208
85.0	962.1128	109.9557	89.0	1194.5906	122.522
.1	967.6184	110.2699	.1	1200.7246	122.836
.2	978.1897	110.5841	.2	1206.8742	128.150
.8	978.6768	110.8982	.3	1213.0396	128.4640
.4	984.2296	111.2124	.4	1219.2207	123.778
.5	989.7980	111.5265	.5	1225.4175	124.0929
.6	995.8822	111.8407	.6	1231.6300	124.407
.7	1000.9821	112.1549	.7	1237.8582	124.7212
.8	1008.5977	112.4690	.8	1244.1021	125.035
.9	1012.2290	112.7832	.9	1250.8617	125.849

Diam.	Area.	Circum.	Diam.	Area.	Circum.
40.0	1256.6371	125.6637	44.0	1520.5308	138.2301
.1	1262.9281	125.9779	.1	1527.4502	188.5442
.2	1269.2848	126.2920	.2	1534.3853	138.8584
.3	1275.5573	126.6062	.8	1541.8860	139.1726
.4	1281.8955	126.9203	.4	1548.3025	139.4867
.5	1288.2493	127.2345	.5	1555.2847	139.8009
.6	1294.6189	127.5487	6.	1562.2826	140.1158
.7	1301.0042	127.8628	.7	1569.2962	140.4292
.8	1307.4052	128.1770	.8	1576.3255	140.7434
.9	1318.8219	128.4911	.9	1583.8706	141.0 <b>5</b> 75
41.0	1320.2543	128.8053	45.0	1590.4318	141.3717
.1	1326.7024	129.1195	.1	1597.5077	141.6858
.2	1333.1663	129.4336	.2	1604.5999	142.0000
.8	1339.6458	129.7478	.3	1611.7077	142.3142
.4	1346.1410	130.0619	.4	1618.8313	142.6283
.5	1352.6520	130.3761	.5	1625.9705	142.9425
.6	1359.1786	130.6903	.6	1633.1255	143.2566
.7	1365.7210	181.0044	.7	1640.2962	143.5708
.8	1372.2791	131.3186	.8	1647.4826	143.8849
.9	1378.8529	131.6327	.9	1654.6847	144.1991
42.0	1385.4424	131.9469	46.0	1661.9025	144.5183
.1	1392.0476	132.2611	.1	1669.1360	144.8274
.2	1398.6685	132.5752	.2	1676.3853	145.1416
.8	1405.3051	132.8894	.3	1683.6502	145.4557
.4	1411.9574	133.2035	.4	1690.9308	145.7699
.5	1418.6254	133.5177	.5	1698.2272	146.0841
.6	1425.3092	133.8318	.6	1705.5392	146.3982
.7	1432.0086	134.1460	.7	1712.8670	146.7124
.8	1438.7238	184.4602	.8	1720.2105	147.0265
.9	1445.4546	184.7748	9.	1727.5697	147.3407
43.0	1452.2012	135.0885	47.0	1784.9445	147.6550
.1	1458.9685	135.4026	.1	1742.3351	147.9690
.2	1465.7415	135.7168	.2	1749.7414	148.2832
.3	1472.5352	186.0310	.3	1757.1635	148.5973
.4	1479.8446	136.3451	.4	1764.6012	148.9115
.5	1486.1697	136.6593	.5	1772.0546	149.2257
.6	1493.0105	136.9734	.6	1779.5237	149.5398
.7	1499.8670	137.2876	.7	1787.0086	149.8540
.8	1506.7393	137.6018	.8	1794.5091	150.1681
.9	1513.6272	187.9159	9.	1802.0254	150.4828

Diam.	Area.	Circum.	Diam.	Area.	Circum.
48.0	1809.5574	150.7964	52.0	2128.7166	163.3628
.1	1817.1050	151.1106	.1	2131.8926	163.6770
.2	1824.6684	151.4248	.2	2140.0843	163.9911
.3	1832.2475	151.7389	.8	2148.2917	164.3053
.4	1839.8423	152.0531	.4	2156.5149	164.6195
.5	1847.4528	152.3672	.5	2164.7537	164.9336
.6	1855.0790	152. <b>6814</b>	.6	2173.0082	165.2479
.7	1862.7210	152.9956	.7	2181.2785	165.5619
.8	1870.3786	153.3097	.8	2189.5644	165.8761
.9	1878.0519	153.6239	.9	2197.8661	166.1903
49.0	1885.7409	153.9380	53.0	2206.1834	166.5044
.1	1893.4457	154.2522	.1	2214.5165	166.8186
.2	1901.1662	154.5664	.2	2222.8653	167.1327
.3	1908.9024	154.8805	.3	2231.2298	167.4469
.4	1916.6543	155.1947	.4	2239.6100	167.7610
.5	1924.4218	155.5088	.5	2248.0059	168.0752
.6	1932.2051	155.8230	.6	2256.4175	168.3894
.7	1940.0042	156.1372	.7	2264.8448	168.7035
.8	1947.8189	156.4518	.8	2273.2879	169.0177
.9	1955.6493	156.7655	.9	2281.7466	169.3318
50.0	1963.4954	157.0796	54.0	2290,2210	169.6460
.1	1971.8572	157.3938	.1	2298.7112	169.9602
.2	1979.2348	157.7080	.2	2307.2171	170.2743
.3	1987.1280	158.0221	.3	2315.7886	170.5885
.4	1995.0370	158.3363	.4	2324.2759	170.9026
.5	2002.9617	158.6504	.5	2332.8289	171.2168
.6	2010.9020	158.9646	.6	2341.3976	171.5310
.7	2018.8581	159.2787	.7	2349.9820	171.8451
.8	2026.8299	159.5929	.8	2358.5821	172.1593
.9	2034.8174	159.9071	.9	2367.1979	172.4735
51.0	2042.8206	160.2212	55.0	2375.8294	172.7876
.1	2050.8395	160.5354	.1	2384.4767	173.1017
.2	2058.8742	160.8495	.2	2393.1396	178.4159
.3	2066.9245	161.1637	.3	2401.8183	173.7301
.4	2074.9905	161.4779	.4	2410.5126	174.0442
.5	2083.0723	161.7920	.5	2419.2227	174.8584
.6	2091.1697	162.1062	.6	2427.9485	174.6726
.7	2099.2829	162.4203	.7	2436.6899	174.9867
.8	2107.4118	162.7345	.8	2445.4471	175.3009
.9	2115.5563	163.0487	.9	2454.2200	175.6150

Diam.	Area.	Circum.	Diam.	Area.	Circum.
56.0 .1 .2 .3	2463.0086 2471.8130 2480.6330 2489.4687 2498.3201	175.9292 176.2483 176.5575 176.8717 177.1858	60.0 .1 .2 .3	2827.4334 2836.8660 2846.3144 2855.7784 2865.2582	188.4956 188.8097 189.1239 189.4380 189.7522
.5 .6 .7 .8	2507.1878 2516.0701 2524.9687 2533.8830 2542.8129	177.5000 177.8141 178.1283 178.4425 178.7566	.5 .6 .7 .8	2874.7536 2884.2648 2893.7917 2903.3343 2912.8926	190.0664 190.3805 190.6947 191.0088 191.3230
57.0 .1 .2 .3	2551.7586 2560.7200 2569.6971 2578.6809 2587.6985	179.0708 179.8849 179.6991 180.0183 180.8274	61.0 .1 .2 .3	2922.4666 2932.0563 2941.6617 2951.2828 2960.9197	191.6372 191.9513 192.2655 192.5796 192.8938
.5 .6 .7 .8	2596.7227 2605.7626 2614.8183 2623.8896 2632.9767	180.6416 180.9557 181.2699 181.5841 181.8982	.5 .6 .7 .8	2970.5722 2980.2405 2989.9244 2999.6241 3009.8395	198.2079 193.5221 193.8363 194.1504 194.4646
58.0 .1 .2 .3 .4	2642.0794 2651.1979 2660.3321 2669.4820 2678.6476	182.2124 182.5265 182.8407 183.1549 183.4690	62.0 .1 .2 .3 .4	8019.0705 8028.8173 8038.5798 8048.3580 8058.1520	194.7787 195.0929 195.4071 195.7212 196.0354
.5 .6 .7 .8	2687 .8289 2697 .0259 2706 .2886 2715 .4670 2724 .7112	183.7882 184.0973 184.4115 184.7256 185.0398	.5 .6 .7 .8	8067.9616 8077.7869 8087.6279 8097.4847 8107.8571	196.3495 196.6637 196.9779 197.2920 197.6062
59.0 .1 .2 .3 .4	2733.9710 2743.2466 2752.5378 2761.8448 2771.1675	185.8540 185.6681 185.9823 186.2964 186.6106	63.0 .1 .2 .3	8117.2458 8127.1492 8137.0688 8147.0040 8156.9550	197.9208 198.2345 198.5487 198.8628 199.1770
.5 .6 .7 .8	2780.5058 2789.8599 2799.2297 2808.6152 2818.0165	186.9248 187.2389 187.5531 187.8672 188.1814	.5 .6 .7 .8	3166.9217 8176.9043 8186.9023 8196.9161 8206.9456	199.4911 199.8058 200.1195 200.4886 200.7478

Diam.	Area.	Circum.	Diam.	Area.	Circum.
<b>64</b> .0	3216.9909	201.0620	68.0	3631.6811	213.628
.1	3227.0518	201.3761	.1	3642.3704	213.942
.2	3237.1285	201.6902	.2	8653.0754	214.256
.3	3247.2222	202.0044	.3	3663.7960	214.570
.4	3257.3289	202.3186	.4	3674.5324	214.884
.5	8267.4527	202.6327	.5	3685.2845	215.199
.6	3277.5922	202.9469	.6	3696,0523	215.518
.7	3287.7474	203.2610	.7	3706.8359	215.827
.8	8297.9183	203.5752	.8	3717.6351	216.141
.9	8308.1049	203.8894	.9	3728.4500	216.455
<b>6</b> 5.0	3318.3072	204.2035	69.0	8789.2807	216.769
.1	8328.5253	204.5176	.1	3750.1270	217.084
.2	3338.7590	204.8318	.2	3760.9891	217.398
.3	8349.0085	205.1460	.3	3771.8668	217.712
.4	8359.2736	205.4602	.4	8782.7608	218.026
.5	8369.5545	205.7743	.5	3793. <b>669</b> 5	218.840
.6	8879.8510	206.0885	.6	3804.5944	218.654
.7	3390.1633	206.4026	.7	3815.5350	218.969
.8	3400.4918	206.7168	.8	3826.4913	219.288
.9	8410.8850	207.0310	.9	8837.4688	219.597
66.0	8421.1944	207.8451	70.0	8848.4510	219.911
.1	8481.5695	207.6593	.1	3859.4544	220.225
.2	8441.9608	207.9734	.2	3870.4786	220.539
.8	3452.3669	208.2876	.8	3881.5084	220.854
.4	3462.7891	208.6017	.4	3892.5590	221.168
.5	3473.2270	208.9159	.5	8908.6252	221.482
.6	3483.6807	209.2301	.6	8914.7072	221.796
.7	<b>8494</b> .1500	209.5442	.7	3925.8049	222.110
.8	8504.6851	209.8584	.8	3936.9182	222.424
.9	8515.1859	210.1725	9.	3948.0478	222.738
67.0	8525.6524	210.4867	71.0	3959.1921	223.058
.1	3536.1845	210.8009	.1	3970.8526	223.367
.2	3546.7324	211.1150	.2	3981.5289	223.681
.8	8557.2960	211.4292	.3	3992.7208	223.995
.4	8567.8754	211.7433	.4	4003.9284	224.309
.5	3578 4704	212.0575	.5	4015.1518	224.629
.6	3589.0811	212.3717	.6	4026.3908	224.938
.7	3599.7075	212.6858	.7	4037.6456	225.252
.8	8610.8497	213.0000	.8	4048.9160	225.566
.9	3621.0075	213.8141	9.	4060.2022	225.880

Diam.	Area.	Circum.	Diam.	Area.	Circum.
72.0	4071.5041	226.1947	76.0	4536.4598	238.7610
.1	4082.8217	226.5088	.1	4548.4057	239.075
.2	4094.1550	226.8230	.2	4560.3673	239.3894
.3	4105.5040	227.1371	.3	4572.8446	239.703
.4	4116.8687	227.4513	.4	4584.3377	240.0177
.5	4128.2491	227.7655	.5	4596.3464	240.3318
.6	4139.6452	228.0796	.6	4608.3708	240.6460
.7	4151.0571	228.3938	.7	4620.4110	240.9602
.8	4162.4846	228.7079	.8	4632.4669	241.2748
.9	4178.9279	229.0221	.9	4644.5384	241.588
78.0	4185.3868	229.3363	77.0	4656.6257	241.9026
.1	4196.8615	229.6504	.1	4668.7287	242.2168
.2	4208.3519	229.9646	.2	4680.8474	242.5310
.3	4219.8579	230.2787	.3	4692.9818	242.845
.4	4231.3797	230.5929	.4	4705.1319	243.1592
.5	4242.9172	230.9071	.5	4717.2977	243.4784
.6	4254.4704	231.2212	.6	4729.4792	243.7870
.7	4266.0394	231.5354	.7	4741.6765	244.1017
.8	4277.6240	231.8495	8.	4753.8894	244.4158
.9	4289.2243	232.1637	.9	4766.1181	244.7301
74.0	4300.8403	232.4779	78.0	4778.3624	245.0442
.1	4312.4721	232.7920	.1	4790.6225	245.3584
.2	4324.1195	233.1062	.2	4802.8983	245.6725
.8	4335.7827	283.4208	.8	4815.1897	245.9867
.4	4347.4616	233.7345	.4	4827.4969	246.3009
.5	4359.1562	234.0487	.5	4839.8198	246.6150
.6	4370.8664	234.3628	.6	4852.1584	246.9292
.7	4382.5924	234.6770	.7	4864.5128	247.2439
.8	4894.8841	234.9911	8.	4876.8828 4889.2685	247.5578
.9	4406.0916	235.3053	.9		247.8717
75.0	4417.8647	235.6194	79.0	4901.6699	248.1858
.1	4429.6535	235.9336	.1	4914.0871	248.5000
.2	4441.4580	236.2478	.2	4926.5199	248.8141
.8	4453.2783	236.5619	.8	4938.9685	249.1289
.4	4465.1142	236.8761	.4	4951.4328	249.4420
. 5	4476.9659	287.1902	.5	4963.9127	249.7566
.6	4488.8332	237.5044	.6	4976.4084	250.0708
.7	4500.7168	287.8186	.7	4988.9198	250.3850
.8	4512.6151	238.1327	8.	5001.4469	250.6991
.9	4524.5296	238.4469	.9	5013.9897	251.0189

Diam.	Атеа.	Circum.	Diam.	Атеа.	Circum.
			I		
80.0	5026.5482	251.3274	84.0	5541.7694	263.8938
.1	5039.1225	251.6416	.1	5554.9720	264.2079
.2	5051.7124	251.9557	.2	5568.1902	264.5221
.3	5064.3180	252.2699	.8	5581.4242	264.8363
.4	5076.9394	252.5840	.4	5594.6739	265.1514
.5	5089.5764	252.8982	.5	5607.9392	265.4646
.6	5102.2292	253.2124	.6	5621.2203	265.7787
.7	5114.8977	253.5265	.7	5634.5171	266.0929
.8	5127.5819	253.8407	.8	5647.8296	266.4071
.9	5140.2818	254.1548	9	5661.1578	266.7212
81.0	5152.9978	254.4690	85.0	5674.5017	267.0354
.1	5165.7287	254.7832	.1	5687.8614	267.3495
.2	5178.4757	255.0973	.2	5701.2367	267.6637
.3	5191.2384	255.4115	.8	5714.6277	267.9779
.4	5204.0168	255.7256	.4	5728.0345	268.2920
.5	5216.8110	256.0398	.5	5741.4569	268.6062
.6	5229.6208	256.3540	.6	5754.8951	<b>268.9203</b>
.7	5242.4463	256.6681	.7	5768.3490	269.2345
.8	5255.2876	256.9823	.0	5781.8185	269.5486
.9	5268.1446	257.2966	9.	5795.3038	269.8628
82.0	5281.0173	257.6106	86.0	5808.8048	270.1770
.1	5293.9056	257.9247	.1	5822.3215	270.4911
.2	5306.8097	258.2389	.2	5835.8539	270.8053
.3	5319.7295	258.5531	.3	5849.4020	271.1194
.4	5332.6650	258.8672	.4	5862.9659	271.4336
.5	5345.6162	259.1814	.5	5876.5454	271.7478
.6	5358.5832	259.4956	.6	5890.1407	272.0619
.7	5371.5658	259.8097	.7	5903.7516	272.3761
.8	5384.5641	260.1239	.8	5917.3783	272.6902
.9	5397.5782	260.4380	.9	5931.0206	273.0044
83.0	5410.6079	260.7522	87.0	5944.6787	273.3186
.1	5423.6584	261.0663	.1	5958.3525	273.6327
.2	5436.7146	261.3805	.2	5972.0420	273.9469
.8	<b>5449.7915</b>	261.6947	.3	5985.7472	274.2610
.4	5462.8840	262.0088	.4	5999.4681	274.5752
.5	5475.9923	262.3230	.5	6013.2047	274.8894
.6	5489.1163	262.6371	6.	6026.9570	275.2035
.7	5502.2561	262.9513	.7	6040.7250	275.5177
.8	5515.4115	263.2655	.8	6054.5088	275.8318
.9	5528.5826	263.5796	.9	6068.3082	276.1460

Diam.	Агеа.	Circum.	Diam.	Area.	Circum.
98.0	6082.1284	276.4602	92.0	6647.6101	289.0265
.1	6095.9542	276.7743	.1	6662.0692	289.3407
.2	6109.8008	277.0885	.2	6676.5441	289.6548
.3	6123.6631	277.4026	.3	6691.0347	289.9690
.4	6137.5411	277.7168	.4	6705.5410	290.2832
.5	6151.4348	278.0309	.5	6720.0630	290.5973
.6	6165.3442	278.3451	.6	6734.6008	290.9115
.7	6179.2693	278.6593	.7	6749.1542	291.2256
.8	6193.2101	278.9740	8.	6763.7283	291.5398
.9	6207.1666	279.2876	9.	6778.3082	291.8540
89.0	6221.1389	279.6017	93.0	6792.9087	292.1681
.1	6235.1268	279.9159	.1	6807.5250	292.4823
.2	6249.1804	280.2301	.2	6822.1569	292.7964
.8	6263.1498	280.5442	.8	<b>6836.8046</b>	293.1106
.4	6277.1849	280.8584	.4	6851.4680	293.4248
.5	6291.2356	281.1725	.5	6866.1471	293.7389
.6	6305.3021	281.4867	.6	6880.8419	294.0531
.7	6319.3843	281.8009	.7	6895.5524	294.3672
.8	6333.4822	282.1150	8.	6910.2786	294.6814
.9	6347.5958	282.4292	.9	6925.0205	294.9956
90.0	6361.7251	282.7433	94.0	6939.7782	295.3097
.1	6375.8701	283.0575	.1	6954.5515	295.6239
.2	6390.0809	283.3717	.2	6969.3106	295.9380
.3	6404.2073	283.6858	.8	6984.1453	296.2522
.4	6418.3995	284.0000	.4	<b>699</b> 8. <b>965</b> 8	296.5663
.5	6432.6073	284.8141	.5	7013.8019	296.8805
.6	6446.8309	284.6283	.6	7028.6538	297.1947
.7	6461.0701	284.9425	.7	7048.5214	297.5088
.8	6475.8251	285.2566	.8	7058.4047	297.8230
.9	6489.5958	285.5708	.9	7073.3033	298.1371
91.0	6503.8822	285.8849	95.0	7088.2184	298.4513
.1	6518.1843	286.1991	.1	7103.1488	298.7655
.2	6532.5021	286.5133	.2	7118.1950	299.0796
.3	6546.8856	286.8274	.8	7133.0568	299.3938
.4	6561.1848	287.1416	.4	7148.0343	299.7079
.5	6575.5498	287.4557	.5	7163.0276	800.0221
.6	6589.9304	287.7699	.6	7178.0866	800.8863
.7	6604.3268	288.0840	.7	7193.0612	800.6504
.8	6618.7388	288.3982	8.	7208.1016	300.9646
.9	6683.1666	288.7124	9.	7223.1577	801.2787

(CONTINUED.)

Diam.	Area.	Circum.	Diam.	Area.	Circum.
96.0	7238.2295	301.5929	98.0	7542.9640	807.8761
.1	7258.8170	301.9071	.1	7558.8656	808.1902
.2	7268.4202	302.2212	.2	7573.7830	308.5044
.3	7283.5391	302.5854	.3	7589.2161	308.8186
.4	7298.6737	302.8405	.4	<b>7604.664</b> 8	309.1327
.5	7313.8240	303.1687	.5	7620.1293	309.4469
.6	7328.9901	308.4779	.6	7635.6095	309.7610
.7	7344.1718	303.7920	.7	7651.1054	310.0752
.8	7359.3693	304.1062	.8	7666.6170	310.3894
.9	7374.5824	304.4208	.9	7682.1444	810.7035
97.0	7389.8118	304.7845	99.0	7697.6893	311.0177
.1	7405.0559	305.0486	.1	7718.2461	811.3818
.2	7420.3162	305.3628	.2	7728.8206	811.6460
.3	7435.5922	305.6770	.3	7744.4107	311. <b>96</b> 02
.4	7450.8839	305.9911	.4	7760.0166	812.2749
.5	7466.1913	306.3053	.5	7775.6382	812.5885
.6	7481.5144	306.6194	.6	7791.2754	312.9026
.7	7496.8532	806.9886	.7	7806.9284	313.2168
.8	7512.2078	307.2478	.8	7822.5971	313.5309
.9	7527.5780	307.5619	.9	7838.2815	313.845
	-	I	100.0	7853.9816	314.1598

To compute the area or circumference of a diameter greater than 100 and less than 1001:

Take out the area or circumference from table as though the number had one decimal, and move the decimal point two places to the right for the area, and one place for the circumference.

EXAMPLE—Wanted the area and circumference of 567. The tabular area for 56.7 is 2824.9687, and circumference 178.1283. Therefore area for 567 = 2824.968.7 and circumference = 1781.283.

To compute the area or circumference of a diameter greater than 1000:

Divide by a factor, as 2, 3, 4, 5, etc., if practicable, that will leave a quotient to be found in table, then multiply the tabular area of the quotient by the *square* of the factor, or the tabular circumference by the factor.

EXAMPLE—Wanted the area and circumference of 2109. Dividing by 3, the quotient is 703, for which the area is 888150.84, and the circumference 2208.54. Therefore area of 2109 = 888150.84  $\times$  9 = 349357.56 and circumference =  $2208.54 \times 3 = 6635.62$ ,

### LOGARITHMS OF NUMBERS.

No.	0	1	2	3	4	5	в	7	8	9	Diff
10	0000	0043	0086	0128	0170	0212	0253	0294	0334	0374	40
11	0414	0458	0492	0531	0569	0607	0645	0682	0719	0755	37
12						0969					33
13						1803					
14						1614					29
15	1761	1790	1818	1847	1875	1903	1931	1959	1987	2014	27
16	2041	2068	2095	2122	2148	2175	2201	2227	2253	2279	25
17	2304	2330	2855	2380	2405	2430	2455	2480	2504	2529	24
18						2672					
19	2788	2810	2833	2856	2878	2900	2928	2945	2967	2989	21
20	3010	3032	3054	3075	3096	3118	3139	3160	3181	3201	21
21	3222	8248	3263	3284	3304	3324	3345	3365	8385	3404	20
22						3522					19
23					3692		3729	3747	3766	3784	18
24	3802	3820	3838	3856	3874	3892	3909	3927	3945	3962	17
25	3979	3997	4014	4031	4048	4065	4082	4099	4116	4133	17
26	4150	4166	4183	4200	4216	4232	4249	<b>426</b> 5	4281	4298	16
27						4393	4409	4425	4440	4456	16
28					4533						
29	4624	4639	4654	4669	4683	4698	4718	4728	4742	4757	14
30	4771	4786	4800	4814	4829	4843	4857	4871	4886	<b>490</b> 0	14
31	4914	4928	4942	4955	4969	4988	4997	5011	5024	5038	18
32	5051	5065	5079	5092	5105	5119	5132	5145	5159	5172	13
33					5237	5250	<b>526</b> 3	5276	5289	5302	18
34						5378					18
35	5441	5453	5465	5478	5490	5502					12
36	5563	5575	5587	5599	5611	5623	<b>563</b> 5	5647	5658	5670	12
37						5740	5752	5763	5775	5786	12
38					5843	5855					12
39	5911	5922	5933	5944	5955	5966	5977	5 <b>9</b> 88	5999	6010	11
No.	0	1	2	3	4	5	в	7	8	9	Dif

#### JONES & LAUGHLINS,

FINITED.

### LOGARITHMS OF NUMBERS CONTALUE

No.	0	1	2	3	4	5	в	7	8	9	Diff.
40	6021	6031	6042	6053	6064	6075	6085	6096	6107	6117	11
41 42						6180 6284					10 10
43					6375	6385					10
44 45 46	6532	6542	6551	6561	6571	6484 6580	6590	6599	6609	6618	10 10
47					6665 6758	6767	6684 6776				9
48 49	6812	6821	6830	6839		6857		6875	6884	6893	9
50					7024	7033	7042	7050	7059	7067	9
51 52				7101 7185			7126 7210				8
53	7248	7251	7259	7267	7275		7292				8
54 55				7348 7427	7356 7425		7872 7451				8
56	7482	7490	7497	7505	7513	7520	7528	7586	7548	7551	8
57 58					7589 7664	7597	7604 7679				8
59						7745					8
60				7803			7825		-		7
61 62					7882 7952		7896 7966				7 6
63	7993	8000	8007	8014	8021	8028	8035	8041	8048	8055	7
64 65						8096 8162					7 6
66						8228					7
67						8293					6
<b>68</b> <b>69</b>						8357 8420					6
No.	0	1	2	3	4	5	в	7	8	9	Diff.

#### LOGARITHMS OF NUMBERS-CONTINUED.

Bo.	0	1	8	3	4	5	В	7	8	9	Diff
70	8451	8457	8463	8470	8476	8482	8488	8494	8500	8506	7
71	0519	0810	OFOR	0801	OFOR	OF 49	0540	OFFE	OF#1	OFOR	
						8548					6
72						8608					6
73	8038	8039	8040	8691	869.4	8663	8668	8675	8681	8686	6
74						8722					6
75											6
76	8808	8814	8820	8825	8831	8837	8842	8848	8854	8859	6
77	8865	8871	8876	8882	8887	8898	8899	8904	8910	8915	6
78	8921	8927	8932	8938	8943	8949	8954	8960	8985	8971	5
79						9004	9009	9015	9020	9025	6
80	9031	9086	9042	9047	9053	9058	9063	9069	9074	9079	6
81	0005	0000	0008	0101	0108	9112	0117	0199	0190	0100	5
82					9159	9165					_
83						9217					5
00	9191	2120	9201	8200	9212	9217	8222	9221	9252	<b>9256</b>	5
84						9269	9274	9279	9284	9289	5
85		9299				9820	9325	9330	9835	9840	5
86	9345	9350	9355	9360	9865	9370	9875	9380	9385	9890	5
87	9395	9400	9405	<b>94</b> 10	9 <b>4</b> 15	9420	9425	9430	9435	9440	5
88	9445	9450	9455	9460	9465	9469					5
89	9494	9499	9504	9509	9513	9518	9523	9528	9533	9538	4
90	9542	9547	9552	9557	9562	9566	9571	9576	9581	9586	4
91	9590	9595	9600	9605	9609	9614	9619	9624	9628	9888	5
92		9643							9675		5
93		9689							9722		4
94	9781	9786	9741	9745	9750	9754	9759	9782	078º	0772	4
95					9795						5
96					9841				9859		5
97	0989	0979	0977	0001	GOOR	9890	0904	0000	0000	0000	
98	0010	0017	0001	0001	0057	9934	0000	RADA	AAAA	PANC	4
88 80	0050	9004	0085	0040	0074	9934	PAGAR	₩¥8	9948 0001	9002	4
	- 0000	9801			4	99.19	9903		AAA 1	BAAR	4
No.	0	1	2	3	4	5	6	7	8	9	Di

# NATURAL SINES, TANGENTS AND SECANTS, ADVANCING BY 10 MIN.

Deg	Min.	Sine.	Tangent	Secant.	Deg	Min.	Sine.	Tangent	Secant.
0	00	.0000	.0000	1.0000	5	00	.0872	.0875	1.0038
-	10	.0029		1.0000	-	10	.0901	.0904	1.0041
	20	.0058		1.0000		20	.0929	.0934	1.0043
	30	.0087		1.0000		30	.0958	.0963	1.0046
	40	.0116		1.0001	1	40	.0987	.0992	1.0049
	50	.0145	.0145	1.0001		50	.1016	.1022	1.0052
1	00	.0175		1.0002	6	00	.1045		1.0055
	10	.0204		1.0002	İ	10	.1074		
	20	.0233	.0233	1.0003		20	.1108	.1110	1.0061
	30	.0262		1.0003		30	.1132	.1139	
	40	.0291		1.0004		40	.1161	.1169	
	50	.0320	.0320	1.0005		50	.1190	.1198	1.0072
2	00	.0349		1.0006	7	00	.1219		1.0075
	10	.0378		1.0007	l	10	.1248		1.0079
	20	.0407	.0407	1.0008		20	.1276	.1287	1.0082
	30	.0436		1.0010		30	.1305		1.0086
	40	.0465		1.0011	l	40	.1834		1.0090
	50	. 0494 	.0495	1.0012		50	.1363	.1376	1.0094
3	00	.0523		1.0014	8	00	.1392		1.0098
	10	.0552		1.0015		10	.1421		
	20	.0581	.0582	1.0017	l	20	.1449	.1465	1.0107
	30	.0610		1.0019		30	.1478		1.0111
	40	.0640		1.0021		40	.1507		
	50	.0669	.0670	1.0022		50	.1536	.1554	1.0120
4	00	.0698		1.0024	9	00	.1564		
	10	0727		1.0027		10	.1593		1.0129
	20	.0756	.0758	1.0029		20	. 1622	.1644	1.0134
	80	.0785		1.0031		30	.1650		
	40	.0814		1.0033		40	.1679		
	50	0843	.0846	1.0036		50	.1708	.1788	1.0149

Deg	Min.	Sine.	Tangent ·	Secant.	Deg	Min.	Sine.	Tangent	Secant.
10	00	.1736	.1763	1.0154	15	00	.2588	.2679	1.0358
	10	.1765	.1793	1.0160		10	.2616	.2711	1.0361
	20	.1794	.1823	1.0165		20	.2644	.2742	1.0369
	30	.1822	.1853	1.0170		30	.2672	.2778	1.0377
	40	.1851	.1883	1.0176		40	.2700	.2805	1.0386
	50	.1880	.1914	1.0181		50	.2728	.2836	1.0394
11	00	.1908	.1944	1.0187	16	00	.2756	.2867	1.0409
	10	. 1937	.1974	1.0193	1 1	10	.2784	.2899	1.0412
	20	.1965	.2004	1.0199		20	.2812	.2931	1.0421
	30	.1994	.2035	1.0205		30	. 2840	.2962	1.0429
	40	.2022	.2065	1.0211	1 1	40	.2868	.2994	1.0439
	50	.2051	.2095	1.0217		50	. 2896	.3026	1.0448
12	00	.2079	.2126		17	00	.2924	. 3057	1.0457
	10	.2108		1.0230	1 1	10	.2952	.3089	1.0466
	20	.2136	.2186	1.0236		20	.2979	.3121	1.0476
	30	.2164	.2217	1.0243		80	.8007	. 3153	1.0485
	40	.2193	.2247	1.0249	1 1	40	.8085	.3185	1.0495
	50	.2221	.2278	1.0256		50	.3062	.3217	1.0505
13	00	. 2250	.2309	1.0263	18	00	.3090	.8249	1.0515
	10	.2278	.2339	1.0270		10	.3118	.3281	1.0525
	20	.2306	.2370	1.0277		20	.3145	.3314	1.0535
	30	.2334	.2401	1.0284		30	.8178	.3346	1.0545
	40	.2363	.2432	1.0291		40	.3201	.3378	1.0555
	50	.2391	.2462	1.0299		50	. 3228	.8411	1.0566
14	00	.2419	.2493		19	00	.3256	.3443	1.0576
	10	.2447	.2524	1.0814		10	.3283	.8476	1.0587
	20	.2476	.2555	1.0321		20	.3311	.3508	1.0598
	80	.2504	.2586	1.0829		30	. 3338	.8541	1.0608
	40 50	.2582	.2617	1.0337		40	3365	.3574	1.0619
	וסט	. 2560	.2648	1.0345		50	.3393	.3607	1.0631

Deg	Min.	Sine.	Tangent	Secant.	Deg	Min.	Sine.	Tangent	Secant.
20	00	. 3420	. 3640	1.0642	25	00	.4226	.4663	1,103
	10	.3448	.3673	1.0653		10	.4253	.4699	1.1049
	20	.8475	.3706	1.0665		20	. 4279	.4734	1.106
	30	. 3502		1.0676		30	.4305	.4770	1.107
	40	.3529		1.0688		40	.4331	.4806	1.109
	50	. 8557	.3805	1.0700		50	.4358	.4841	1.111
21	00	.3584	.3839	1.0711	26	00	.4384	.4877	1.112
	10	.3611	.3872	1.0723		10	.4410		1.114
	20	. 3638	.3906	1.0736		20	.4436	.4950	1.115
	30	.3665		1.0748		30	.4462	.4986	1.117
	40	.3692		1.0760	i i	40	.4488		1.119
	50	.3719	.4006	1.0773		50	.4514	.5059	1.120
22	00	.3746		1.0785	27	00	. 4540		1.122
	10	.8773		1.0798		10	.4566		1.124
	20	.3800	.4108	1.0811		20	. 4592	.5169	1.125
	30	.3827		1.0824		30	.4617		1.127
i	40	.3854	.4176	1.0837		40 50	.4643	.5243	1.129
	50	.3881	.4210	1.0850		ĐΨ	.4669	.5280	1.130
23	00	.3907	.4245	1.0864	28	00	. 4695	.5317	1.132
	10 20	.3934 .3961	.4279 .4314	1.0877 1.0891		10 20	.4720 $.4746$	.5354 .5392	1.134 1.136
	20	.0801	.4014	1.0091		20	.4740	.0082	1.100
	30	. 3987	.4348	1.0904		30	.4772		1.137
	40 50	.4014		1.0918		40 50	.4797 $.4823$	.5467 .5505	1.139 $1.141$
	90	.4041	.4417	1.0932	]. '	90	.4020	.0000	1.141
24	00	.4067	.4452	1.0946	29	00	.4848	.5543	
	10	.4094		1.0961		10	.4874	.5581	1.145
	20	.4120	.4522	1.0975		20	.4899	.5619	1.147
	30	.4147	.4557	1.0989		30	.4924	.5658	1.149
	40	.4173		1.1004		40	.4950		1.150 1.152
	50	. <b>42</b> 00	.4628	1.1019	1	50	.4975	.5735	1.10%

Deg	Min.	Sine.	Tangent	Secant.	Deg	Min.	Sine.	Tangent	Secant.
80	00	.5000	.5774	1.1547	35	00	. 5736	.7002	1.2208
	10	.5025	.5812	1.1566		10	.5760		1.2238
	20	.5050		1.1586		20	.5783		1.2258
	30	.5075	.5890	1.1606		30	.5807	.7138	1.2288
	40	.5100		1.1626		40	.5831	.7177	1.2309
	50	.5125	.5969	1.1646		50	.5854	.7221	1.2335
81	00	.5150		1.1666	36	00	.5878	.7265	1.2361
	10	.5175	.6048	1.1687		10	.5901	.7810	1.2387
	20	.5200	.6088	1.1707		20	.5925	.7355	1.2418
	30	. 5225		1.1728		30	.5948	.7400	1.2440
	40	.5250	.6168	1.1749		40	.5972	.7445	1.2467
	50	.5275	.6208	1.1770		50	.5995	.7490	1.2494
82	00	.5299	.6249	1.1792	37	00	.6018	. 7586	1.2521
	10	.5324		1.1813		10	.6041	.7581	1.2549
	20	.5348	.6330	1.1835		20	.6065	.7627	1.2577
	30	.5873		1.1857		30	.6088	.7678	1.2605
	40	.5398		1.1879		40	.6111	.7720	1.263
	50	.5422	.6453	1.1901	'	50	.6134	.7766	1.2661
33	00 10	.5446 .5471	.6494 .6536	1.1924 1.1946	38	00 10	.6157 .6180	.7813 .7860	1.2690
	20			1.1940		20	.6202	.7907	1.2748
	20	5495	.0077	1.1909		20	. 6202	.7807	1.2740
	30	. 5519		1.1992		30	.6225	.7954	1.2778
	40	.5544	.6661	1.2015		40	.6248	.8002	1.2808
	50	.5568	.6703	1.2039		50	.6271	.8050	1.2837
84	00	.5592		1.2062	39	00	.6293	.8098	1.2868
	10	.5616		1.2086	1	10	. 6316	.8146	1.289
	20	.5640	.6830	1.2110		20	.6338	.8195	1.2929
	30	.5664		1.2184	1	30	.6861	.8243	1.2960
	40	.5688		1.2158	1	40	.6383	.8292	1.2991
	50	.5712	.6959	1.2183		50	.6406	.8342	1.3022

Deg	Min.	Sine.	Tangent	Secant.	Deg	Min.	Sine.	Tangent	Secant.
40	00	.6428	.8891	1.3054	45	00	.7071	1.0000	1.414
	10	.6450		1.3086		10		1.0058	1.418
	20	.6472		1.3118		20		1.0117	1.422
	30	. 6494		1.8151		30		1.0176	1.426
	40	.6517		1.3184	٠.	40		1.0235	1.431
	50	.6539	.8642	1.3217		50	.7178	1.0295	1.435
41	00	.6561	.8693	1.3250	46	00		1.0355	1.439
	10	.6583		1.3284		10		1.0416	1.448
	20	.6604	.8796	1.3318		20	. 7284	1.0477	1.448
	30	.6626	.8847	1:3352		30	.7254	1.0538	1.452
	40	.6648	.8899	1.3386		40	.7274	1.0599	1.457
	50	.6670	.8952	1.8421		50	.7294	1.0661	1.461
42	00	.6691		1.3456	47	00		1.0724	1.466
	10	.6713		1.3492	1	10	. 7333	1.0786	1.470
	20	.6784	.9110	1.3527		20	.7 <b>8</b> 53	1.0850	1.475
	30	. 6756		1.3563		30		1.0913	1.480
	40	.6777		1.8600		40		1.0977	1.484
	50	.6799	.9271	1.3636		50	.7412	1.1041	1.489
<b>4</b> 3	00	.6820		1.3678		00	.7481	1.1106	1.494
	10	.6841		1.3711		10 20	7470	1.1171 1.1237	1.499 1.504
	20	.6862	.9435	1.3748		20	. 7470	1.1207	1.504
	30	.6884		1.3786		30		1.1303	
	40	.6905		1.3824		40	.7509	1.1869	1.514
	50	.6926	.9601	1.3863		50	. 7528	1.1436	1.519
44	00	.6947		1.3902	49	00		1.1504	1.524
	10	.6967		1.8941		10		1.1571	1.529
	20	.6988	.9770	1.3980		20	7585	1.1640	1.534
	30	.7009		1.4020		80		1.1708	1.539
	40	7030		1.4061		40		1.1778	1.545
	50	.7050	.9942	1.4101	l i	50	.7642	1.1847	1.550

#### NATURAL SINES, TANGENTS AND SECANTS.

(CONTINUED.)

Deg	Min.	Sine.	Tangent	Secant.	Deg	Min.	Sine.	Tangent	Secant.
50	00	.7660	1.1918	1.5557	55	00	8192	1.4281	1.7434
- 1	10		1.1988	1.5611		10		1.4370	1.7507
	20		1.2059	1.5666		20		1.4460	1.7581
	30		1.2181	1.5721		30		1.4550	1.7655
	40		1.2203	1.5777	1 1	40		1.4641	1.7730
	50	.7753	1.2276	1.5833		50	.8274	1.4783	1.7800
51	00		1.2349	1.5890	56	00		1.4826	1.788
	10		1.2423	1.5948		10		1.4919	1.790
	20	.7808	1.2497	1.6005		20	. 8323	1.5013	1.803
	30	.7826	1.2572	1.6064		30		1.5108	1.8118
	40		1.2647	1.6123		40		1.5204	1.8196
	50	.7862	1.2723	1.6183		50	.8371	1.5301	1.8279
52	00		1.2799	1.6243	57	00		1.5399	1.8361
	10		1:2876	1.6303		10		1.5497	1.844
	20	.7916	1.2954	1.6365		20	.8418	1.5597	1.852
1	30		1.3032	1.6427		30		1.5697	1.861
	40		1.3111	1.6489		40		1.5798	1.8699
	50	.7969	1.3190	1.6553		50	.8465	1.5900	1.878
53	00		1.8270		58	00		1.6003	1.887
	10		1.3352	1.6681		10		1.6107	1.8959
	20	.8021	4.3432	1.6746		20	.8511	1.6213	1.9048
	30		1.3514	1.6812		30		1.6319	1.9139
	40		1.3597	1.6878	1 1	40		1.6426	1.9230
	50	.8073	1.3680	1.6945		50	.8557	1.6534	1.932
54	00		1.3764	1.7018	59	00		1.6643	1.9410
	10		1.3848	1.7081		10		1.6753	1.951
	20	.8124	1.3934	1.7151		20	.8601	1.6864	1.9600
	30		1.4019	1.7221		30		1.6977	1.970
	40		1.4106	1.7291		40		1.7090	1.980
1	50	.8175	1.4193	1.7362	1 1	50	.8646	1.7205	1.9900

#### NATURAL SINES, TANGENTS AND SECANTS.

(CONTINUED.)

Deg	Min.	Sine.	Tangent	Secant.	Deg	Min.	Sine.	Tangent	Secant.
60	90	.8660	1,7321	2.0000	65	00	.9063	2.1445	2.366
	10	.8675	1.7437	2.0101		10	.9075	2.1609	2.381
	20	.8689	1.7556	2.0204		20	.9088	2.1775	2.396
	30		1.7675	2.0308		80		2.1943	2.411
	40		1.7796	2.0413	1	40		2.2113	2.426
	50	.8732	1.7917	2.0519		50	. 9124	2.2286	2.442
61	00		1.8040	2.0627	66	00		2.2460	2.458
	10		1.8165	2.0736		10		2.2637	2.474
	20	.8774	1.8291	2.0846		20	. 9159	2.2817	2.491
	30		1.8418	2.0957		30		2.2998	2.507
	40		1.8546	2.1070	1	40		2.3183	2.524
	50	.8816	1.8676	2.1185		50	.9194	2.3369	2.541
62	00		1.8807	2.1301	67	00		2.3559	2.559
	10		1.8940	2.1418		10		2.3750	
	20	.8857	1.9074	2.1537		20	.9228	2.3945	2.594
	30		1.9210	2.1657		80		2.4141	2.619
	40		1.9347	2.1786		40		2.4342	2.631
	50	.8897	1.9486	2.1902		50	9261	2.4545	2.650
63	00		1.9626	2.2027	68	00		2.4751	2.669
	10		1.9768			10		2.4960	2.688
	20	.8986	1.9912	2.2282		20 	.9293 	2.5172	2.708
	30		2.0057			80		2.5386	
	40		2.0204	2.2543	H	40		2.5605	
	50	.8 <b>9</b> 75	2.0353	2.2677		50	.9825	2.5826	2.769
64	00		2.0503	2.2812	69	00		2.6051	2.790
	10	1.9001	2.0655	2.2949		10		2.6279	
	20	.9013	2.0809	2.3088		20	.9356 	2.6511	2.833
	30		2.0965			30		2.6746	
	40		2.1128	2.3371	1	40.		2.6985	
	50	.9051	2.1288	2.3515	11	50	.9387	2.7228	2.900

#### NATURAL SINES, TANGENTS AND SECANTS.

(CONTINUED.)

Deg	Min.	Sine.	Tangent	Secant.	Deg	Min.	Sine.	Tangent	Secant.
70	-00	9397	2.7475	2.9238	75	00	9859	3.7321	3.8637
••	10		2.7725	2.9474		10		3.7760	3.906
	20		2.7980	2.9713		20		3.8208	3.949
	30		2.8239	2.9957		30		3.8667	3.993
	40		2.8502	3.0206		40		3.9136	4.039
	50	. 9446	2.8770	3.0458		50	. 9696	3.9617	4.085
71	00		2.9042	3.0716	76	00		4.0108	4.133
	10		[2.9319]	3.0977				4.0611	4.182
	20	.9474	2.9600	3.1244		20	.9717	4.1126	4.232
	30		2.9887	8.1515		30		4.1653	
	40		3.0178	3.1792		40		4.2198	
	50	. 9502	3.0475	8.2074		50	.9737	4.2747	4.390
72	00		3.0777	8.2361	77	00		4.3315	4.445
	10		3.1084	3.2653		10		4.3897	
	20	.9528	3.1397	3.2951		20	. 9757	4.4494	4.560
	30		3.1716	3.3255		30		4.5107	4.620
	40		3.2041	8.8565	ĺ	40		4.5736	4.681
	50	.9555	3.2371	3.3881		50	.9770	4.6382	4.744
73	00		3.2709	8.4203	78	00 10		$4.7046 \\ 4.7729$	
	10		3.3052	3.4532	1	20			4.945
	20	. 9580	3.3402	3.4867		20	.9193	4.8430	4.840
	30		3.3759	3.5209		30 40		4.9152 4.9894	5.015 5.088
	40		3.4124	3.5559					
	50	. 9605	3.4495	3.5915		50	.9011	5.0658	5.163
74	00		3.4874	3.6280	79	00		5.1446	5.240 5.320
	10		3.5261	3.6652		10		5.2257	
	20	.9628	3.5656	3.7032		20	.9827	5.3093	5.402
	30		3.6059	8.7420		80		5.3955	
	40		3.6470	3.7817	1	40		5.4845	
	50	. ₩552	3.6891	8.8222		50	. 9843	5.5764	5.665

# NATURAL SINES, TANGENTS AND SECANTS. (CONTINUED.)

Deg	Min.	Sine.	Tangent	Secant.	Deg	Min.	Sine.	Tangent	Secant.
80	00	.9848	5.6713	5.7588	85	00	.9962	11.430	11.474
27	10	.9853	5.7694	5.8554	17.7	10		11.826	11.868
	20	.9858	5.8708			20	.9967	12.251	12.291
	30	.9863	5.9758	6.0589		30	.9969	12.706	12.745
	40	.9868		6.1661		40	.9971	13.197	13.235
	50	.9872	6.1970	6.2772		50	.9974	13.727	13.763
81	00	.9877	6.3138	6.3925	98	00	.9976	14.301	14.336
91	10	.9881	6.4348		00	10		14.924	14.958
							.9978		
	20	.9886	6.5606	6.6363		20	.9980	15.605	15.637
	30	.9890		6.7655		30	.9981	16.350	
	40	.9894	6.8269	6.8998		40	.9983	17.169	17.198
	50	.9899	6.9682	7.0396		50	.9985	18.075	18.108
82	00	.9903	7.1154	7.1853	87	00	.9986	19.081	19.107
	10	.9907	7.2687	7.3372		10	.9988		
	20	.9911	6.4287	7.4957		20	.9989		
	30	.9914	7.5958	7.6613		30	.9990	22.904	22.926
	40	.9918	7.7704	7.8344		40	.9992	24.542	24.562
	50	.9922	7.9530	8,0156		50	.9993		26.451
83	00	.9925	8.1443	8.2055	88	00	.9994	28,636	28.654
-	10	.9929			00	10	.9995		31.258
	20	.9932	8.5555	8.6138		20	.9996		34.382
	30	.9936	8.7769	8.8337		30	,9997	38,188	38.202
	40	.9939				40	.9997	42.964	42.976
	50					50			
	90	.9942	9.2553	9.3092		90	.9998	49.104	49.114
84	00	.9945			89	00			
	10	.9948	9.7882	9.8391		10	.9999	68.750	68.757
	20	.9951	10.0780	10.1275		20	.9999	85.940	85.946
	30	.9954	10.3854	10.4334		30	1.0000	114.589	114,598
	40		10.7119					171.885	
	50		11.0594					343.774	
				1-	90	00	1 0000	Infinite.	T. Carlton

#### SQUARES, CUBES, SQUARE ROOTS & CUBE ROOTS.

Nos.	Squares.	Cubes.	Square Root.	Root.	Nos.	Squares.	Cubes.	Square Root.	Cube Root.
1	1	1	1.000	1.090	51	26 01	132 651	7.141	3.708
2	1 4	8	1.414	1.260	52	27 04	140 608	7.211	8.733
8	9	27	1.789	1.442	53	28 09	148 877	7.280	3.756
4	16	64	2.000	1.587	54	29 16	157 464	7.849	8.780
5	25	125	2.236	1.710	55	80 25	166 375	7.416	8.808
6	86	216	2.449	1.817	56	31, 36	175 616	7.488	3.826
7	49	348	2.646	1.918	57	82 49	185 198	7.550	3.849
8	64	512	2.828	2.000	58	83 64	195 119	7.616	8.871
9	81	729	8.000	2.000	59	84 81	205 379	7.681	3.898
10	1 00	1 000	3.162	2.154	60	86 00	216 000	7.746	3.915
11	1 21	1 381	3.817	2.224	61	87 21	226 981	7.810	8.937
12	1 44	1 728	8.464	2.289	62	<b>38 44</b>	238 328	7.874	3.958
18	1 69	2 197	3.606	2.351	63	89 69	250 047	7.987	8.979
14	1 96	2 744	8.742	2.410	64	40 96	262 144	8.000	4.000
15	2 25	3 875	8.878	2.466	65	42 25	274 625	8.062	4.021
16	2 56	4 096	4.000	2.520	66	48 56	287 496	8.124	4.041
17	2 89	4 913	4.128	2.571	67	44 89	800 768	8.185	4.062
18	3 24	5 832	4.248	2.621	68	46 24	814 432	8.246	4.082
19	8 61	6 859	4.859	2.668	69	47 61	828 509	8.307	4.102
20	4 00	8 000	4.472	2.714	70	49 00	348 600	8.367	4.121
21	4 41	9 261	4.588	2.759	71	50 41	857 911	8.426	4.141
22	4 84	10 648	4.690	2.802	72	51 84	878 248	8.485	4.160
28	5 29	12 167	4.798	2.844	78	53 29	889 017	8.544	4.179
24	5 76	13 824	4.899	2.885	74	54 76	405 224	8.602	4.198
25	6 25	15 625	5.000	2.924	75	56 25	421 875	8.660	4.217
26	6 76	17 576	5.099	2.968	76	57 76	438 976	8.718	4.236
27	7 29	19 683	5.196	8.000	77	59 29	456 533	8.775	4.254
28 29	7 84	21 952	5.292	3.037	78	60 84	474 552	8.882	4.278
Z9	8 41	24 889	5.385	8.072	79	62 41	498 089	8.888	4.291
80	9 00	27 000	5.477	3.107	80	64 00	512 000	8.944	4.309
31	9 61	29 791	5.568	8.141	81	65 61	581 441	9.000	4.327
32 33	10 24	32 768	5.657	8.175	82	67 24	551 368	9.055	4.845
	10 89	85 987	5.745	3.208	88	68 89	571 787	9.110	4.862
34 85	11 56 12 25	39 304 42 875	5.881 5.916	3.240 3.271	84 85	70 56 72 25	592 704 614 125	9.165	4.897
36	12 96	46 656	6.000	8.302	86	73 96	686 056	9.274	
87	18 69	50 653	6.088	8.882	87	75 69	658 508	9.327	4.414
38	14 44	54 872	6.164	8.862	88	77 44	681 472	9.381	4.481
39	15 21	59 819	6.245	8.391	89	79 21	704 969	9.484	4.448
40	16 00	64 000	6.825	8.420	90	81 00	729 000	9.487	4.481
41	16 81	68 921	6.408	8.448	91	82 81	758 571	9.539	4.498
42	17 64	74 088	6.481	8.476	92	84 64	778 688	9.592	4.514
48	18 49	79 507	6.557	8.508	93	86 49	804 857	9 644	4.581
44	19 86	85 184	6.638	8.530	94	88 36	830 584	9.695	4.547
45	20 25	91 125	6.708	8.557	95	90 25	867 375	9.747	4.568
46	21 16	97 336	6.782	3.588	96	92 16	884 786	9.798	4.579
47	22 09	103 828	6.856	8.609	97	94 09	912 678	9.849	4.595
48	23 04	110 592	6.928	8.684	98	96 04	941 192	9.900	4.610
49	24 01	117 649	7.000	8.659	99	98 01	970 299	9.950	4.696
50	25 00	125 000	7.071	8.684	100		1000 000	10.000	4.643
					1		- 300 000	1-0.000	

#### SQUARES, OFFICE, SQUARE ROOTS & CUBE ROOTS.

## SQUARES, CUBES, SQUARE ROOTS & CUBE ROOTS. (CONTINUED.)

===			- Bonera	Cube		<del></del>		Square	Cube
Kos.	Squares.	Cubes.	Square Root.	Root.	Nos.	Squares.	Cubes.	Root.	Root.
201	4 04 01	8 120 601	14.1774	5.8578	251	6 30 01		15.8430	6.8080
202	4 08 04	8 242 408			252	6 85 04	16 008 008	15.8745	6.8164
208	4 19 09	8 365 427	14.2478	5.8771	258	6 40 09	16 194 277 16 387 064	15.9060	6.8947
204	4 16 16	8 489 664	14.2829	5.8868	254	6 45 16	16 387 064	15.9874	6.8830
205	4 20 25	8 615 125	14.8178	5.8964	255		16 581 375		
206	4 94 86	8 741 816						16.0000	6.3496
207	4 28 49	8 969 748 8 998 912	14.8875	5.9155	257	6 60 49	16 974 598	16.0812	6.8579
208	4 82 64	8 998 912	14.4222	5.9950	258	6 65 64	17 178 512	16.0624	6.8661
209	4 86 81	9 129 329	14.4568	5.9845	259	6 70 81	17 378 979	16.0935	6.8748
210	4 41 00	9 261 000	14.4914	5.9439	260	6 76 00	17 576 000	16.1 <b>24</b> 5	6.3825
<b>2</b> 11	4 45 21	9 398 981	14.5258	5.9583	261	6 81 21	17 779 581	16.1555	6.3907
212	4 49 44	9 528 128	14.5009	5.9027	262	6 86 44	17 984 728	16.1864	6.3988
213	4 58 69	9 668 597			268		18 191 447		
214	4 57 96	9 800 844					18 899 744		
215	4 62 25	9 938 375	14.6629	5.9907	265	7 08 25	18 609 625	16.2788	6.4232
216	4 66 56	10 077 696	14.6960	6.0000	266	7 07 56	18 821 096	16.3095	6.4312
217	4 70 89	10 218 313	14.7809	6.0092		7 12 89	19 084 168	16.8401	6.4893
218	4 75 24	10 860 282	14.7648	6.0185	268		19 248 882	16.8707	6.4473
219	4 79 61	10 508 459			269				
290	4 84 00	10 648 000	14.8324	6.0868	270	7 29 00	19 688 000	16.4317	6.4 <b>683</b>
221	4 88 41	10 798 861	14.8661	6.0459	271	7 84 41	19 902 511	16.4621	6.4713
222		10 941 048			272		20 123 648		
223	4 97 29	11 089 567	14.9882	6.0641	273	7 45 29	20 846 417	16.5227	6.4872
224		11 230 424			274		20 570 824	16.5529	6.4951
225	5 06 25	11 390 625	15.0000	6.0822	275	7 56 25	20 796 875	16.5831	6.5080
226	5 10 76	11 543 176			276	7 61 76	21 024 576	16.6182	6.5108
227	5 15 29	11 697 088	15.0665	6.1002	277	7 67 29	21 253 933	16.6483	6.5187
228	5 19 84	11 852 352			278				
229	5 24 41				279			16.7033	6.5848
<b>23</b> 0	5 29 00	12 167 000	15.1658	6.1269	280	7 84 00	21 952 000	16. <b>7332</b>	6.5421
281	5 88 61	12 826 391			281	7 89 61	22 188 041		
232	5 38 24	12 487 168			282	7 95 24			
288	5 42 89	12 649 337	15.2648	6.1584	283		22 665 187	16.8226	6.5654
234	5 47 56	12 812 904			284		22 906 304		
285	5 52 25	12 977 875	15.8297	6.1710	285	8 12 25	28 149 125	16.8819	6.5808
236	5 56 96	18 144 256			286	8 17 96			
237	5 61 69	13 812 058			287		23 689 908	16.9411	6.5962
288	5 66 44	13 481 272	15.4272	6.1972	288		28 887 872	16.9706	6.6089
289	5 71 21	18 651 919			289		24 187 569	17.0000	6.6115
<b>34</b> 0	5 76 00	18 824 000	15.4919	6.2145	290	8 41 00	24 889 000	17.0294	6.6191
241	5 80 81	18 997 521			291	8 46 81	24 642 171		
242	5 85 64	14 172 488 14 848 907	15.5568	6.2817	292		24 897 088	17.0880	6.6343
248	5 90 49				298		25 158 757	17.1172	6.6419
244 245	5 95 86 6 00 25	14 526 784 14 706 125			294 295		25 412 184 25 672 875		
-									
246	6 05 16	14 886 986	15.6844	6.2658	296	8 76 16	25 934 836		
247 248	0 10 09	15 069 228	15.7162	6.2743		8 82 09			
	6 15 04 6 20 01		15.7480	0.2528	2000	8 88 04	26 468 592	17.2027	0.6794
			110.7757	10.ZH12	2560	1 × 444 ()]	26 780 899	17 WUIR	~ ~~
249 250	6 95 00	15 625 000	18 0114	8 0000	900		27 000 000		

# SQUARES, CUBES, SQUARE ROOTS & CUBE ROOTS. (CONTINUED.)

Nos.	Squares.	Cubes.	Square Root.	Cube Root.	Nos.	Squares.	Cubes.	Square Root.	Cube Root.
301 302	9 06 01 9 12 04	27 970 901 27 548 608	17.8494 17.8781	6.7018	851 850	12 82 01 12 89 04		18.7 <b>85</b> 0	7.0540
308	9 18 09	27 818 127	17.4069	6.7166	858	12 46 09	48 986 977	18.7888	7.0674
804	9 94 16	28 094 464				12 58 16	44 861 864	18.8149	7.0740
305	9 80 25	28 872 625	17.4043	0.7318	800	12 60 25	44 738 875	1	
306	9 36 36	28 652 616			856	12 67 36	45 118 016 45 499 293 45 882 712	18.8680	7.0878
807	9 42 49	28 984 448				12 74 49	45 499 293	18.8944	7.0940
308 309	9 48 64 9 54 81	29 218 112 29 508 629			358 359	12 81 64 12 88 81	46 268 279	18.9473	7.1000
810	9 61 00	29 791 000				12 96 00	46 656 000		
811	9 67 21	30 090 281	17 8050	e 77750	-	18 08 21	47 045 881	10 0000	7 1904
312	9 78 44	80 871 828	17.6685	6.7824	862		47 437 928	19.0268	7.1269
818	9 79 69	80 664 297	17.6918	6.7897	868	18 17 69	47 832 147	19.0526	7.1885
814	9 85 96 9 92 25	30 959 144 81 255 875				18 24 96	48 228 544		
315	9 878 20	91 200 919	17.7450	0.001	<b>500</b>	18 82 25	48 627 125	19.1000	7.1900
816	9 98 56	31 554 498	17.7764	6.8118	366		49 027 896	19.1811	7.1581
817	10 04 89	81 855 018 88 157 482			367 368	18 46 89 18 54 24	49 480 868 49 886 082		
318 319	10 11 24 10 17 61	82 461 759			369		50 248 409	19.2024	7.1726
320		88 768 000			870		50 658 000	19.2854	7.1791
321	10 80 41	88 076 161	17 0165	8 8470	271	18 76 41	51 064 811	10 9814	7 19KK
828	10 86 84	88 886 248					51 478 848	19.2873	7.1920
828	10 43 29	88 698 267					51 895 117	19.3132	7.1984
324 325	10 49 76 10 56 25	84 012 224 84 898 125							
									•
826	10 62 76	84 645 976							
327 328	10 69 29 10 75 84	84 965 788 85 287 552	18 1108	6 8084	878	14 21 29	58 582 688 54 010 152	10 4499	7 9904
829	10 82 41	85 611 289	18.1884	6.9084	879	14 96 41	54 439 989	19.4679	7.2868
880	10 89 00	<b>85 987</b> 000	18.1659	6.9104	380	14 44 00	54 872 000	19. <b>493</b> 6	7.2482
381	10 95 61	36 964 691	18.1984	6.9174	881	14 51 61	55 306 341	19.5192	7.2495
882	11 02 24	86 594 868 86 926 087	18.9209	6.9244	882	14 59 24	55 742 968	19.5448	7.2558
888 884	11 08 89 11 15 56	86 926 087 37 259 704					56 181 887 56 628 104	19.5704	7.2622
885	11 22 25	87 595 875	18.8090	6.9451	885	14 82 25	57 066 625	19.6214	7.2748
-				1	1 1			10 0100	~ 0044
886 887	11 28 96 11 85 69	87 988 056 88 979 758				14 89 96 14 97 69	57 512 456 57 960 608	19.6469	7.2811
888	11 42 44	88 614 472	18.3848	6.9658	388	15 05 44	58 411 072	19.6977	7.2936
889	11 49 21	88 958 219					58 868 869		
840	11 56 00	89 804 000	18.4891	B.9796	890	15 21 00	59 319 000	19.7484	7.3061
841	11 62 81	89 651 891	18.4662	6.9864	891	15 28 81	59 776 471	19.7787	7.8124
342 343	11 69 64	40 001 688				15 86 64	60 236 288 60 698 457		
844	11 76 49 11 88 86	40 858 607 40 707 584				15 44 49 15 52 86	61 162 984		
845	11 90 95	41 068 625			895	15 60 25	61 629 875		
846	11 97 16	41 421 736	18 4011	7 0000	904	15 <b>68</b> 16	62 099 186	10 9007	7 9494
847	12 04 09	41 781 928	18.6279	7.0271	897	15 76 09			
848	12 11 04	42 144 192	18.6548	7.0888	898	15 84 04	68 044 792	19.9499	7.8558
849		42 508 549 42 875 000					68 521 199		
<b>30</b> 0	14 40 00	200 OLD AND	110 1000	11.02/0	) TOO	10 00 00	02 W W	μου.υυυυ	11.0001

# SQUARES, CUBES, SQUARE ROOTS & CUBE ROOTS. (CONTINUED.)

401 16 06 01 64 481 301 20.0250 7.8742 451 20 34 01 91 733 851 21.2368 408 16 16 04 64 904 808 20.0499 7.8808 452 20 43 04 32 344 408 21.2608 408 16 24 09 65 450 827 20.0749 7.3804 453 20 52 00 92 959 677 21.2838 404 16 33 16 65 939 204 20.0998 7.8825 464 20 61 16 38 56 65 93 204 20.0998 7.8825 464 20 61 16 38 576 664 21.3073 406 16 40 25 66 450 125 20.1246 7.8986 455 20 70 25 94 196 375 21.8307 407 16 56 49 67 419 14329 0.1424 7.4047 456 20 79 26 94 818 816 21.3542 407 16 56 49 67 419 14329 0.1742 7.4108 457 20 88 49 25 448 993 21.3773 408 16 64 64 67 917 312 20.1990 7.4169 458 20 97 64 96 071 913 21.4009 409 16 73 81 68 417 929 90 92377 7.4169 458 20 97 64 96 071 913 21.4009	7.6744 7.6801 7.6857 7.6914 7.6970 7.7096 7.7082 7.7188
406 16 24 09 65 450 827 20.0749 7.3954 455 20 62 00 92 956 977 [31.2838] 404 16 32 16 55 959 954 20.0956 7.8955 455 20 61 16 98 576 664 21.3073 405 16 40 25 66 420 125 20.1246 7.3895 455 20 70 25 94 196 375 21.3073 406 16 46 36 66 928 416 20.1494 7.4047 456 20 79 25 94 818 816 21.3542 407 16 56 49 67 419 143 20.1742 7.4108 457 20 88 49 95 443 993 21.3776 408 16 64 64 79 77 312 20.1907 7.4169 458 20 77 64 96 77 91 312 21.004 409 16 73 81 68 417 929 90.929 90.929 77.4399 459 21 06 81 96 702 579 31.4243	7.6801 7.6857 7.6914 7.6970 7.7096 7.7082 7.7188
404 16 38 16 16 5 939 394:90.0998/7.5925 454 50 61 16 98 576 664 21.3073 406 16 40 25 66 450 125 50.1246 7.8986 455 20 70 25 94 196 375 21.8307 406 16 45 36 66 923 416 20.1494 7.4047 455 20 79 26 94 818 816 21.3549 407 16 55 49 67 419 143:00.1742/7.4108 457 30 88 49 95 445 968 31.3776 408 16 64 64 67 917 312:30.1990/7.4169 458 20 97 64 95 071 912 21.4009 409 16 78 81 [68 417 929990.32377.4339 409 21 06 61 6 702 579 31.4243	7.6914 7.6970 7.7096 7.7082 7.7188
406 16 40 25 66 450 125 20.1246 7.8986 455 20 70 25 94 196 375 21.8307 406 16 48 56 66 923 416 20.1494 7.4047 456 20 79 36 94 818 816 21.3542 407 16 56 49 67 419 143290.1742 7.4108 457 20 88 49 95 443 993 21.3776 408 16 64 64 67 917 312 20.1990 7.4169 458 20 97 64 95 071 912 21.4000 409 16 73 81 68 417 92990.92377.4329 459 21 06 81 96 702 579 31.4243	7.6914 7.6970 7.7096 7.7082 7.7188
4071 16 56 491 67 419 148190.17427.41061 4571 20 88 491 95 448 988131.87761 4081 16 64 641 67 917 312 20.199017.41691 4581 20 97 641 96 071 913 21.4009 4091 16 73 811 88 417 929980.32837[7.4839] 4590 21 06 811 96 702 579191.4243	7. <b>7096</b> 7. <b>7082</b> 7. <b>7188</b>
408  16 64 64  67 917 312 30.1990 7.4169  458  20 97 64  96 071 913 21.4009  409  16 73 81  68 417 929 30.2237 7.4329  459  21 06 81  96 702 579 31.4248	7.7082 7.71 <b>8</b> 8
409 16 72 81 68 417 929 90.3237 7.4339 459 21 06 81 96 702 579 21.4248	7.71 <b>88</b> 7.71 <b>94</b>
	7.7194
410 16 81 00 68 921 000 20.2485 7.4290 460 21 16 00 97 836 000 21.4476	
411 16 89 21 69 426 581 20.2781 7.4850 461 21 25 21 97 972 181 21 4709	
412 16 97 44 69 984 528 20.2978 7.4410 462 21 84 44 98 611 128 21.4942 418 17 05 69 70 444 997 20.8224 7.4470 468 21 48 69 99 252 847 21.5174	7.7806
413 17 05 69 70 444 997 20.8224 7.4470 468 21 43 69 99 252 847 21.5174 414 17 18 96 70 957 944 20.8470 7.4580 464 21 52 96 99 897 844 21.5407	7.7418
415 17 82 25 71 478 875 20.3715 7.4500 465 21 62 25 100 544 625 21.5689	
416 17 30 56 71 991 296 20.3961 7.4650 466 21 71 56 101 194 696 21.5870	7.7529
417 17 88 89 72 511 718 20.4206 7.4710 467 21 80 89 101 847 563 21.6102	7.7584
418 17 47 24 78 084 632 20.4450 7.4770 468 21 90 24 102 503 232 21 6833 419 17 55 61 78 560 059 20.4695 7.4829 469 21 99 61 108 161 709 21 6564	7.7695
420 17 64 00 74 088 000 20.4939 7.4889 470 22 09 00 108 828 000 21.6795	7.7750
421 17 72 41 74 618 461 20.5188 7.4948 471 22 18 41 104 487 111 21.7025	7.7906
428 17 89 84 75 181 448 90 5498 7 5007 479 22 37 84 105 134 048 21.7358 428 17 89 29 75 666 967 90 5670 7 5067 473 22 37 29 105 828 817 21.7486 424 17 97 76 76 325 024 20 5913 7 5120 474 22 46 76 106 486 494 21.7718	7.7860
428 17 89 29 75 686 967 20.5670 7.5067 473 22 37 29 105 828 817 21.7486 424 17 97 76 76 225 024 20.5913 7.5126 474 22 46 76 106 496 424 21.7715	7.7970 7.7970
425 18 06 25 76 765 625 20.6155 7.5185 475 22 56 25 107 171 875 21.7945	7.8025
496 18 14 76 77 808 776 20.6398 7.5944 476 22 65 76 107 850 176 21.8174	7.8079
427   18 23 29   77 854 483 20.6640 7.5802   477   22 75 29   108 531 333 21.8403  428   18 31 84   78 402 752 20.6892 7.5361   478   22 84 84   109 215 352 21.8632	7.8184
427, 18 28 29 77 854 458 90, 684017, 53902 4771 22 75 591 108 531 383 91, 8408 428 18 81 84 78 402 758 20, 6859 7, 5361 478 22 84 84 109 215 352 21, 8532 429 18 80 41 78 888 689 20, 7128 7, 5420 479 22 94 41 109 902 239 21, 8652 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8652 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 479 22 94 41 109 902 239 21, 8651 86 20 7128 7, 5420 80 80 80 90 7128 7, 8620 80 80 80 80 80 80 80 80 80 80 80 80 80	7.8548
480 18 49 00 79 507 000 20.7364 7.5478 480 23 04 00 110 592 000 21.9089	7.8997
481 18 57 61 80 062 991 20.7805 7.5587 481 23 18 61 111 284 641 21.9817	
482 18 66 24 80 621 568 20.7846 7.5595 482 28 28 24 111 980 168 21.9545 483 18 74 89 81 182 737 20.8087 7.5654 483 28 82 89 112 678 587 21.9778	7.8406
483 18 74 89 81 182 737 20.8087 7.5654 483 28 82 89 112 678 587 21.9778 484 18 88 56 81 746 504 20.8327 7.5712 484 23 42 56 118 879 904 22.0000	7.8514
435 18 92 25 82 812 875 20.8567 7.5770 485 23 52 25 114 084 125 22.0227	7.8568
436 19 00 96 82 881 856 20.2806 7.5828 486 23 61 96 114 791 256 22.0454	7.8603
437 19 09 69 83 458 458 20.9045 7.5886 487 23 71 69 115 501 308 22.0681	7.8676
488 19 18 44 84 027 672 20.9284 7.5944 488 23 81 44 116 214 272 22.0907 439 19 27 21 84 604 519 20.9528 7.6001 489 28 91 21 116 980 169 22.1188	7.8784
440 19 86 00 85 184 000 20.9762 7.8059 490 24 01 00 117 649 000 22.1859	7.8887
441 19 44 81 85 766 121 21.0000 7.6117 491 24 10 81 118 370 771 22.1565	
- 442  19 58 64  86 850 888 21.0238 7.6174  492  <b>24</b> 20 64  119 0 <b>95 488</b>   22.1811	7.8944
444 19 71 86 87 528 384 21.0713 7.6289 494 24 40 36 120 558 784 22.2261	7.9051
445 19 80 25 88 121 125 21.0950 7.6846 495 24 50 25 121 287 875 22,2486	7.9105
446 19 89 16 88 716 586 21.1187 7.6408 496 24 60 16 122 023 986 22.2711	7.9158
447  19 98 09  89 814 623 21.1424 7.6460  497  24 70 09  122 768 478 22.2985 7	7.9211
448 20 07 04 89 915 892 21.1660 7.6517 498 24 80 04 128 505 993 22.8159 449 20 16 01 90 518 849 21.1896 7.6574 499 24 90 01 124 251 499 22.8388 7	7.9817
450 20 25 00 91 125 000 21.2182 7.6681 500 25 00 00 125 000 000 22.8607	.9870

#### SQUARES, CUBES, SQUARE ROOTS & CUBE ROOTS.

(CONTINUED)

Nos	Bq	uar	<b>06</b> .	_	Cube	١.		uare oot.		loot.	N	04	89	UAI	·es.	_ (	Jube	B		uare oot.	Root.
501	25	10	01	125	751	501	22.	8830	7.	9428	50	51	<b>3</b> 0	36	01	167	284	151	23.	4784	8.1982
502	25	20	04	126	506	008	22.	4054	7.	9476	55	52	80	47	04	168	196	608	23.	4947	8.2081
																					8.2081
504	25	40	16	128	024	064	22.	4499	7.	9581	)	4	<b>50</b>	ĕΑ	16	170	031	464	23.	5372	8.2130
505	20	<b>5</b> U	ಭಾ	128	787	CSO	ZZ.	4122	۲.	9034	OC	oo	συ	ðυ	20	170	ษอง	810	23.	.0004	8.2180
506	25	60	36	129	554	216	22.	4944	7.	9686	S.	6	30	91	86	171	879	616	23	5797	8.2220
507	25	70	49	180	328	843	22.	5167	7.	978	O.	7	81	ÛŽ	49	172	808	693	23	OUUS.	8.2278
506	ZO	ᄣ	04	181	ONO	012	22	5889 5610	4.	DO 45											8.2327
510	26	8U 01	90	182	651	000	22	5832	7.	9896	56	30	81	24 86	90	175	616	000	23	6643	8.2377 8.2426
			04	100	400	001	90	40EO	_	00.46			01	477	01	100		401		40×4	0 0 47%
511	30	# 11	21	100	90%	2000 001	00	0000 4074	١.	DOO!	100	21	01	44 RO	21	1777	500	900	8	20004 2005	8.2475 8.2524
012 K19	20	21 91	80	125	005	807	22	RACK	g.	OOK!	2	10	21	80	Ã	178	459	547	23	7278	9 9575
510 K14	28	41	GR.	135	798	744	22	6716	g.	010		4	31	Ã	QA.	179	406	144	28	7487	8.2578 8.2621
515	26	52	25	136	590	875	22	6936	8.	9156	56	35	31	92	25	180	362	125	28	7697	8.2670
K1A	98	gυ	RR	197	200	noe	99	715B	Q	വരവം	1	20	99	ΩR	KR	181	991	408	98	7006	8 9710
517	26	72	80	122	188	418	22	7876	Š.	0260		37	32	14	89	182	284	268	28	8118	8.2768
518	26	83	24	188	991	882	22	7596	8	0311	56	38	32	26	24	183	250	432	23	8828	8.2816
519	26	93	61	189	798	859	22	7816	8.	0368	56	39	82	37	61	184	220	009	23	.8537	8.2719 8.2768 8.2816 8.286
520	27	04	00	140	608	000	22	8035	8.	0418	57	70	32	49	00	185	198	000	23	.8747	8.2918
521	27	14	41	141	420	761	22	8254	8.	0466	57	71	82	60	41	186	169	411	23	.8956	8.2969 8.3010 8.8059 8.3107
522	27	24	84	142	236	648	22	8478	8.	0517	5	72	82	71	84	187	149	248	28	.9165	8.3010
523	27	85	29	148	055	667	22	8692	8.	0569	57	78	82	83	29	188	132	517	28	.9874	8.8059
524	27	45	76	143	877	824	22	.8910	8.	0620	5	74	82	94	76	189	119	224	23	.9581	8.310
625	27	56	25	144	708	125	22	.9129	8	067	5	75	88	06	25	190	109	375	28	.9792	8.3150
526	27	66	76	145	581	576	22	.9347	8.	072	5	76	83	17	76	191	102	976	24	.0000	8.3203 8.325 8.330
527	27	77	29	140	863	183	22	.9565	8	.0774	1 5	77	88	29	29	192	100	088	24	.U.U.	8.825
	27	8	84	144	197	904	22	.978U	Ö	000	9 2	18	88	4U	64	120	100	500		OPPO	0.000
580	28	98	00	146	877	000	23	.0217	18	.092	7 5	80	38 38	64	00	195	112	000	24	.083	8.834 8.389
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500	30	18	01	150	N KAC	789	20	0481	Ö	100		97	33 99	90	01	190	192	941	04	1001	8. <b>344</b> 8. <b>349</b>
KQS	20	40	20	151	410	487	20	OGGS.		102		04 99	33	os de	20	100	155	997	94	1454	8.353
584	28	51	S.A	159	27	200	29	1084	ĺŘ	119	1 5	Ñ	84	10	54	100	176	704	24	1661	8.358
585	28	62	25	15	180	375	23	.1801	Š	.118	5	85	84	22	25	200	201	62	24	.1868	8.363
KRE	128	72	Q.F	151	906	ALV	28	1512	78	123	1 5	æ	84	23	98	201	230	OSF	24	2074	8.368
587	28	83	69	15	854	155	22	178	ığ	.128	illis	87	84	45	69	202	262	00	24	.228	8.368 8.373
58	1128	94	44	115	5720	872	2 23	.1948	318	.183	2115	88	84	-57	<b>' 4</b> 4	11200	297	472	24	.248	718.377
589	29	00	21	150	3 590	818 (	) 23	.216	18	.138	2  5	89	84	68	21	204	. 336	469	) 2 <b>4</b>	.2690	3 8.382
540	) 29	16	00	15	7 46	1 000	) 28	.2371	9 8	.143	8 5	90	34	81	00	200	879	000	24	.2899	8.387
54	1 29	26	81	15	8 <b>84</b> 0	421	1 28	.259	18	.148	8 5	91	34	92	81	200	425	071	24	.3100	8.891 8.396
54	2 29	37	64	1 15	9 220	089	3 23	3.280	9 8	.158	3  5	92	85	04	64	207	474	1 686	3 24	.381	18.396
54	8 29	48	49	16	0 10	3 00	7 2	.802	18	.158	8  5	63	85	16	4	200	527	857	24	.8510	8.401 8.406
54	4 29	5	8	16	98	18	12	.823	3 8	.163	3 5	94	85	25	36	201	584	584	24	.372	18.406
	- 1			Ī			1		1		- 11		i i			i			1		8.410
54	6 29	8	10	16	2 77	1 88	8 2	3.366	8	.178	8 5	96	8	55	10	21	700	78	3 24	.418	1 8.415 8 8.420
54	22	, y	Ň	16	5 66°	7 82	0 2	3.888	١	1.178	o o	) V (	S.	04	, U	121	77(	177	3 24	454	DO.420
54	الارة	Ų	S U	116	2 00	0 04/		5.4U9	1	100	3	ACC COO	100		) U	101	09	ישני ו	100	474	08.424
04	000	14	. U.	110	0 40 a 97	5 AA	0	3,45U 3 459	18	, 100 1 100		m	100	, og	) (V.	101	: 878. } (N∩	100	18	1.414 1.404	5 8.429 9 8.484
6363	いるし	, 4	·	110	0 0/	U UU	UKE	). <del>4</del> 0%	#IC		w)  C	,,,,,	OC	, 0		No.T.	,	, 001	100	. 101	alo. 202

## SQUARES, CUBES, SQUARE ROOTS & CUBE ROOTS (CONTINUED.)

### SQUARES, CUBES, SQUARE ROOTS & CUBE ROOTS

_	Squa			Cube			uare loot.	ᆜ	Cube Root.	Nos	_			_	Jube		B	uare oot.	B	ube oot.
701	49 14	01	844	472	101	26	4764	8	.88 <b>3</b> 3 .8875	751	56	40	01	428	564	751	27	4044	9.	0896
708	40 X	5 ()4	840	948	406	20	4908	8	8675	752	56	55	04	425	259	008	27	4226	9.	0987
704	10 1/ 40 R	5 US	940	925	884	80	.D141	0	.8917 .8959	708	20	70	W	400	907	777	27	.4400 .4591	y.	1017
705	49 7i	25	850	402	625	26	.5518	8	9001	755	50 57	60	25	490	388	875	27	4001 4778	9.	1017 1087
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706	49 8	86	851	895	816	26	.5707	8		756								4955		
707	49 Y	49	500	898	248	20	.5000	8	9085	757	57	90	49	488	798	098	27	5136	9.	1128
700	20 O	6 04 1 01	304	400	ALE	20	.0U68	ğ	9127 9169	708	57	40	64	430	519	51%	27	5818	٦.	1178
710	50 4	00	357	911	000	26	.645R	8	9211	780	57	76	笳	488	240 978	000	27	5691	å.	1210 1258
- 1			i			ļ		1		1	ŀ									
711	50 SK	81	359	425	481	26	.6646	8	9258	761	57	91	21	440	711	081	27	5862	9.	1298
712	50 61	44	860	944	128	26	.6888	8	9295 9887	762	58	06	44	442	450	728	27	.6043	9.	1338
713	0U 83	, 04	200	407	044	20	7061	ğ	.9878	708	ρö	21	땅	444	194	947	27	02200	y.	1378
715	51 15	25	265	505	875	26	7896	8	9420	785	20	KO	98	440	807	195	5	04U0	å.	1450
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716	51 20	56	367	061	696	26	7582	8	9462	766	58	67	56	440	455	096	27.	6767	9.	1498
717	51 40	89	868	601	818	26	.7700	8	9508 9545	767	58	82	89	451	217	668	27.	6948	9.	1587
718	DI DE	24	870	140	222	20	7800	Ö.	9040	768	58	26	24	458	964	832	27.	7128	9.	1577
790	S1 84	i m	273	948	m	28	300g	8	9687 9628	709	88	10	D1	404 488	700	000	97	7490	ğ.	1017
			l					1	- 1	1 .							}		Į .	
781	51 96	3 41	374	805	361	26	.8514	8	9670	771	59	44	41	458	814	011	27.	7669	9.	1696
722	52 12	84	376	867	048	26	.8701	8	9711 9752	772	59	59	84	460	099	648	27.	7849	9.	1786
723	52 87	29	877	988	067	26	8667	8	9752	778	59	75	29	461	889	917	27.	8029	9.	1775
795	100 K/	96	281	079	424 108	98	S)UE	0	9794 9885	775	ผ	ᄣ	95	405 488	404	978	21.	KUSS.	y.	1010
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796	52 70	76	882	657	176	26.	9444	8	.9876	776	60	21	76	467	<b>\$88</b>	576	27.	8568	9.	1894
727	59 R	5 2 <b>9</b>	(394	240	508	28	.9829	IR.	9918	777	An	27	20	480	007	<b>488</b>	27	2717	Q	I QRR
788	52 91	84	385	828	858	20	9815	8	9959	778	60	28	84	470	910	952	27.	8927	9.	1978
790	58 90 58 90	. W.	900	017	100	07	0000 2010	3	0000	779	80	앯	41	47%	729	198	27. 07	9100	y.	WIZ.
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781	58 41	61	390	617	891	27	.0870	9.	.0082	781	60	99	61	476	879	541	27.	9464	9.	2091
788	58 58	24	392	228	168	27	0555	9.	0123	782	61	15	24	478	211	768	27.	9648	9.	<b>9180</b>
758	08 73 08 00	, es	200	832	837	27	0740	ž	0164	768	61	80	69	480	048	687	27.	9821	9.	2170
735	00 00 64 06	200	307	088	90% 97K	97	1100	9	.0246	795	81 81	40	96	461 408	798	804	20.	0170	y.	82UV 0040
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786	54 16	96	398	688	<b>256</b>	27	1298	9	.0087	786	61	77	96	485	587	656	28.	0357	9.	2287
787	54 81	l <b>6</b> 9	1400	815	558	27.	.1477	9	.0828	787	61	93	69	487	448	408	28	OKRE	9	2826
788	04 40 K4 P	44	401	V47	272	27	1662	9	.0969 .0410	788	68	(19	44	489	303	872	28.	0718	9.	2865
740	54 7	121	405	994	919	97	0000 0000	a	.0450	700	8	20 41	21	491 402	100	009	120.	1080 1080	9.	2404
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741	54 90	81	406	869	021	27	.2218	9	.0491	791	62	56	81	494	918	671	28.	1247	9.	2482
742	55 Q	64	408	518	488	27	.2307	9	.0582	792	62	72	64	496	798	088	28	1425	9	2521
748	00 21 KK 01	48	410	172	407	27	.₩580 • 2000	9	.0572 .0613	798	62	88	49	498	677	257	28	1608 1780	9.	2560
745	JO (50 NS (M	98	419	402	698	27	.ቖ/04 የ <u>አር</u>	6	.0654	704	00 69	91	98	500	450	104	90	176U	o.	9490 9490
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746	55 66	16	415	160	936	27	.8180	9	.0694	796	68	86	16	504	358	896	28.	2185	9.	2677
747	DO 81	) Uu	416	8002	722	127	.ชยาช	ΙU	.0785	1797	ĸ	522	(19	IM IS	261	573	128	2812	19.	2718
748	55 90	04	418	508	992	27	.8496	9	.0775 .0816	798	68	68	04	508	109	592	28	2489	9.	2754
750	20 T	, UI	491	275	149	21	.00/9 9041	6	.0816 .0856	600	80	04	NI NI	D10	002	999	80	2000 100	ě.	27V3
	<b></b> A	, 00	TOI	010	w	100	.0001	10	OUOU.	.000	IO.	w	w	1014	w	UUU	40	×010	J.	0002

## SQUARES, CUBES, SQUARE ROOTS & CUBE ROOTS (CONTINUED.)

So?	8q	UBI	<del>0</del> 6.	Ŀ	Cube	8.	S	uar e loot.	ŀ	Root.	Nos	89	uai	œ.	'	Cube	s.	Bo	uare oot.	Oub Root
101	64	16	01	518	922	401	28	8019	9	2870	851	72	42	01	616	295	051	29	1719	9.470
102	64	88	04	515	849	608	28	8196	9.	.2870 .2909	852	72	59	04	618	470	208	29	1800	9.480
08	64	48	09	517	781	627	28	8878	9	2948 2966	858	72	76	09	620	650	477	80.	2062	9.48
304	64	64	16	519	718	464	28	3549	9.	2966	854	72	98	16	622	885	864	20.	2283	9.487
905	64	80	25	521	660	125	28.	.8726	9.	.8025	855	78	10	25	025	026	875	29.	2404	9.491
306	64	96	36	523	606	616	28.	<b>89</b> 01	9	3063 3102	856	78	27	86	627	222	016	29.	2575	9.494
	65	12	40	005	557	940	28.	4077	9.	8102	857	78	44	40	680	422	798	29.	2746	9.49
308	65	28	64	527	514	112	28	4253	9.	8140	858	78	61	64	681	628	712	29.	2916	9.50
309	65	44	81	529	475	129	28.	4429	9.	8179 8217	859	78	78	81	683	889	779	29.	3087	9.500
310	66	61	00	581	441	000	28.	4605	9.	8217	860	78	96	00	686	056	000	29.	3258	9.50
11	65	77	21	583	411	781	28.	4781	9.	8255 8294	861	74	18	21	638	277	<b>3</b> 81	29.	8428	9.518
512	65	88	44	525	567	322	<b>N</b> 6	4906	9.	3294	862	74	80	44	640	508	928	29.	8698	9.517
118	66	ŭ	œ	637	367	797	20	5132	۶.	3332	868	74	47	60	642	735	647	29.	3769	9.520
514	00	20	30	DAA	303	144	20.	5400	۶.	3370	804	74	94	90	044	ALS.	044	zy.	2020	9.524
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316	66	58	56	543	338	496	28.	5657	9.	8447 8485	866	74	99	56	649	461	896	29.	4279	9.531
117	00	74	84	240	3225	919	20.	2000	y.	0400	007	20	10	ğ	651	714	203	<b>ж</b> .	4449	9.53
210	00	AI.	24	240	040	452	80	8100	γ.	3523 3561	000	20	34	24	000	972	000	2¥.	4000	9.55
100 0 T 0	87	94	20	681	920	000	60	0104 20Kg	S.	3599	000	70 78	51	ST.	eko	204 E00	ACC.	27. 00	4100 40ko	9.092 0 544
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21	67	40	41	558	387	661	28	.6531	9.	3637	871	75	86	41	660	776	811	29.	5127	9.550
22	07	20	64	000	41%	240	8	0000	2	8675	872	76	Ŭά	84	008	004	648	20.	DEVIO	9.000
20	07	78	2	007	441	707	20	U000U	Ľ.	8713 8751	074	76	21	29	000	200	017	29.	0400	9.00
XXX XXX	80	ᅋ	94	E41	510 515	2224 20K	60	7002	6	3789	078	70	20	98	420	001	024 078	28.	5000 5004	0 KG4
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26	68	22	76	563	559	976	28	7402	9	3827	876	76	78	76	672	221	876	<b>29</b> .	5978	9.568
200	00	25	23	000	OUN	283	80	7070	ς.	8865	077	20	ΜĪ	20	0/4	250	188	æυ.	0142	9.571
200	20	200	41	001	700	700	20	77004	8	8902 8940	010	77	æ	64	0.10	151	102	29. 66	0011	A.010
880	68	89	90	571	787	000	28	8097	õ	8978	880	77	44	<u></u>	681	472	000	29.	6648	9.589
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831	68	ω	61	578	856	191	28	8871	Ų.	4016	881	$\overline{7}$	61	61	683	797	841	29.	6816	9.588
										4053										
										4091										
										4129 4166										
100	•	12	20	JOSE	10€	010	20.	.0809	8	4100	000	10	<b>5</b> 20	220	089	104	120	20.	1200	9.00I
										4204										
387	70	05	69	586	876	258	28	9310	9.	4241	887	78	67	69	697	864	108	29.	7825	9.608
										4279										
										4316										
MU.	w	90	w	<b>5</b> 62	704	w	20	. <del>10</del> 228	۳.	.4354	990	79	<b>21</b>	w	704	909	w	25V.	8328	v.619
41	70	72	81	594	828	321	29	.0000	9.	4891	891	79	88	81	707	847	971	29.	8496	9.622
42	70	8	64	296	947	688	29	.0172	Đ.	4429	892	79	56	64	709	732	288	20.	8664	9.626
740	14	W	47	801	017	107	20	.U040	ď.	4466	696 60	73	74	49	712	IZI	907	20	8831 88631	y.029
345	71	40	25	603	351	125	29	.0689	9	4508 4541	895	80	10	25	716	917	875	20. 20.	9166	9.687
	1			l							1				1			l		
<b>92</b> 7	71	74	w	··········	640	423	23	. 10003	190	4578 4615	X97	m	48	no	721	734	9.78	90	OKANA	0 844
348	71	91	04	609	800	192	29	1204	ğ	4652	899	ăŏ	64	ŭ	724	150	709	20	2666	0.647
<b>349</b>	72	08	01	611	960	049	29	1876	9	4652 4690	899	8ñ	82	ŏi	726	572	699	20	9888	9.651
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# squares, cubes, square roots & cube roots. (continued.)

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918	184	27 2	14	778	620	682	80.	2985	19.1	7188	968		70						.1127	9.8	
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								8809			978	94	67	29					.1929	9.90	092
924	85	37 7	76	788	889	024	80.	8974	9.	7400	974	94	86	76					.2090	9.9	126
925	85	56 2	25	791	458	125	<b>3</b> 0.	4188	9.	7485	975	95	06	25	920	85	875	81	.2250	9.9	160
926	85	74 7	76	794	022	776	80.	4802	9.	7470	976	95	25	76	921	714	176	81	.2410	9.9	194
								4467			977	95	45	59	989	2 574	l 888	31	.2570	9.9	227
928	186	11 8	34	799	178	752	80.	4681	9.	7540	978	95	64	84					.2730	9.9	
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981	86	67 6	31	806	954	491	80.	5128	9.1	7645	981		23		944	1 070	141	31	.8209	9.9	368
932	186	86.8	24	809	557	568	80.	5287	9.1	7680	982		48		940	3 960	3 168	8 81	,8869	9.93	
988	187	04 8	30	812	166	237	<b>3</b> 0.	5450	9.7	7715	968		62						.3528	9.9	
								5614			984		82						.3688	9.9	
935	87	42 2	25	817	400	875	30.	5778	9,7	7785	985	97	02	25	95	5 67	020	81	.8847	9.9	197
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								6105			987	97	41	69	96	1 504	808	31	.4166	9.9	
								6268			988	97	61	44					4325	9.90	598
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194	188	92	19	888	561	807	30	7088	9.	3068	993		60		97	9 14	657	81	.5119	9.9	
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940	89	49 1	16	84R	590	586	80.	7571	9.1	8167	996	99	20	16	98	8 04'	7 936	81	.5595	9.96	366
								7784			997		40						.5758	9.9	
948	89	87	14	851	971	392	80	7896	9.	8286	998		60		99	4 01	994	81	.5911	9.9	
949	90	06.6	ml	854	670	849	130.	8068	9.	8270	999	99	80	01	99	7 00	999	81	.6070	9.9	167
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## PATENT COLD ROLLED STEEL SHAFTING, PISTON RODS, ETC.

Made to Whitworth's Standard Gauge, and accurately straightened.

	ROU	SQU	ARE.		
Diam.	Weight per foot.	Diam.	Weight per foot.	Size.	Weight per foot.
in.  5 114	67. 45 65. 50 60. 88 54. 11 52. 62 48. 26 42. 75 41. 04 89. 40 87. 57 86. 40 82. 22 27. 16 26. 09 24. 05 23. 06 22. 09 24. 05 23. 06 22. 09 21. 15 20. 21 19. 81 17. 55 16. 70 15. 89 15. 07 14. 85 16. 70 17. 85 10. 69 10. 03 9. 39 8. 78 8. 78 8. 78 8. 78	In.  In.  In.  In.  In.  In.  In.  In.	7.06 6.53 6.01 5.60 5.52 5.26 5.05 4.61 4.17 3.86 3.77 3.88 3.20 2.68 2.53 2.20 2.05 1.94 1.77 1.50 1.38 1.17 1.05 1.00 1.00 1.00 1.00 1.00 1.00 1.00	4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	54. 42 47. 84 41. 67 35. 92 30. 61 25. 72 21. 26 17. 25 13. 60 10. 41 8. 98 7. 66 6. 43 5. 31 4. 30 2. 99 2. 60 2. 25 1. 61 1. 84 1. 08 . 850 . 652 . 479 . 382 . 270 . 218

The shafts are kept on hand at the mill, in lengths of 24 feet, and are cut to any length desired.

SEND FOR OUR SHAFTING CATALOGUE.

# COLD-DRAWN STEEL HEXAGONS. SPECIAL STEEL FOR SCREWS.

Size.	Lbs. per foot.	Size.	Lbs. per foot.	Size.	Lbs. per foot.	Size.	Lbs. per foot.
16 16 8 7 16	.195 .87 .58 .56 .78	9 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6	.98 1.15 1.40 1.66 1.91	7 15 1 1 1 16 1 18	2.25 2.58 2.94 3.38 3.78	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4.15 4.60 5.07 5.57 10.82

#### PATENT COLD-ROLLED STEEL FLATS.

FOR KEYS, ENGINE GUIDES, ELEVATOR SLIDES, ETC.

We are already prepared to furnish many sizes of Cold-Rolled Steel Flats, and will provide grooves for making other sizes whenever the quantities wanted are large enough to warrant us in incurring the necessary expense.

### PATENT COLD-ROLLED STEEL

#### FINGER BARS,

#### KNIFE BACKS, Z BARS AND

ANGLE BARS

#### FOR MOWERS, REAPERS AND HARVESTERS.

Bicycle manufacturers will find our Cold-Rolled Steel especially adapted to their work.

Prices will be given on application.

Estimates made promptly for producing new shapes or special sections.

Note.—On sizes 2\frac{1}{2}' square and larger, the corners are slightly rounded. All sizes below 2\frac{1}{2}' sharp corners.

All sizes are accurately rolled.

#### TURNBUCKLES.



- D. Size=Diameter of Screw.
- A. Length in Clear between Heads.
- B. Length of Tapped Heads=1½ D.
- C. Total Length of Buckle.
- L. Total Length of Buckle and Stub Ends, when open.

Size D.	A	В	С	L	Size D.	A	В	C	L
8 7 16 9 16 8	6 6 6 6	9 6 - 48 7-910-6 9 1-95 44 82-5-1	7 to 7 to 7 to 7 to 7 to 7 to 7 to 7 to	22 22 22 22 22 22	1# 1# 2 2 2 2	6 6 6 6	25 218 3 3 36 38	11 <del>1</del> 11 <del>§</del> 12 12 <del>§</del> 12 <del>§</del>	28 29 29 29 29
\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	6 6 6	1	8 <del>1</del> 8 <del>1</del> 9 9	23 24 25 25	28 21 28 28 28	6 6 6	3 1 5 6 4 8 4 8 4 8 4 8	18 <del>1</del> 13 <del>1</del> 13 <del>1</del> 14 <u>1</u>	81 82 82 83
11 18 11 11 18	6 6 6	$\begin{array}{c} 1\frac{7}{8} \\ 2\frac{1}{16} \\ 2\frac{1}{4} \\ 2\frac{7}{16} \end{array}$	9 <del>2</del> 10 <del>1</del> 10 <del>1</del> 10 <del>2</del>	26 27 27 28	2 <del>1</del> 3 3 <del>1</del> 3 <del>1</del>	6 6 6	418 41 47 51	148 15 152 161	33 34 36 37

Lengths given above are Standard for Bridge, Roof and ordinary Truss Buckles.

They have a guaranteed strength of 60,000 pounds per square inch of section of bolt at bottom of thread. Stub bolt ends are made of good bridge iron having tensile strength of 50,000 pounds per square inch.

Open Buckles of this form can be adjusted with a bar, hook, or wrench, and have the great advantage of showing the ends of the bolts, so that inspectors can see that they have a good hold of thread, and do not butt together.

#### MENSURATION.

$$\pi = 3.1415926536$$
 $\pi = 1.5700$ 

$$\frac{\pi}{2}$$
=1.5708

$$\frac{\pi}{2}$$
=1.0472

$$\frac{\pi}{4}$$
=0.7854

$$\frac{\pi}{12}$$
=0.2618

$$\frac{\pi}{64}$$
=0.04909

$$\frac{1}{2}$$
=0.31831

$$\frac{1}{78}$$
=0.10132

$$\pi^{*}$$
 $\pi^{*}=9.86960$ 

$$\pi^{8}$$
=31.00628

log. 
$$\pi$$
=0.4971499  $\sqrt{\pi}$ =1.77245

$$\sqrt{1}_{=0.56419}$$

$$\pi$$
 log.  $\sqrt{\pi}$ =0.2485749

$$\frac{h^2 + \frac{8^2}{4}}{2h}$$

or very nearly 
$$=\frac{s^2}{8h}$$

$$n = \sqrt{r^2 - x^2 - (r - h)}$$

$$h=r-\sqrt{r^2-\frac{8^2}{4}}$$

or very nearly 
$$=\frac{s^2}{8r}$$

 $c = a \ 2 \ r \ 0.008727$ 

#### CIRCLE.

$$A =$$
area.  $d =$ diameter.

$$r =$$
radius.  
 $V =$ contents.

$$A = \frac{\pi \times d^2}{4} = 0.7854 d^2$$

$$A = \frac{a}{880} \pi r^2$$

#### SEGMENT.

$$A = \left(\frac{a}{180}\pi - \sin a\right) \frac{r^2}{2}$$

or approximately

$$\frac{h}{65}$$
 (3  $h^2+4s^2$ )

For flat segments very nearly A = 2 sh

#### MENSURATION-CONTINUED.

#### TRIANGLE.

$$A = \sqrt{s \times (s-a)(s-b)(s-c)}$$

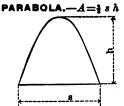
if s half of the sum of the sides a, b, and c or=base×half perpendicular height.

#### POLYGONS.

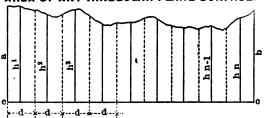
Area of any irregular polygon can be found by dividing the polygon into triangles and take the sum of the triangles' area. Area of any regular polygon

$$= \frac{\text{No. of sides}}{2} \times (\text{circumscribed rad.})^{2} \times \sin. \frac{2 \pi}{\text{No. sides.}}$$





#### AREA OF ANY IRREGULAR PLANE SURFACE.



then is, after Poncelet's rule,

$$A = d \Sigma h + \frac{1}{18} d (a-h) + \frac{1}{18} d (b-h)$$

but more exact after Francke's rule,

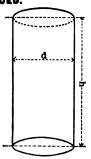
$$A = d \sum_{k=1}^{\infty} h + \frac{1}{18} d \left( 8 a + \frac{h-9}{2} \frac{h}{1} \right) + \frac{1}{18} d \left( 8 b + \frac{h-9}{2} \frac{h}{1} \right)$$

#### MENSURATION-CONTINUED.



$$A = \pi d h + \left(\frac{\pi d^2}{4}\right) 2$$

$$V = \frac{\pi d^2}{4} h$$



#### SPHERE.

$$A=\pi d^2$$

$$V = \frac{\pi d^3}{6}$$

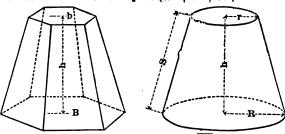
#### PYRAMID AND CONE.

A = periphery or circumference of base  $\times$  half slant height. V = area of base  $+ \frac{1}{4}$  perpendicular height.

#### FRUSTUM.

A = sum of peripheries or circumferences of the two ends $\times$  half slant height + area of both ends.

Frustum of a cone.  $V = \frac{1}{4} \pi h (R^2 + r^2 + Rr)$ 



Frustum of pyramid.  $V = h (B + \sqrt{Bb + b})$ (h being the distance of the two parallel end surfaces B and b).

#### MENSURATION-CONTINUED. PROPERTIES OF THE CIRCLE.

Circumference = Diam.  $\times$  3.1416 or 31.

 $Diam. \times .8862 = Side of an equal square.$ 

 $Diam. \times .7071 =$ 4.6 inscribed

Diam.  $^2 \times 7854 =$  Area of circle.

Radius  $\times$  6.2832 = Circumference,

Circumference = 3.5446 Varea of circle.

Diam.= 1.1283 /area of circle.

Length of arc = No. of degrees  $\times$ .017453 radius.

Degrees in arc whose length equals radius = 57° 2958. Length of an arc of  $1^{\circ}$  = Radius  $\times .017458$ .

 $1' = \text{Radius} \times .0002909.$ 

 $1'' = \text{Radius} \times .0000048$ .

 $\pi$ =Proportion of circumference to diameter=3.1415926.  $\pi^{2}=9.8696044$ .

 $\sqrt{\pi} = 1.7724588$ .

Log.  $\pi = 0.4971499$ .

$$\frac{1}{}$$
 = 0.8188001.

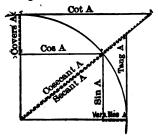
$$\frac{1}{360}$$
 = .002778.

=114.59

#### TRIGONOMETRICAL FORMULÆ. GENERAL EQUIVALENTS.

The diagram shows the different trigonometrical expressions in terms of the angle A.

In the following formulæ Radius = 1.



#### MENSURATION-CONTINUED.

Complement of an angle = its difference from 90° Supplement of an angle = its difference from 180°

$$Sin. = \frac{1}{cosec.} = \frac{cos.}{cot.} = \sqrt{(1 - cos.^3)}$$

$$Tan. = \frac{\sin}{\cos} = \frac{1}{\cot}.$$

Sec. = 
$$\sqrt{\frac{\text{Rad}^2 + \tan^2}{\text{cos.}}} = \frac{1}{\sin x} = \frac{\tan x}{\sin x}$$

$$\cos = \sqrt{(1-\sin^{s})} = \frac{\sin^{s}}{\tan^{s}} = \sin^{s} \times \cot^{s} = \frac{1}{\sec^{s}}$$

$$\cot = \frac{\cos}{\sin} = \frac{1}{\tan}.$$
 Cosec. =  $\frac{1}{\sin}$ .

Versin. = Rad.—cos Coversin. = Rad.—Sin.

Rad. =  $\tan \times \cot = \sqrt{\sin^2 + \cos^2}$ 

#### SOLUTION OF RIGHT-ANGLED TRIANGLES.

Hypoth.\*=base\*+perpend.\*

Perp. = (hyp. +base)  $\times$  (hyp. -base).

$$Sin.=a \frac{A}{C}$$

$$\cos a = \frac{B}{C}$$

Tan. 
$$a = \frac{A}{R}$$

Cosec. 
$$a = \frac{C}{4}$$

Sec. 
$$a = \frac{C}{R}$$

$$B = C \cos a = A \cot a =$$

$$\sqrt{(C+A)(C-A)}$$

$$C = \sqrt{A^2 + B^2} = \frac{A}{\sin a} = \frac{B}{\cos a}$$

C A

$$\cot a = \frac{B}{A}$$

$$\cos b = \frac{A}{C}$$

Cot. 
$$b = \frac{A}{B}$$

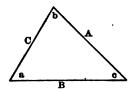
$$b = 90^{\circ} - a$$

$$A = B \tan a$$

$$A = C \sin a$$

#### MENSURATION-CONTINUED.

#### SOLUTION OF OBLIQUE-ANGLED TRIANGLES.



Value of any side C is:

$$C = \frac{A \sin \cdot c}{\sin \cdot a} = \frac{B \sin \cdot c}{\sin \cdot b} = \frac{A}{\cos \cdot b + \sin \cdot b \cot \cdot c}$$

$$C = \frac{B}{\cos a + \sin a \cot c} = A \cos b + A$$

$$C = \sqrt{A^2 + B^2 - 2AB\cos, c} =$$

$$B\cos a+B\sin a \cot b$$

Value of any angle a is:

Sin. 
$$a = \frac{A \sin \cdot c}{c} = \frac{A \sin \cdot b}{B} = \sin \cdot (b+c)$$

Sin. 
$$a = \sin b \cos c + \cos b \sin c$$

Cos. a = 
$$\sin b \sin c$$
— $\cos b \cos c$ 

$$\cos a = \frac{C^2 + B^2 - A^T}{2 B C}$$

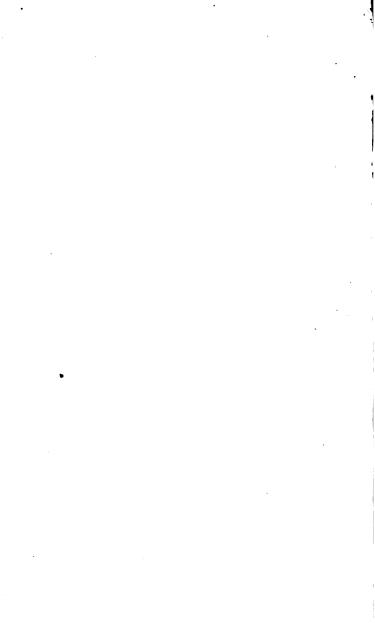
Tan. 
$$a = \frac{A \sin c}{B - A \cos c} = \frac{A \sin b}{C - A \cos b}$$

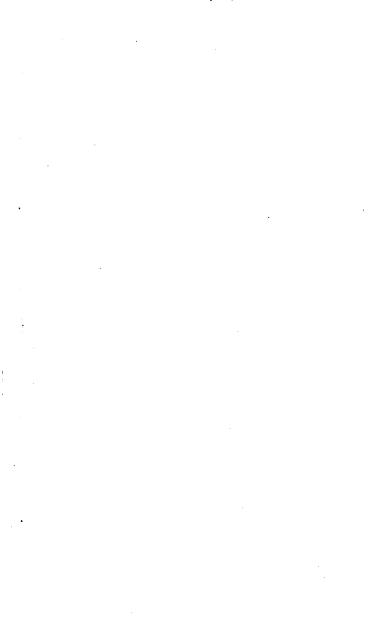
Tan. 
$$a = \frac{\tan b + \tan c}{\tan b \cdot \cos a - 1}$$

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